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# Annual Performance Evaluation of Ground Water Remediation From March 2004 Through March 2005 at the Tuba City, Arizona, Disposal Site

July 2005



# Office of Legacy Management

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Work Performed by S.M. Stoller Corporation under DOE Contract No. DE–AC01–02GJ79491 for the U.S. Department of Energy, Grand Junction, Colorado This page intentionally left blank

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# **1.0 Introduction**

## 1.1 Purpose of Report

This report evaluates the performance of the ground water remediation system at the U.S. Department of Energy (DOE) Land Management site near Tuba City, Arizona, for the period of March 2004 through March 2005. The site is located in Coconino County, Arizona, within the Navajo Nation and near Hopi Reservation land (Figure 1). Ground water in an underlying sandstone aquifer is contaminated by inorganic constituents from former uranium-ore milling at the site, including nitrate, uranium, and sulfate, the primary site contaminants. A pump-and-treat remediation system constructed to restore ground water quality began full operation in mid-2002.

## 1.2 Ground Water Remediation System

The ground water remediation system currently operates 25 extraction wells completed within the most contaminated region of the aquifer. The extracted water is conveyed in underground piping to an on-site facility where it is mechanically distilled following ion exchange pretreatment. Engineered solar evaporation ponds receive the waste liquid (brine), and an infiltration trench located upgradient of the contaminant plume returns the treated water (distillate) to the aquifer. Six injection wells originally intended to create a hydraulic barrier at the downgradient limit of contamination remain unused for that purpose. Eight additional extraction wells (wells 1126 through 1133) installed in summer 2004 were not in service during this review period. These wells, and four monitoring wells recently converted to extraction use (wells 935, 942, 936, and 938), will be in service by summer 2005. Figure 2 shows the primary site features.

## 1.3 Ground Water Compliance Strategy

The ground water compliance strategy for the Tuba City site, as defined in the *Phase I Ground Water Compliance Action Plan for the Tuba City, Arizona, UMTRA Site* (GCAP) (DOE 1999), is to achieve applicable cleanup levels through active remediation of those portions of the aquifer affected by previous site activities. Cleanup levels for the aquifer comprise restoration "standards" (requirements of 40 CFR 192 [Uranium Mill Tailings Radiation Control Act]), and restoration "goals" (cleanup levels requested by the Navajo Nation but not required by 40 CFR 192).

Ground water contaminants requiring active remediation at the site are molybdenum, nitrate, selenium, sulfate, and uranium [DOE 1999]). Restoration standards (see Table 1) for these constituents, except sulfate, correspond to a maximum concentration limit (MCL) in ground water as established in 40 CFR 192. Sulfate is not regulated by 40 CFR 192. However, a restoration standard was adopted for this constituent because it is present in ground water at the site at concentrations that cause an excess potential risk (DOE 1999). The Navajo Nation also requested that the distillate not exceed 20 mg/L of sodium.

#### Table 1. Ground Water Remediation Goals

Constituent/Property	Cleanup Level	Baseline Concentrations in Plume	
Nitrate <sup>a</sup>	10 mg/L as N (44 mg/L as $NO_3^{-}$ )	840–1,500 mg/L	
Molybdenum <sup>a</sup>	0.10 mg/L	0.01–0.58 mg/L	
Selenium <sup>a</sup>	0.01 mg/L	0.01–0.10 mg/L	
Uranium <sup>a</sup>	30 pCi/L (0.044 mg/L) U-234 + U-238	0.3–0.6 mg/L	
Sulfate <sup>a</sup>	250 mg/L	1,700–3,500 mg/L	
TDS <sup>b</sup>	500 mg/L	3,500–10,000 mg/L	
Chloride <sup>b</sup>	250 mg/L	20–440 mg/L	
рН <sup>ь</sup>	6.5–8.5	6.3–7.6	
Corrosivity <sup>b</sup>	not corrosive	not applicable	

<sup>a</sup>Restoration standard

<sup>b</sup>Restoration goal

## 1.4 Performance Monitoring and Reporting

Performance of the ground water remediation system is evaluated yearly upon receipt of water quality and water level monitoring data obtained in August and February of each year. These data are compared to baseline conditions to evaluate the capture zone of the extraction system, movement of contamination in the aquifer, and concentration trends, as measures of aquifer restoration progress.

Additionally, the composition and volumetric totals of treatment system inflow and outflows are determined weekly, and each extraction well is sampled monthly for water quality analysis. These data are used to track the extraction and treatment volumes, contaminant mass recovery, distillate composition, and waste production.

The semi-annual monitoring events covered in this report occurred in August 2004 and February 2005. Monitoring data obtained between 1998 and March 2002 represent baseline conditions at the site (DOE 2003). The 13-month review period for this report includes March 2004 through March 2005.

## 1.5 Ground Water Hydrology

The Tuba City site lies on the middle of three alluvial terraces associated with ancestral flow in Moenkopi Wash, located about 1.25 miles southeast of the site. The regionally extensive Navajo Sandstone, a massively cross-bedded, friable, fine to very fine sandstone and siltstone, underlies coarse, semi-indurated, Quaternary alluvium at most terrace locations. Loose dune sand and silt is prevalent to depths of up to 20 feet except where bedrock slopes and cliffs dominate the terrace escarpments. Regional bedrock dip is about one degree to the northeast.

Within about 200 feet below ground, the eolian dune deposits of the "classic" Navajo Sandstone become interbedded with fine-grained alluvium more typical of the underlying Kayenta Formation. This "inter-tonguing interval" is 400 to 450 feet thick. Occasional thin ( $\leq 2$  feet [ft]), resistant limestone beds occur throughout as relicts of former playa lakes. Locally, the Kayenta Formation consists of 100 ft or more of slope-forming, flat-lying red silt and fine sand.

Ground water beneath the Tuba City site occurs in the regionally extensive "N" multiple-aquifer (Cooley et al. 1969), which in the site area comprises the Navajo Sandstone. From the ambient water table about 50 to 60 feet below ground at the site, the saturated zone extends through the inter-tonguing interval to the upper contact of the Kayenta Formation.

Ground water flow beneath the site is southeast to Moenkopi Wash. There, regional discharge occurs from a laterally extensive (miles) spring zone that outcrops near the exposed base of the inter-tonguing interval. Some local discharge of ground water from higher in the formation occurs to sustain scattered populations of desert phreatophytes, such as in the "greasewood area" shown in Figure 2, where depth to water is only about 20 feet. Plant uptake requires this water to reside in fractured, decomposed, or unconsolidated material rather than competent bedrock. Figure A-1 in Appendix A depicts a conceptual model of the site hydrogeology.

#### 1.5.1 Vertical Discretization of the N-Aquifer

Site hydrostratigraphy is discretized into 50-ft intervals, or "horizons," each with a letter designation. The top of the middle terrace, nominally 5,050 feet in elevation, marks the top of the uppermost horizon (Horizon A). Horizons A, B, C, and possibly D span the interval of "classic" Navajo Sandstone beneath the site, whereas the depths of Horizons E through J include the regions of the inter-tonguing interval. Horizons K, L, and M include the lower intertonguing interval and possibly the upper Kayenta Formation. These stratigraphic relationships to aquifer horizon are shown in Figure A-1.

Related to ground surface topography, the uppermost horizon on the lower terrace progresses from Horizon C to D, north to south. The steep topography at Moenkopi Wash intersects Horizons E through G. Ground water remediation at the site focuses primarily on the upper 250 ft of the bedrock aquifer (Horizons A through E).

Color-coding in Figure 2 identifies the horizon in which the mid-point of each well screen is located for extraction wells (round symbols) and monitoring wells (square symbols). Figure A-2 of Appendix A is a cross-section schematic of the placement depth of well screens in relation to aquifer horizon for all project wells.

# 2.0 Treatment System Performance

## 2.1 Bulk Treatment Parameters

During the review period the treatment plant operated for 344 of 392 total days, for a net onstream factor of 88 percent. About 48-million gallons of water were treated during this 56-week period resulting in an average operating rate of 97 gpm and an effective rate (downtime included) of 85 gpm. The operating capacity of the treatment plant as currently configured is about 120 gallons per minute. Total ground water treatment as of April 1, 2005 was approximately 136-million gallons, equivalent to about 11 percent of the total estimated volume of uranium-contaminated ground water present before the start of remediation (see Section 5.3). Figure 3 shows the feed rate to the treatment plant and the corresponding concentration of nitrate and sulfate determined from weekly composite samples since the start of remediation. Uranium concentration in the bulk feed for the same period is shown in Figure 4. These figures indicate that contaminant concentrations entering the treatment system have remained relatively stable while the treatment plant is operating. A slight downward trend in uranium concentrations over time is indicated in Figure 4. The masses of nitrate, sulfate, and uranium extracted during the current review period, based on the weekly inflow volume and feed composition are respectively, 159,000 lbs, 389,000 lbs, and 102 lbs (Table 2).

Contaminant	Typical Concentration (mg/L)	Distillate Concentration (mg/L)	Mass Removed during Review Period (Ib)	
Nitrate	400	5-15	159,000	
Sulfate	970	20-40	389,000	
Uranium	0.25	0.004-0.01	102	

Table 2. Treatment System Performance Summary

## 2.2 Distillate Quality

Concentrations of nitrate, sulfate, and uranium in the distillate averaged about 9, 30, and 0.008 mg/L, respectively, during the review period (Table 2 and Figure 5). Total dissolved solids (TDS) ranged between about 40 and 80 mg/L, and chloride concentrations were generally less than 2 mg/L with little variation. These results indicate highly effective contaminant removal and very high quality of water returned to the aquifer.

## 2.3 Return Flow to the Aquifer

Weekly production of wastewater sent to the evaporation pond averaged about 7 percent of the total inflow rate for the year in review. The balance of the treated water (93 percent) was returned to the aquifer at the infiltration trench.

# 3.0 Extraction & Infiltration System Performance

#### 3.1 Extraction Wells

In Figure 2, the extraction wells that operated during this review period are those labeled 1101 to 1125. They are constructed of 6-inch diameter Schedule 40 PVC solid casing and 6-inch, continuous V-wrap stainless steel (0.017-inch slot). A filter pack of 20-40 graded silica sand completes the 2-in annulus to 30 or 40 feet above the screen slots. Screen lengths are 150-ft, extending from the bottom half of Horizon B to the mid-depth of Horizon E, except for wells 1116, 1117, and 1118, which have 100-ft screens that extend nearly to the base of Horizon D. Extraction wells 1126 to 1133, installed in September 2004, are of similar specification but consist of 4-inch diameter casing and screen. In addition, they are much shallower such that their 30-ft screen is located across most of Horizon B. These latter wells will become operational in summer 2005, but currently serve as monitoring wells. All extraction pumps are 1/4 to 1/3

horsepower submersible type, located 10 to 15 ft above the bottom of the well. Pumping is interrupted when the water level reaches the pump intake and resumes after a prescribed period of water level recovery.

The production rate of the well field is generally equivalent to the treatment plant feed rate shown in Figures 3 and 4. Although not obvious in the figures, total well-field production increased during the review period by about 10 gpm after wells 1116 and 1117 were returned to service in July after pump failures in March and December 2003, respectively. In addition, pump controls were adjusted in July 2004 to maximize well yield and minimize on-off cycling due to excessive drawdown. As a result, pumping is nearly continuous at all but wells 1123 and 1120. Continuous pumping rates range between 2 and 5.5 gpm, and average 4 gpm. Wells 1120 and 1123 operate half-time at rates of 7 and 0.5 gpm, respectively. In map view, there is no apparent relationship between location and extraction rate. The operational history of each extraction well for the evaluation period is included in Appendix A, Table A–1.

# 4.0 Extent of Ground Water Contamination

Figures 6a through 14a illustrate the concentrations of nitrate, sulfate, and uranium in ground water before the start of remediation. Most of the information is from sample collection in March 2002 but extends back to 1999 for some locations. These figures define contaminant distribution during the baseline period in the various aquifer horizons shown. Figures 6b through 14b show contaminant distribution in February 2005 (new extraction wells 1126 through 1133 were not operating during the review period). Although each well location sampled for the respective period is shown, a concentration value is posted only where the applicable remediation standard was exceeded. Tabulated analytical results for August 2004, February 2005, and the baseline period for each contaminant requiring remediation are included in Appendix B.

In map view, the horizontal extents of contamination in the various horizons are not significantly different from the baseline condition, indicating no lateral spreading of the contaminant plume (sentinel well 271, located southwest of well 267, was not sampled in February 2005 but remained uncontaminated as of August 2005; see also Section 5.1 for additional discussion regarding plume expansion). The new wells installed on the middle terrace (extraction wells 1126 through 1133 and monitoring wells 281 through 283) confirmed suspected contamination in Horizons A and B at each of those locations within the previously defined plume boundary.

Before installation of wells 272 through 276 in August and September 2004, discrete depth monitoring of Horizons C and D in the main area of the plume was not possible. Sample collection in February 2005 indicates contamination at the respective depths of wells 273 and 275 (Figures 7b, 10b, and 13b), but no contamination in the screened intervals at the remaining locations (wells 272, 274, and 276). The absence of contamination in Horizon E (see Figures 8b, 11b, and 14b) suggests no downward plume movement to this depth. Deeper in the aquifer, contamination remains at Horizon I wells 254 and 256, and Horizon M wells 255 and 257. As discussed in Section 6.2, the origin of contamination at these latter locations is attributed to downward leakage of shallower ground water through failed annular seals. Contamination at well 251 (Horizon E) during the later portion of the baseline period, before which the contamination was not present, is possibly of the same origin. Contaminant concentrations at

well 251 have since decreased to below cleanup standards in response to ground water extraction.

On the lower terrace, nitrate and sulfate contamination remains minor and localized to one or two wells (Figures 7b and 10b). Uranium contamination at the single lower terrace location decreased to less than the remediation standard during the review period (see also Section 5.1 for additional information on concentration trends). New monitor wells installed on the lower terrace during the review period (wells 277, 278, and 279) confirmed the absence of contamination at those locations.

## 4.1 Capture Analysis

#### 4.1.1 Water Table Configuration

Figure 15 shows the phreatic surface for the baseline period estimated using water levels in Horizon A and B monitor wells for the middle terrace and Horizon C wells for the lower terrace. On the middle terrace, water levels from deeper wells are not representative of water table conditions because of pronounced vertical hydraulic gradients (see Section 4.1.4), and within the network of monitoring wells between the escarpment and greasewood area, the water table beneath the lower terrace occurs in Horizon C. The horizontal direction of ground water flow was predominantly south during the baseline period. A steeper hydraulic gradient corresponds to aquifer thinning at the escarpment (Figure 15).

Figure 16 shows a similarly constructed water table for February 2005. At that time, ground water mounding and increased hydraulic gradients in Horizons A and B were evident along the north edge of the disposal cell due to infiltration of treatment system distillate at the trench. Comparison of Figures 15 and 16 indicates that operation of the extraction wells has significantly depressed the water table and consequently changed flow directions in the shallow ground water throughout the area of extraction where shallow monitor wells are present. Insufficient well control in the area of ground water extraction on the east side of the site prevents analysis of water table conditions there. The water table underlying the escarpment and lower terrace appears unaffected by ground water extraction.

#### 4.1.1.1 Infiltration Trench

The infiltration trench is constructed into bedrock along the north side of the site (see Figure 2 for trench location). Distillate enters the trench at its mid-point from where it can flow in either direction in perforated pipe embedded in a 3 ft thick gravel pack. Through mid-2003, non-uniform infiltration caused greater than 20 ft of ground water mounding beneath the southwest section of the trench but only about 1 ft beneath the northeast section. The ground water mound has become more symmetrical since November 2003 when flow valves were installed and all inflowing water was diverted to the northeast segment of the trench. Water level hydrographs for wells located near the respective ends of the trench (wells 687 and 688, Figure C-1, Appendix C) indicated that the northeast section would soon experience excessive mounding if a correction were not made. Since April 2005 therefore, a portion of the inflow was diverted to the southwest section of the trench.

The absence of ground water in new wells 284 and 285 (see Figure 2 for location), screened across the contact of the terrace alluvium and bedrock immediately downgradient of the trench,

indicates that mounding has not over-topped the trench to saturate the alluvium. Ground water flow from the trench area is south to the extraction wells to assist in flushing the main region of contamination.

#### 4.1.2 Water Level Drawdown

Figure 17 further illustrates the effect of ground water extraction and infiltration on water levels in Horizons A and B by showing the difference between baseline and February 2005 water levels as the computed drawdown. Figures 18 and 19 plot the drawdowns for the deeper horizons for the same period. Positive values identify locations where the water level in February 2005 is less than the baseline value. Negative values, such as those at the wells surrounding the infiltration trench (Figure 17), indicate that water levels at the respective locations are presently higher than during the base-line period. Well hydrographs in Appendix C provide an additional view of water level drawdowns over time at numerous site monitoring wells.

The overall pattern of water level drawdown reflects three-dimensional converging flow to the extraction wells. Because the water level in each extraction well is generally maintained near the base of the well (Horizon D or E), the greatest drawdown (44 ft) is observed at the Horizon E wells (wells 251 and 268) located within the extraction field. Among all monitor wells, the intakes of wells 251 and 268 are nearest in radial distance to the interval of ground water extraction. Consistent with convergent flow, drawdown at the remaining monitor wells is observed to decrease with distance from the extraction zone. Although water level drawdown in response to ground water extraction affects the entire aquifer within the region of contamination, it does not imply capture of all contaminated ground water.

#### 4.1.3 Horizontal Capture

Figures 20 and 21 depict the estimated zone of ground water capture by the extraction system for Horizons A and B combined, and Horizons C and D combined, respectively. In these figures, the extent of contamination (solid line) is generalized from the distributions presented in Figures 6a through 14b. The dashed line represents the capture zone as determined by hydraulic gradient vector analysis within respective depth intervals using a model of triangulation with linear interpolation and February 2005 water levels. Water levels in the extraction wells were not included in either analysis.

The results indicate that the estimated capture zone of Horizons A and B (Figure 20), within which all ground water ultimately reaches an extraction well, does not fully encompass the extent of contamination. The residual area between the extent of contamination and capture zone on the middle terrace is the targeted zone for the extraction wells installed in 2004. In the east area of the site, where A and B Horizon monitoring wells are absent, the estimated capture zone assumes that significant drawdown (20 ft) in Horizon C at wells 683 and 684 (not contamination in Horizons C and D wells on the middle terrace is fully captured (Figure 21). The horizontal extent of capture in Horizon E and deeper cannot be determined with the available wells completed in those horizons. This limitation is of no consequence because contamination is absent from these horizons.

#### 4.1.4 Vertical Capture

Hydrographs included in Appendix C for selected sets of co-located monitor wells illustrate that at a given location, the piezometric head is a function of well-intake depth. This relationship clearly identifies vertical flow components throughout the entire monitored thickness of the aquifer, both before and since the start of ground water remediation. With few exceptions, the vertical potentials were downward during the baseline period.

Since that time, the magnitude of downward flow in the horizons above the extraction interval has increased, as seen as the greater water level differences in the hydrographs for the respective locations of well pairs 265/266, 263/264, 908/912, and 909/932, since about mid-2002 (see Appendix C, Figures C-4 through C-7). In the main region of contamination, these increased gradients imply capture of ground water from the upper horizons by the extraction wells.

In the deeper horizons, vertical gradients are now generally upward to the extraction intakes. For example, the vertical flow potentials have reversed to upward between Horizons M, I, and E at co-located wells 268/256/257 in response to ground water extraction (Figure C-8). A similar result between Horizons E and I, and possibly M, is apparent at the location of wells 251/252/253 (see Figure C-9, the monitoring record is incomplete for well 253, a former Horizon M well that was abandoned in 2001). A downward flow potential remains between Horizon I and M at wells 254/255 (Figure C-10); however, there is an upward gradient at that location between Horizon I (well 254) and Horizon D (well 277). The apparent vertical flow divide at this location implies ground water capture possibly to Horizon I but not Horizon M.

Because the observed vertical influence of the extraction wells extends much deeper than the presumed depth of contamination, it is likely that the remediation system captures the full vertical extent of the contaminant plume. Although ground water extraction has no affect on downward flow between Horizons D and G at wells 915 and 916 (Figure C-11), this region of the aquifer is not contaminated. Downward flow potentials in lower terrace ground water also remain unaffected by ground water extraction (Figure C-12) but contamination there is only minor and limited to the shallowest horizon and there is no evidence of vertical or lateral spreading of contamination in the lower terrace ground water.

# 5.0 Remediation Progress

## 5.1 Contaminant Concentration Trends at Monitor Wells

Appendix D contains time-series graphs of nitrate, sulfate, and uranium concentrations, respectively, in ground water at selected monitor wells located throughout the project area.

Within Horizons A and B, wells 940, 941, and 942 are nearest the south side of the disposal cell and so are likely to first detect return flow from the infiltration trench as a pronounced decrease in contaminant concentration. Such trending at these locations has not yet been observed (see Figure D–1 through D–3). Assuming porous media flow under the observed water table gradient (Figure 16) and hydraulic conductivity of 1 ft/day, the calculated travel time from the infiltration trench to well 940 is 17 years, which is greater than the cumulative remediation period to date.

Farther south in the mid-section of the plume (near Horizon A and B wells 262, 906, 908, 934, 935, and 936), concentrations generally remain relatively stable, with local exceptions of either increasing or decreasing trends. Toward the outer (south) margin of the plume (near wells 263, 265, 267, and 909), contaminant concentrations are relatively stable or decreasing. Horizon A and B sentinel wells, specifically those located near the plume boundary (wells 271, 683, 684, 914, and 921), remain uncontaminated with the exception of minor but stable nitrate contamination at well 929, indicating no significant expansion of the contaminant plume (Figures D–4 through D–6).

Stable concentrations below remediation standards in Horizon C and D wells 264, 266, 915, and 932 (Figures D–7 through D–8) indicates no southward plume expansion to these locations at this depth of the aquifer. In these figures, elevated nitrate and sulfate concentrations at well 912 (Horizon C) are seen to decrease over time, which also indicates that contaminants are not spreading to the west of that location. In ground water beneath the lower terrace, uranium contamination did not exceed the restoration standard at any location during the past year. Previously, uranium contamination in lower terrace ground water was limited to low levels at co-located wells 691 and 1003. These are also the only wells with appreciable nitrate and sulfate contamination on the lower terrace. Stable concentration trends have not developed for these constituents at these wells. At three other nearby wells, stable nitrate values only marginally exceed the restoration standard. Migration of the very localized and relatively low magnitude contamination on the lower terrace apparently is not significant, as indicated by persistent background levels at nearby wells located farther downgradient. Contaminant concentration plots for lower terrace monitor wells are include in Appendix D (Figures D–10 through D–12).

# 5.2 Contaminant Concentration Trends at Extraction Wells

Figures 22, 23, and 24 illustrate concentration trends at the extraction wells for nitrate, sulfate, and uranium, respectively. For each contaminant, the trend at most wells is of decreasing concentration as contaminant mass is removed from the aquifer. Appendix E contains concentration plots for each extraction well based on the monthly on-site sampling and analysis (in Appendix E, concentration units are mg/L for nitrate as NO<sub>3</sub> and sulfate, and  $\mu$ g/L for uranium).

Figures 25, 26, and 27 are identical to the previous three figures but at a finer concentration scale to highlight occurrences of ground water extraction at concentrations less than the respective remediation standards. In a summary of that information, Table 3 identifies that at no location is the extract below the remediation standard for all three contaminants, although very nearly so at wells 1113 and 1125.

Nitrate	Sulfate	Uranium	
	1107		
	1112	1112	
1113 <sup>a</sup>	1113	1113	
		1114	
	1116	1116	
		1117	
	1123	1123	
1125 <sup>a</sup>	1125	1125	

Table 3. Pumping Wells where a Contaminant Concentration
is Below the Remediation Standard in the Extract

<sup>a</sup>Concentration is currently 45 mg/L nitrate as NO<sub>3</sub>.

#### 5.3 Contaminant Inventory and Removal Rates

Table 4 compares cumulative quantities of contamination removed from the aquifer as of April 1, 2005. Calculation methods to estimate the initial volume of contaminated ground water and initial contaminant mass listed in Table 4 are included in Appendix F. The listed initial mass of solute in ground water above remediation standards assumes a geometric average of measured baseline concentrations at numerous monitoring wells, per respective contaminant, in the corresponding estimated volume of contaminated ground water.

By these estimates, at current mass recovery rates of about 2 to 5 percent per year, ground water restoration will require between 20 and 50 years to complete since its inception in mid-2002. The corresponding minimum volume of extracted ground water, assuming constant withdrawal of 85 gpm, is 890-million gallons, approximately equivalent to one estimated pore volume of the contaminant plume.

Contaminant	Initial Mass (Ib) <sup>a</sup>	Cumulative Mass Removed (Ib)	Cumulative Percent Mass Reduction	Initial Volume (gal)ª	Volume Treated (gal)	Percent Plume Volume Reduction
Nitrate	9,500,000	459,000	5	1.2E+09	135,900,000	11
Sulfate	20,150,000	1,123,000	6	1.2E+09	135,900,000	11
Uranium	2,300	325	14	1.2E+09	135,900,000	11

Table 4. Summary of Cumulative Mass and Volume Recovery

<sup>a</sup>Source: see Appendix F

#### 5.3.1 Aquifer Restoration Index

Using a similar approach to that described in the preceding section, but independent of the estimated volume of contaminated ground water, the average concentration of a contaminant, when computed for each sampling event from a selected group of wells provides an additional measure of restoration progress when viewed over time. By this method, the composition of the ground water plume is represented as a single concentration value for a given contaminant at a given time. Figures 28 and 29 illustrate respectively how the geometric mean of the sulfate and uranium concentration for the individual sampling events varies since the baseline period. The selected monitor wells for this analysis are those located throughout the contaminant plume and

sampled most regularly. Appendix G provides calculation information for this performance metric.

Despite the small increment of change and the relatively brief period of observation, the results presented in Figures 28 and 29 suggest a developing trend showing the effects of remediation in reducing the bulk concentration of the uranium and sulfate plume (nitrate results not analyzed). Linear projection of these data predict a total restoration time of 20 years since the inception of active remediation in mid-2002. This compares to an estimated 25 years to remove one pore volume of the initial contaminant plume (Table 4) at the current extraction rate of approximately 4 percent per year.

# 6.0 Special Topics

# 6.1 Concentration Rebound Study

A field study conducted during January 2004 evaluated the extent of contaminant rebound at the extraction wells after a scheduled 9-day maintenance shutdown (DOE 2004a). This was done to determine if contaminant removal could be enhanced by cyclic or "pulsed" pumping of the extraction wells (periods of pumping and non pumping of a given well or group of wells). Test results showed significant concentration rebound at most locations after the wells were idle followed by rapidly decreasing concentrations once pumping resumed. Because the overall benefit was short-lived (< 1 day), effective pulsed pumping would require rapid cycling. The associated operational and maintenance requirements suggest that pulsed pumping is not practical at this time.

# 6.2 Deep Wells

DOE issued a draft report in April 2004 (DOE 2004b) addressing the origin of ground water contamination at wells 251 through 257, installed in May 2000 and comprising the deepest wells at the site (up to 700 ft deep). In September 2000, significant grout accumulation in the bottom of well 253 was discovered. A sudden increase in contaminant concentration also occurred at that time. Previous samplings or well 253 indicated that contaminant concentrations in the screened interval (600 to 700 ft deep) were consistent with background levels. These findings indicated that the annual seal had failed, thus allowing downward migration of contaminants through the well bore, and so the well was soon abandoned.

A similar pattern of apparent well failure and delayed arrival of contamination to the screened interval occurred later at several other deep wells. Further investigation using down-hole video imaging during October 2000 and August 2002 identified grout seeping through the screen slots and accumulations of 10 to 20 feet of grout in the bottom of wells 254 and 256. About 5-ft of grout accumulated in well 256 during this 2-yr period. Fifteen to 20 ft of unidentified foreign material was also observed at the bottom of well 255. Imaging of well 257 was not conducted. Visual inspection of samples collected at well 254 in November 2003 confirmed the material in the bottom of that well to be grout.

In their report, DOE cited these and other lines of evidence in concluding that the apparent contamination of the deep wells is the result of failed annular seals and consequent downward

flow of ground water through the well bore from the shallower contaminated horizons. Ambient downward flow potentials before the start of ground water remediation provided the necessary driving force. Since the start of active remediation, deep vertical flow potentials have reversed to upward at well pair 251/252, and the contamination in the screened interval of well 251 (Horizon E) has decreased to less than the remediation standards. Well 252 (Horizon I) has shown no evidence of contamination at any time.

Vertical flow potentials have also reversed to upward at well pair 256/257 in response to pumping. At well 256 (Horizon I), slightly elevated concentrations of nitrate, sulfate, and uranium have gradually decreased from peak levels in February 2002 such that only nitrate, at 48 mg/L, presently exceeds its restoration standard. As of February 2005, deep well 257 (Horizon M) is contaminated only by sulfate, but concentrations of that constituent continue to rise (see Appendix D, Figures D–13 through D–15 for time-series concentration graphs for the deep wells).

A downward flow potential remains between Horizons I and M at well pair 254/255, but shallower in the aquifer at that location, upward flow is indicated between Horizon I (well 254) and Horizon D (well 273), which should limit downward migration of contamination (see also Section 4.1.4). Both nitrate and sulfate continue to rise at well 254 to now exceed restoration goals by an order of magnitude, while uranium has simultaneously decreased from its peak of 0.21 to 0.09 mg/L between in February 2002 and 2005. As of February 2005, deep well 255 (Horizon M) is contaminated only by sulfate, but concentrations of that constituent continue to rise (see Appendix D). Similar to well 257, sulfate contamination in the absence of other site related constituents, possibly originates from the bentonite grout used to complete the wells.

As per the recommendations in DOE 2004b, proceedings are underway to abandon wells 254, 255, 256, and 257. The abandonment will occur during calendar year 2005. Deep wells 251 and 252 will be retained to maintain at-depth monitoring capability.

# 6.3 Well Field Expansion

Eight ground water extraction wells (wells 1126 to 1133) and 14 monitoring wells (wells 272 to 285) were installed during August and September 2004. The extraction wells will capture contaminated ground water in portions of the contaminant plume on the middle terrace that are currently unaffected by pumping. Based on contaminant concentration data for paired monitoring wells along the escarpment separating the middle and lower terraces (wells 263/264, 265/266, 909/932), the new extraction wells were installed to intercept Horizon B only to thus minimize capture of deeper ground water in this area that is not contaminated. Two of the three primary site contaminants exceed their respective restoration standards at each new extraction well. Preliminary flow rates for the new extraction wells range from about 0.5 to 3 gpm. These rates are not unexpectedly low considering the corresponding screens lengths (30 to 40 ft) are much shorter than those of the previously installed extraction wells (150 ft). The new extraction wells will begin operating in summer 2005.

Data uses for the new monitoring wells include: (1) determine ground water quality and capture in Horizon D in the main area of pumping (new monitor wells 272-276), (2) evaluate the capture zone of the new extraction wells (new monitor wells 281-283), (3) determine vertical flow relationships and water quality on the lower terrace near the greasewood area (new monitor

wells 277-280), and (4) evaluate performance of the infiltration trench (new monitor wells 284 and 285). Data obtained from the new monitoring wells (and the non-operating new extraction wells) are incorporated in previous sections of this report.

## 6.4 Aquifer Isolation Tests

In March and June, 2004, field testing was conducted to evaluate the vertical distribution of contamination in the aquifer using three existing extraction wells. The objective of the tests was to determine if the wells penetrate uncontaminated intervals of the aquifer at depth that do not require capture and treatment. None of the tests recognized a well-defined base of contamination, but interpretation of test results was subject to considerable uncertainty arising from the test methods and field conditions (DOE 2005). Monitoring results for newly installed wells completed in Horizon D (wells 272-276) and mass balance analysis (DOE 2005) suggest that contamination in Horizon D is not pervasive but rather may be a localized occurrence. Currently, there are no plans to modify the existing extraction wells for the purpose of limiting ground water extraction from deeper portions of their screened interval. Additional field investigation of contaminant stratification may be conducted, which could eventually lead to a pumping scheme that focuses on the shallow Horizons A through C.

## 6.5 Geologic Reconnaissance

Field investigation of the Navajo Sandstone was conducted on January 12 to 14, 2005 by project personnel to identify features that might affect hydrogeological conditions at the site. This activity was prompted by depth-dependent water levels in wells and drill holes in the area of the middle terrace near the escarpment. Water levels in shallow wells (< 100 ft) are about 20 to 30 ft higher than the wells 50 to 100 feet deeper in the area. For example, at the location of well 1130, the initial borehole remained open at a depth of about 75 ft for more than one week during which the water level remained at about 60 ft below ground surface. In an adjacent borehole advanced to 125 ft, the static water level was about 90 ft below ground surface. Lithologic contrasts to account for the water level difference were not apparent during drilling. However, the field reconnaissance and additional review of project well logs tentatively identified a depositional bounding surface, possibly of low permeability, in this depth interval. Such a feature, acting locally either as a leaky aquitard or aquiclude could account in part for the locally strong downward flow gradient. The low permeability interval, and perhaps similar others, may also explain decreasing contaminant concentrations with depth across Horizons A through D.

# 7.0 Year in Review Summary

- On-stream extraction and treatment flow rates meet design objectives.
- Distillate quality meets or exceeds design objectives.
- Return flow to the aquifer as a percentage of extracted water meets design objectives.

- The current configuration and operation of the extraction system effectively captures the region of maximum ground water contamination.
- The current configuration and operation of the extraction system likely captures the full vertical extent of ground water contamination.
- Plume expansion is not significant on either the middle or lower terrace.
- Uranium concentrations have decreased to less than the restoration standard at all lower terrace monitoring locations.
- New extraction wells installed in 2004 will extend the capture zone to include regions of contamination on the middle terrace currently not captured.
- Developing bulk concentration trends indicate measurable progress in contaminant mass removal from the aquifer.

# 8.0 Recommendations

- Reduce ground water monitoring (except that conducted for treatment plant operations) to one annual event.
- Continue ground water extraction, treatment, and infiltration as currently conducted, with the addition of the new extraction wells to become operational in summer 2005.

# 9.0 References

Cooley, M.E., J.W. Harshbarger, J.P. Akers, and W.F. Hardt, 1969. *Regional Hydrogeology of the Navajo and Hopi Indian Reservations, Arizona, New Mexico and Utah*, U.S. Geological Survey Professional Paper 521-A.

U. S. Department of Energy (DOE), 1999. *Phase I Ground Water Compliance Action Plan for the Tuba City, Arizona, UMTRA Site*, GJO–99–99–TAR. U. S. Department of Energy Grand Junction Office, Grand Junction, Colorado, June.

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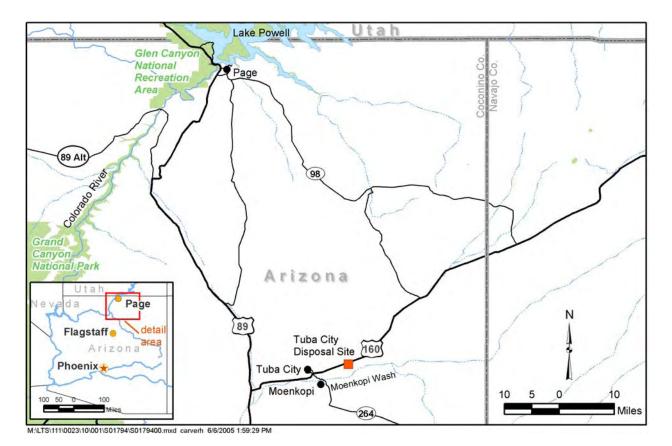


Figure 1. Tuba City Site Location

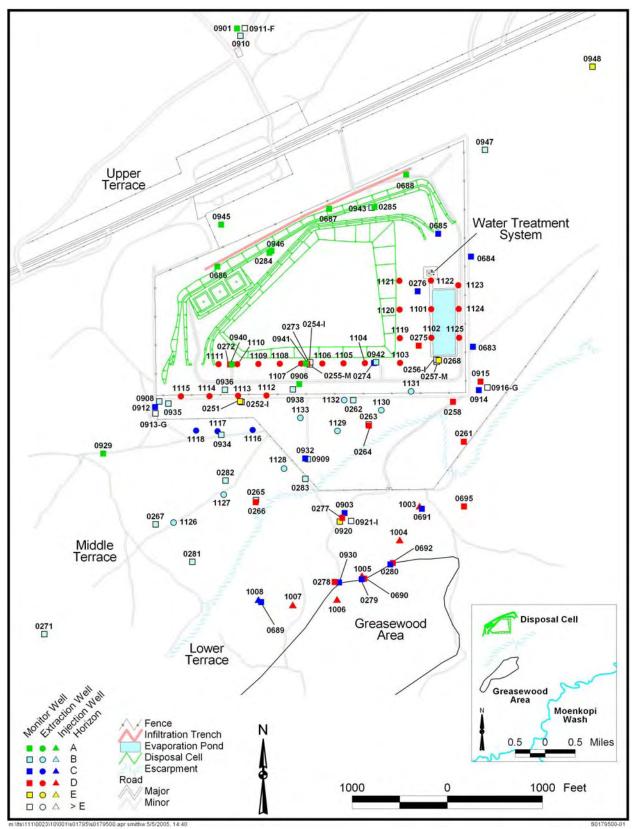


Figure 2. Tuba City Site Features and Well Locations

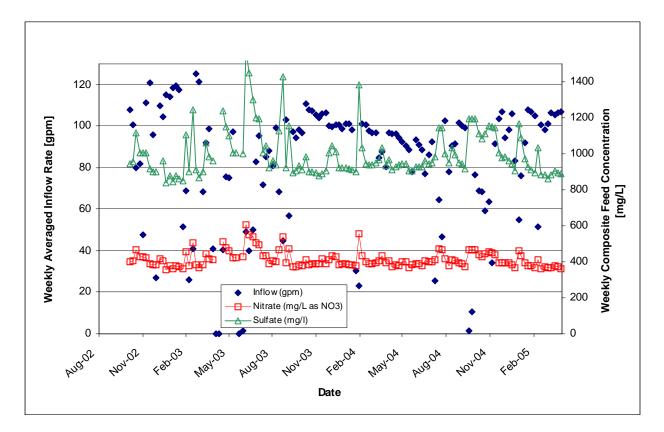


Figure 3. Treatment Plant Inflow Rate and Nitrate and Sulfate Concentration

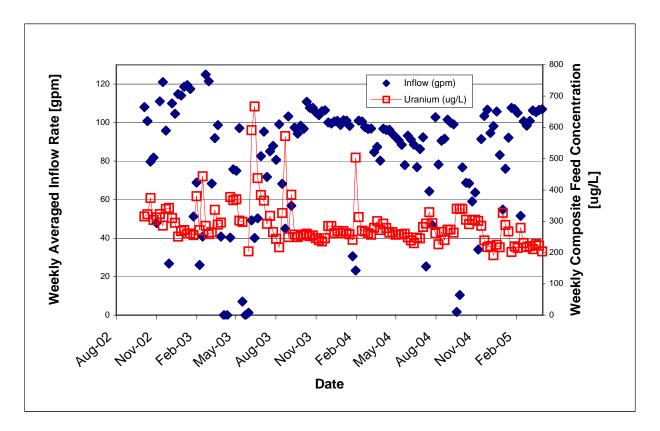


Figure 4. Treatment Plant Inflow Rate and Uranium Concentration

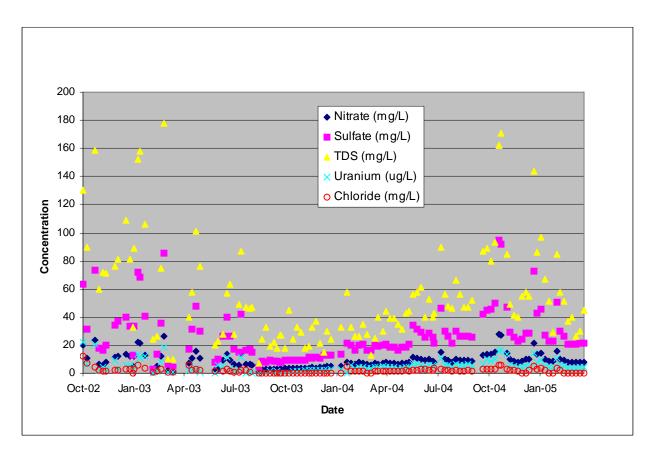


Figure 5. Treatment Plant Distillate Quality

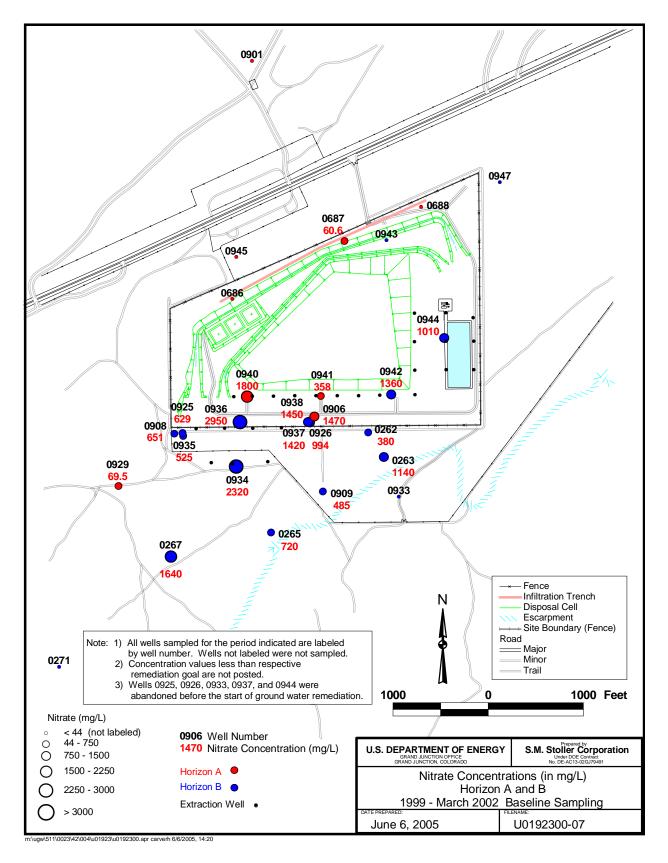


Figure 6a. Nitrate Concentrations in Ground Water, Horizons A and B, Baseline Period

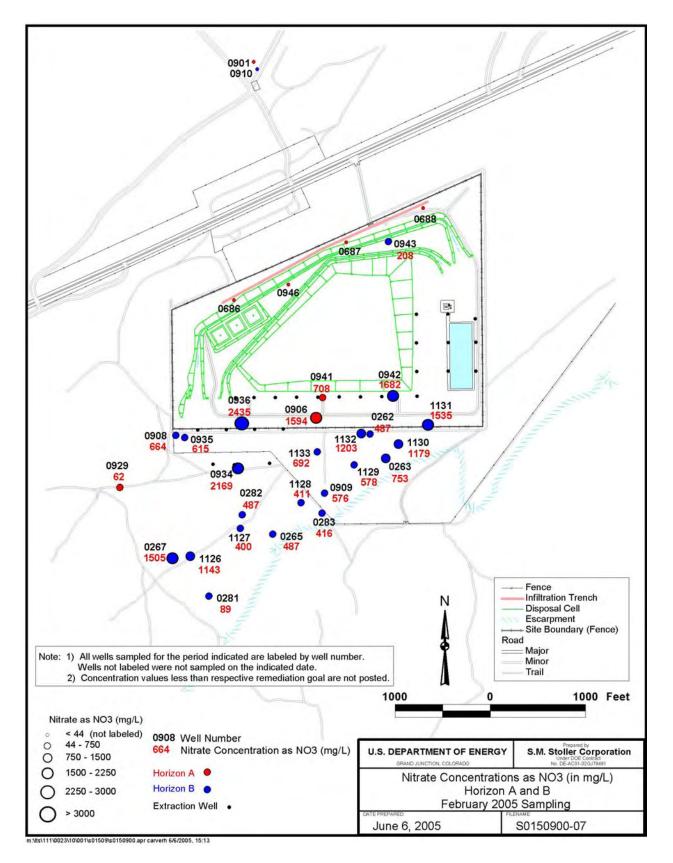


Figure 6b. Nitrate Concentrations in Ground Water, Horizons A and B, February 2005

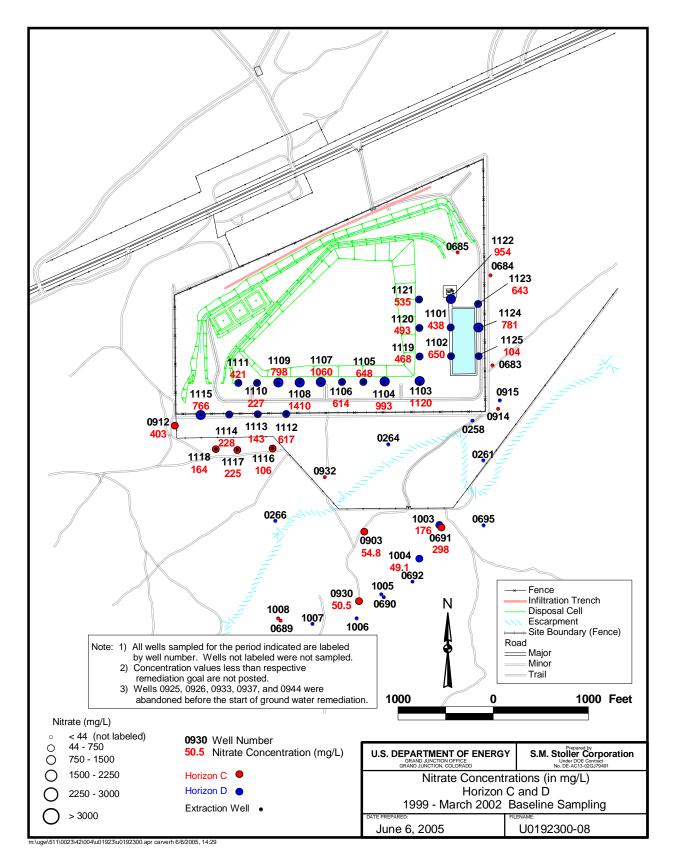


Figure 7a. Nitrate Concentrations in Ground Water, Horizons C and D, Baseline Period

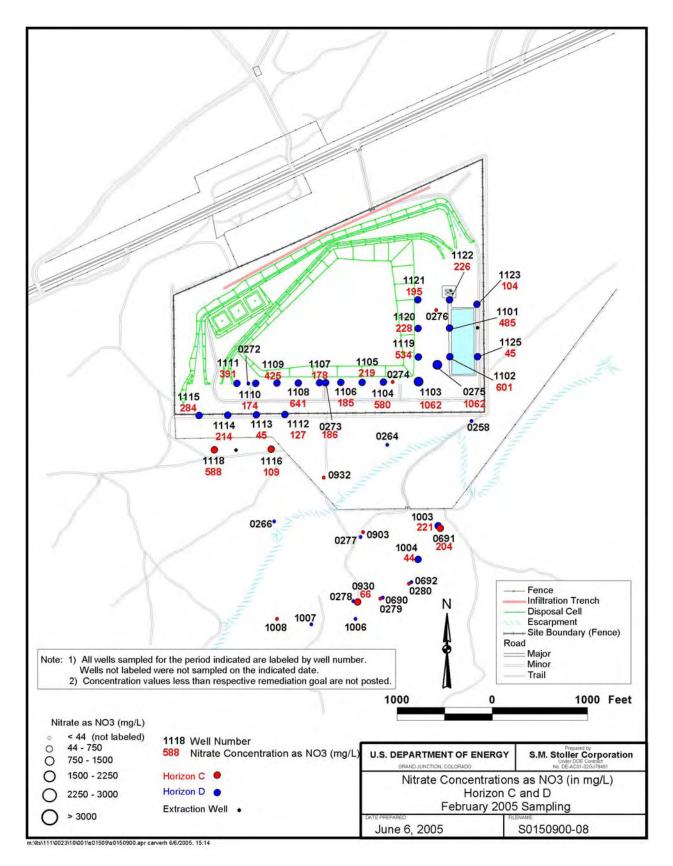


Figure 7b. Nitrate Concentrations in Ground Water, Horizons C and D, February 2005

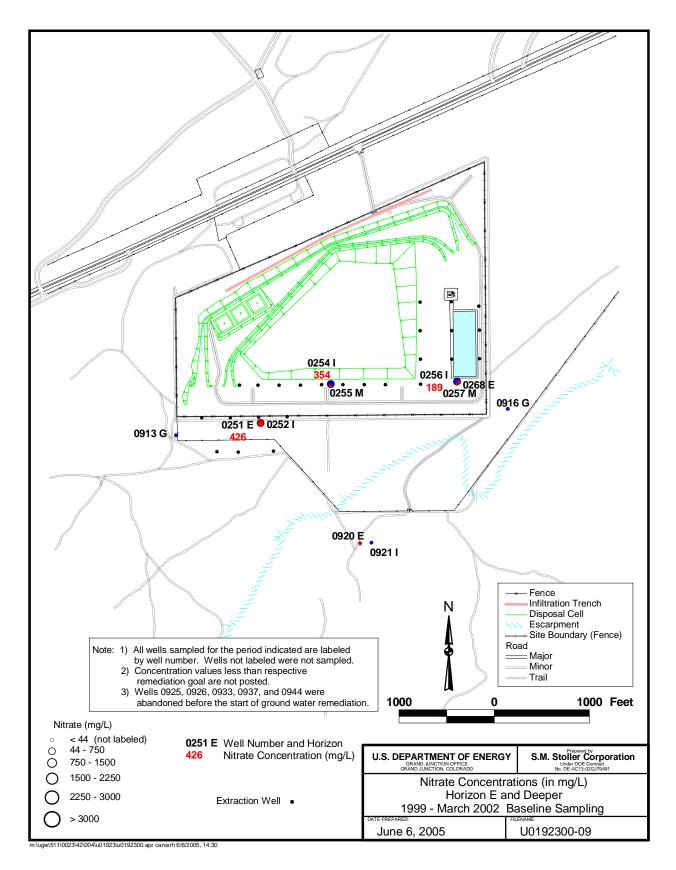


Figure 8a. Nitrate Concentrations in Ground Water, Horizons E and Deeper, Baseline Period

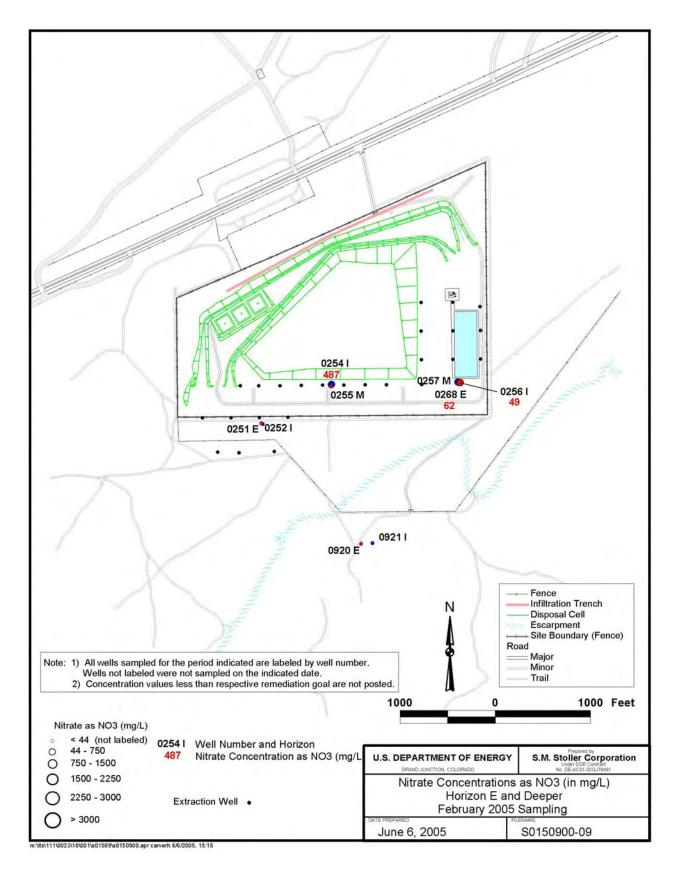


Figure 8b. Nitrate Concentrations in Ground Water, Horizons E and Deeper, February 2005

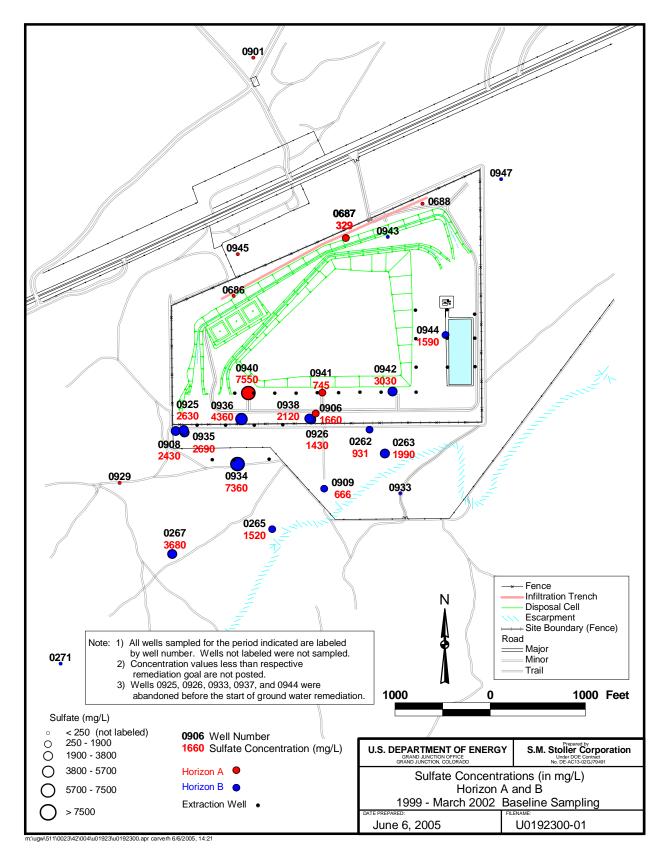


Figure 9a. Sulfate Concentrations in Ground Water, Horizons A and B, Baseline Period

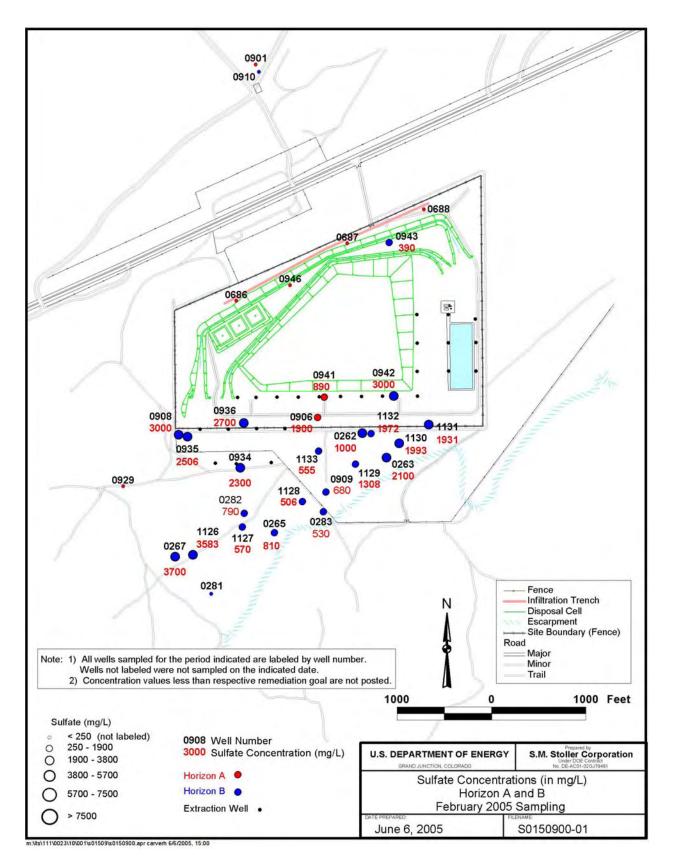


Figure 9b. Sulfate Concentrations in Ground Water, Horizons A and B, February 2005

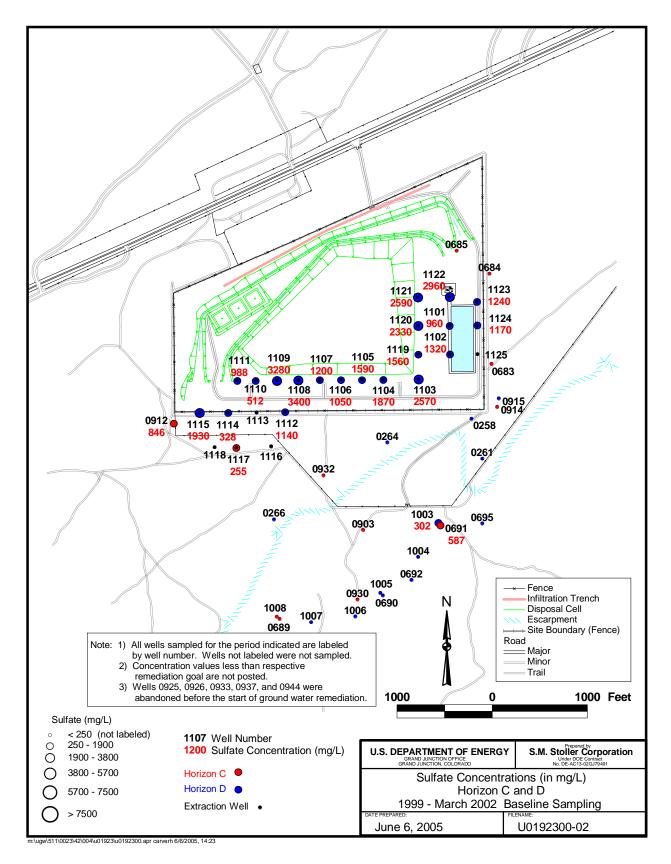


Figure 10a. Sulfate Concentrations in Ground Water, Horizons C and D, Baseline Period

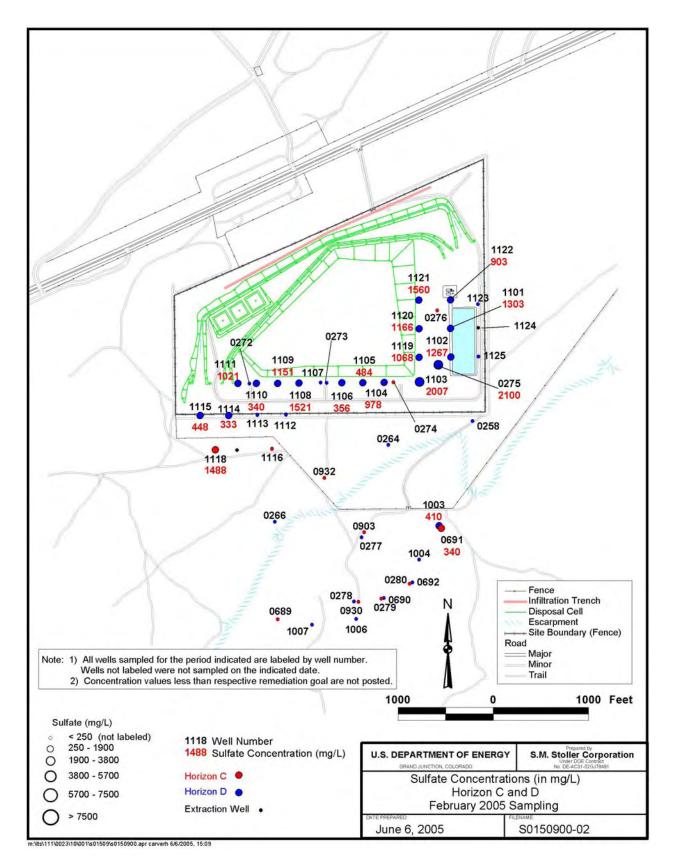


Figure 10b. Sulfate Concentrations in Ground Water, Horizons C and D, February 2005

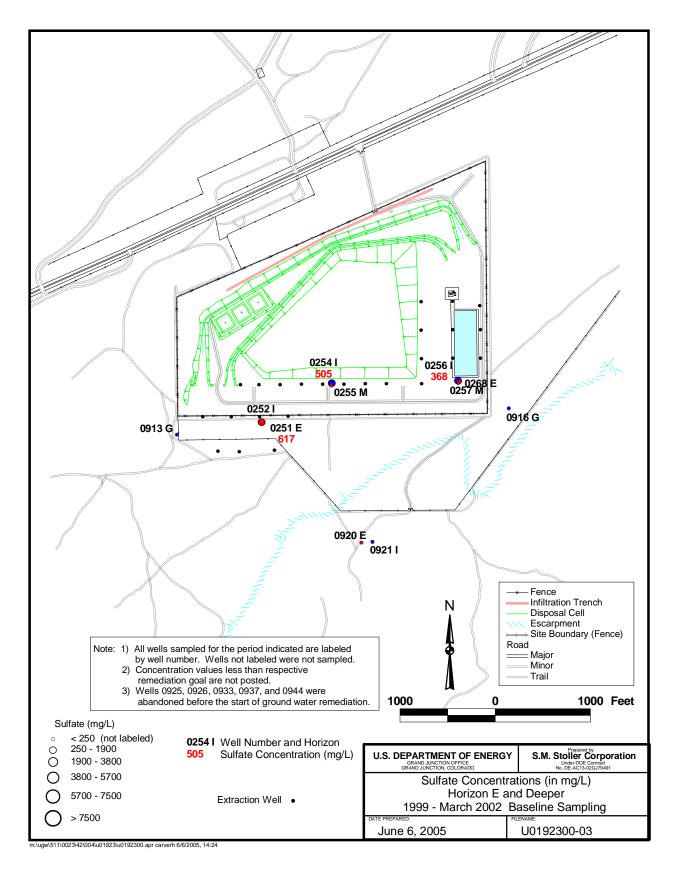


Figure 11a. Sulfate Concentrations in Ground Water, Horizons E and Deeper, Baseline Period

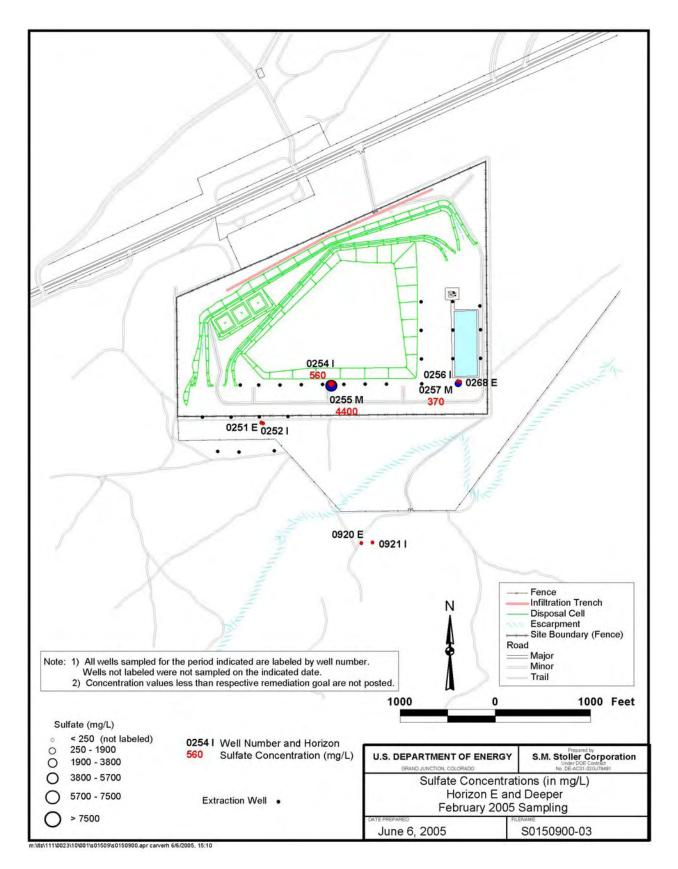


Figure 11b. Sulfate Concentrations in Ground Water, Horizons E and Deeper, February 2005

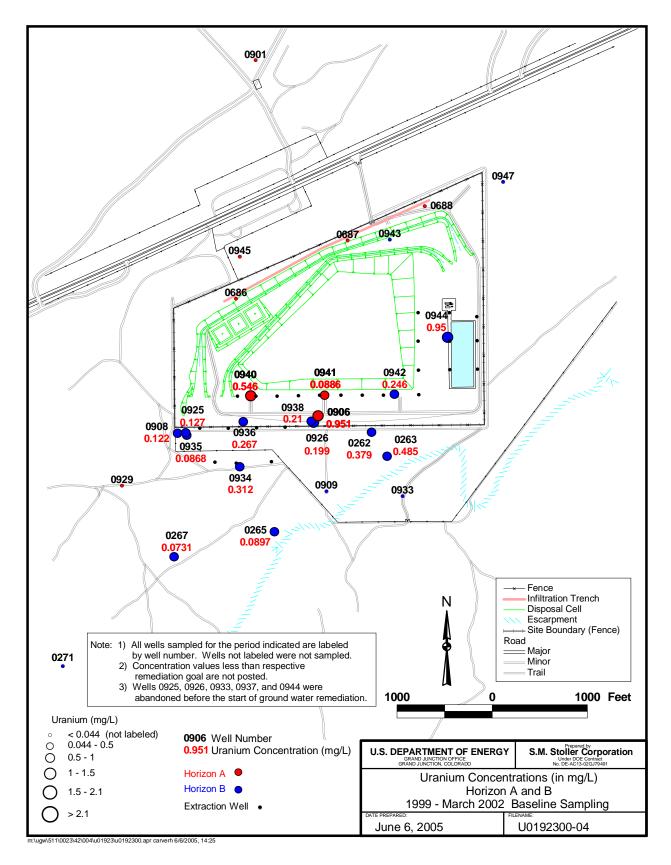


Figure 12a. Uranium Concentrations in Ground Water, Horizons A and B, Baseline Period

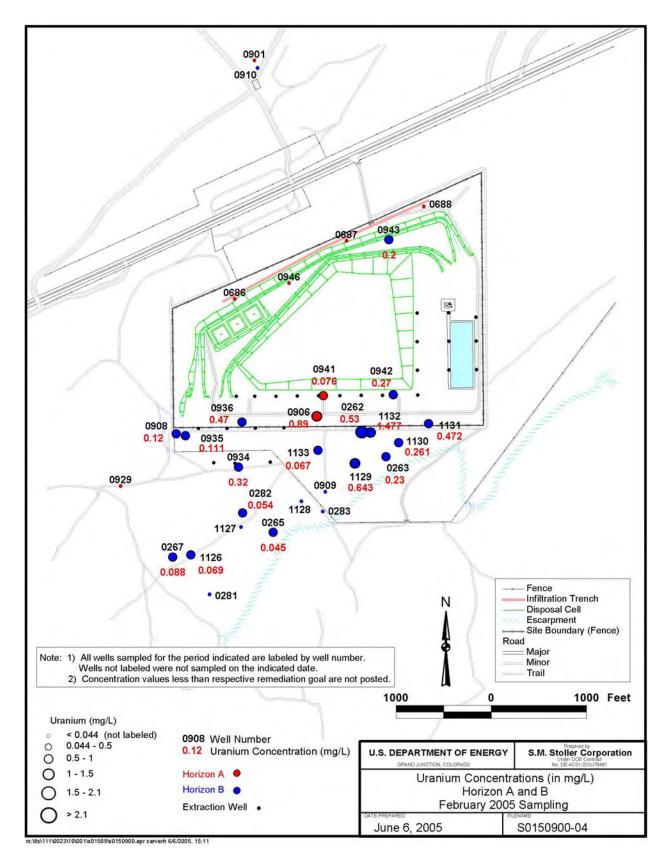


Figure 12b. Uranium Concentrations in Ground Water, Horizons A and B, February 2005

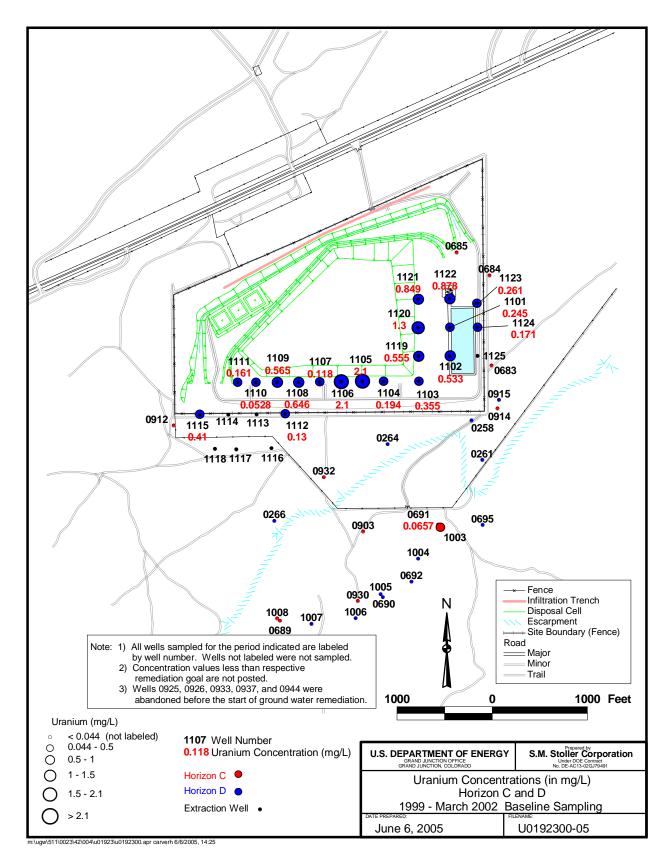


Figure 13a. Uranium Concentrations in Ground Water, Horizons C and D, Baseline

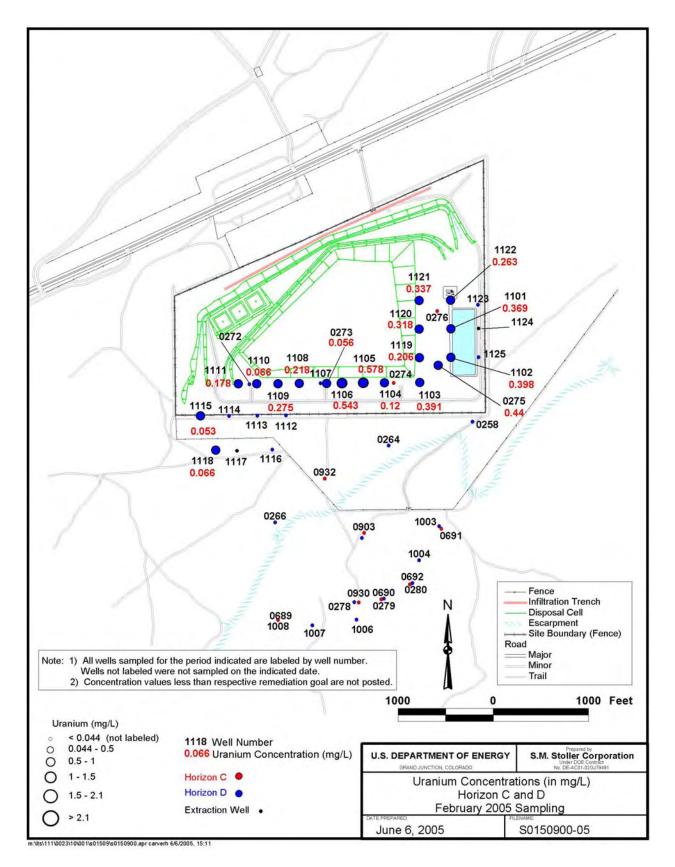


Figure 13b. Uranium Concentrations in Ground Water, Horizons C and D, February 2005

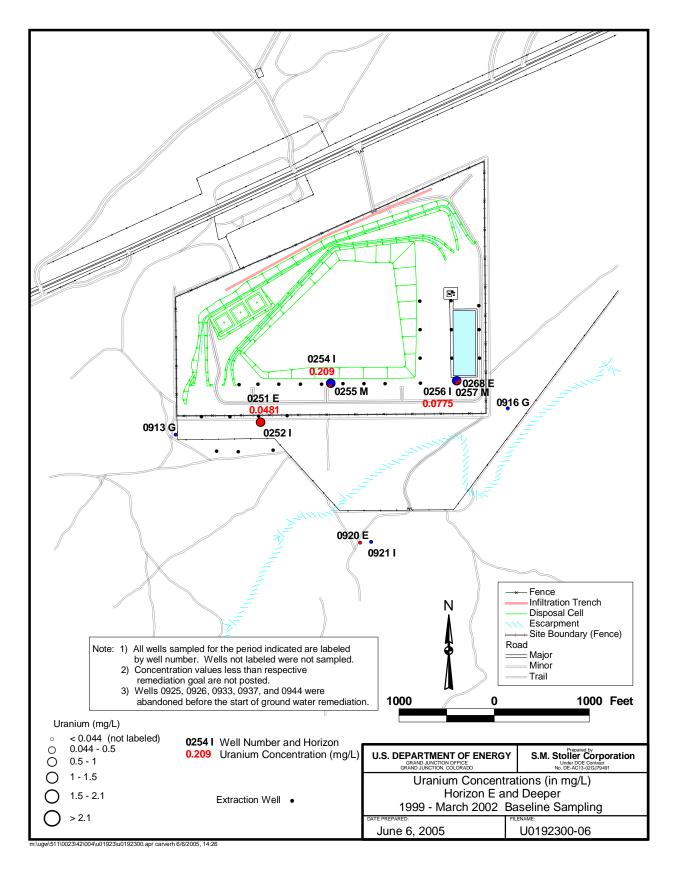


Figure 14a. Uranium Concentrations in Ground Water, Horizons E and Deeper, Baseline Period

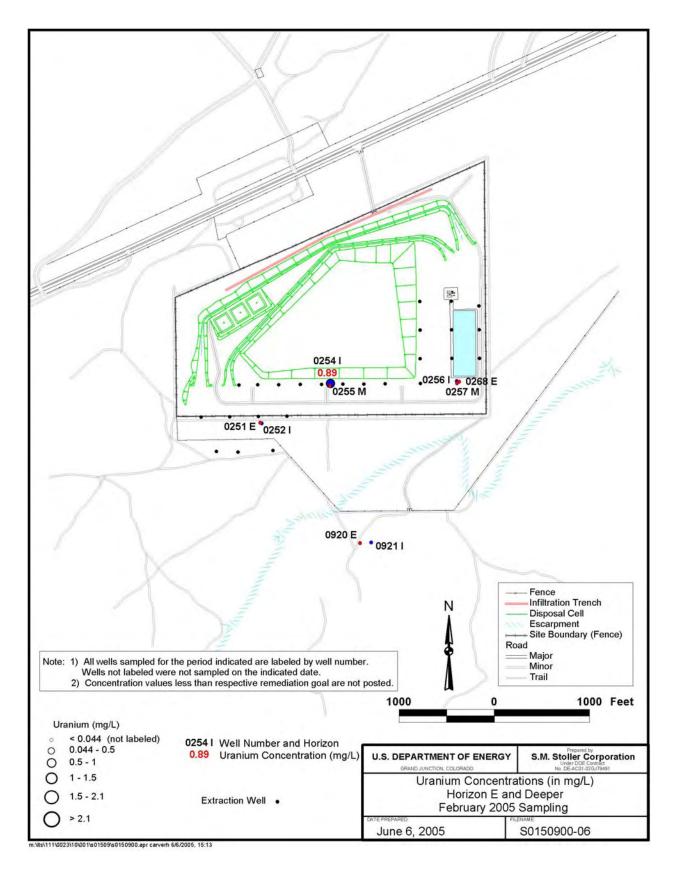


Figure 14b. Uranium Concentrations in Ground Water, Horizons E and Deeper, February 2005

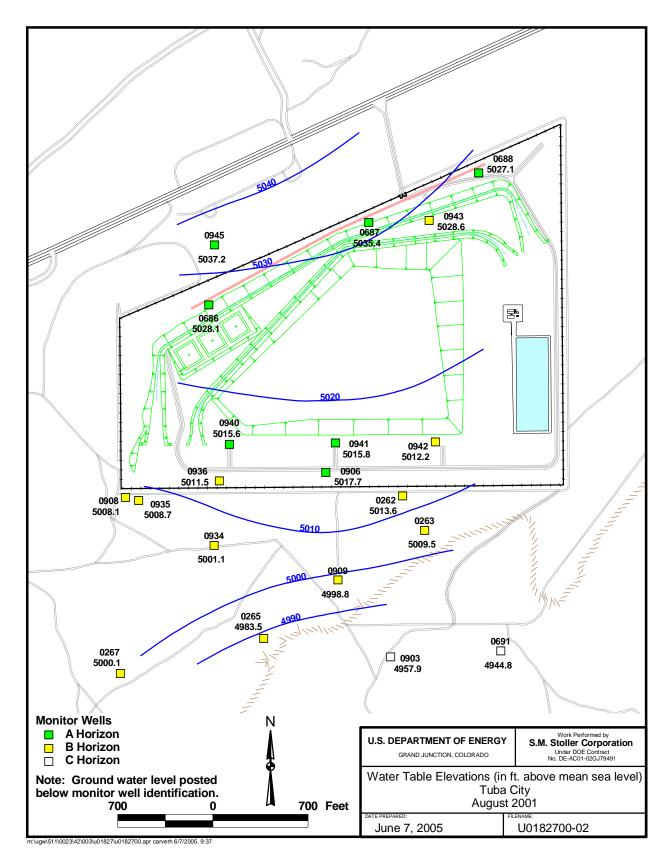


Figure 15. Water Table Elevations (in ft. above mean sea level), Tuba City Site, August 2001

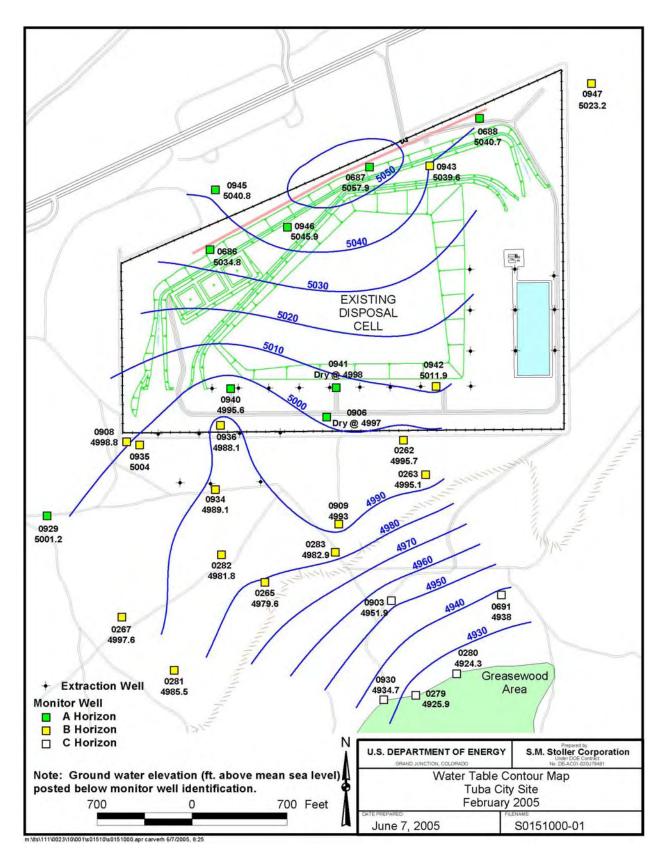


Figure 16. Water Table Contour Map, Tuba City Site, February 2005

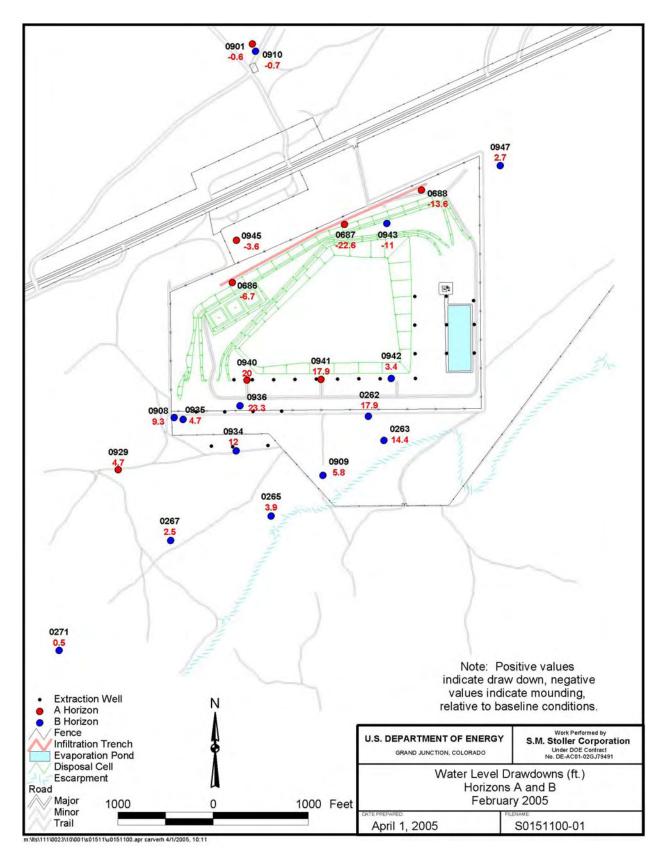


Figure 17. Water Level Drawdowns (ft), Horizons A and B, February 2005

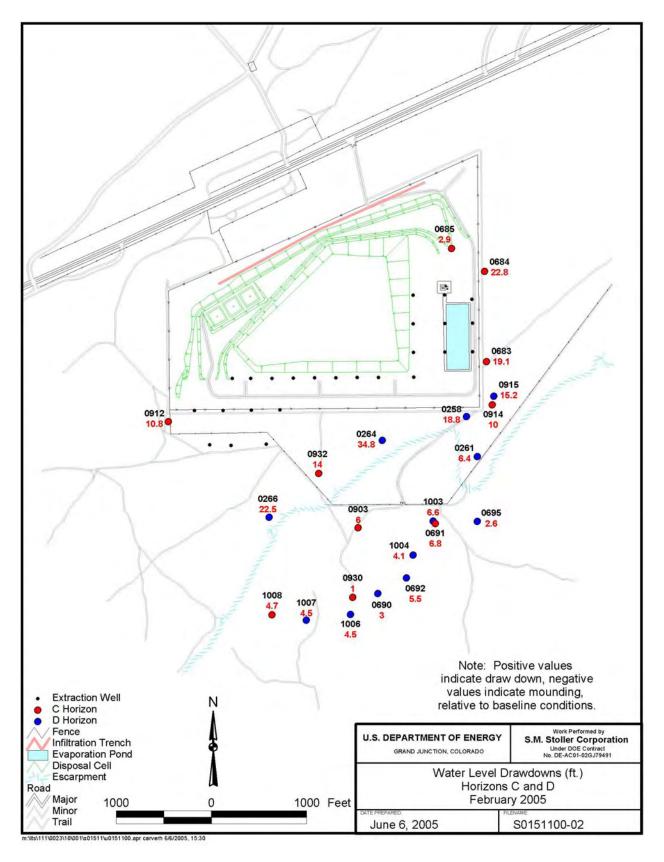


Figure 18. Water Level Drawdowns (ft), Horizons C and D, February 2005

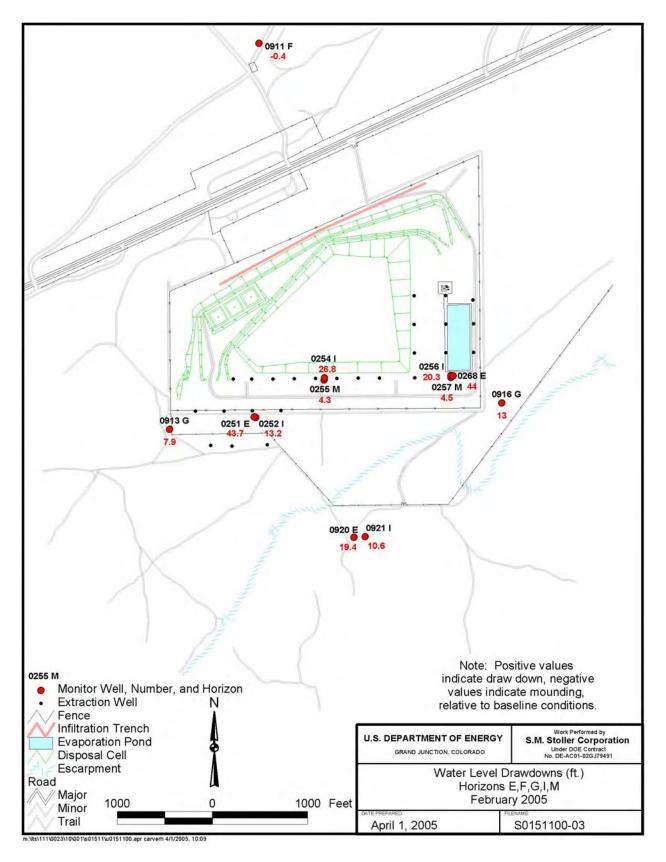
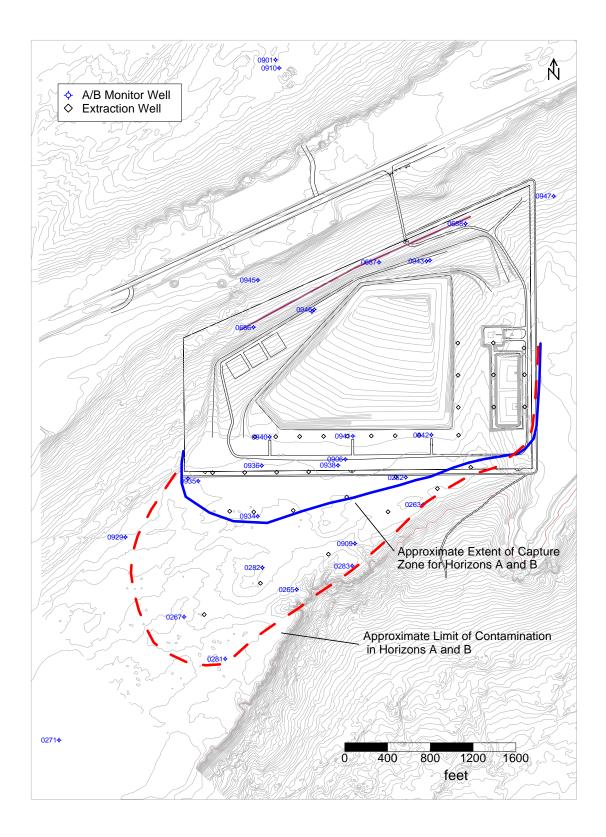


Figure 19. Water Level Drawdowns (ft), Horizons E, F, G, I, and M, February 2005



#### Figure 20. Extent of Ground Water Contamination and Extraction System Capture Zone: Horizons A and B

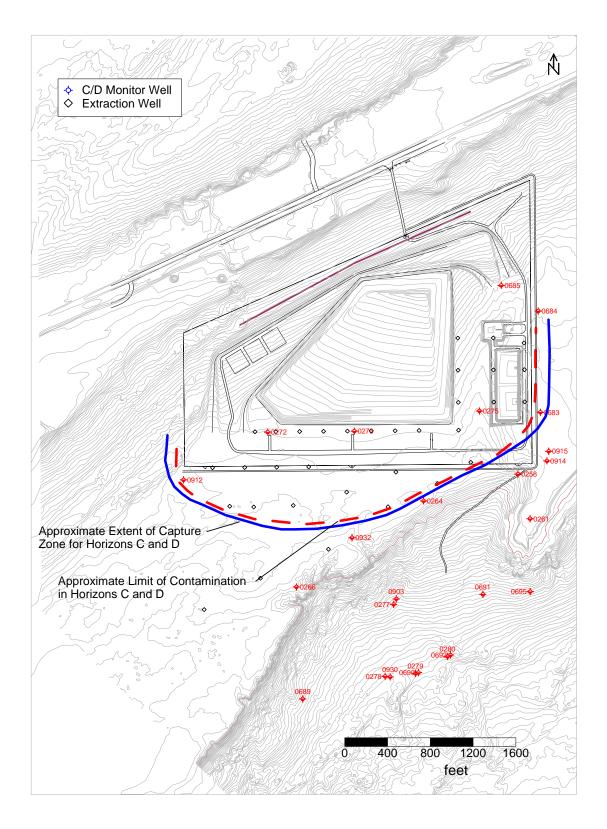
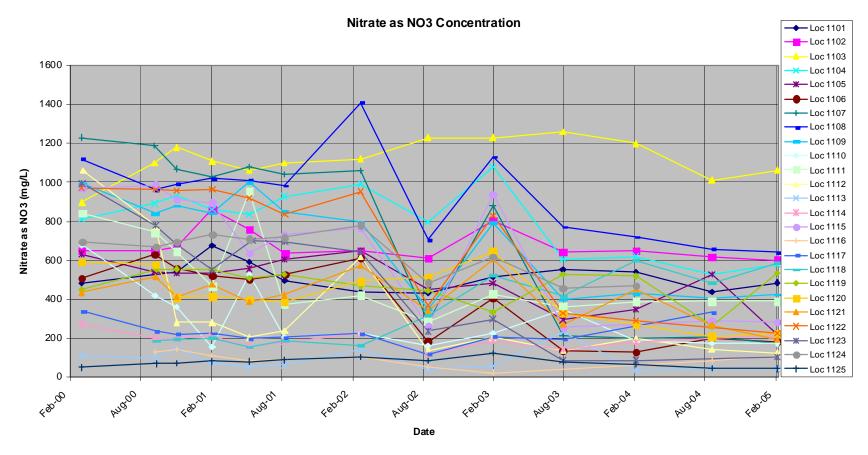


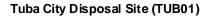
Figure 21. Extent of Ground Water Contamination and Extraction System Capture Zone: Horizons C and D





Tuba City Disposal Site (TUB01)

Figure 22. Nitrate Concentration Trends at Extraction Wells



**Sulfate Concentration** 

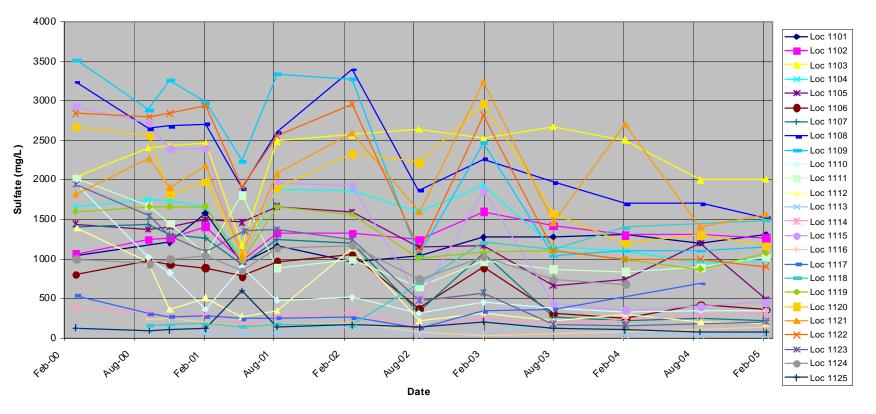


Figure 23. Sulfate Concentration Trends at Extraction Wells

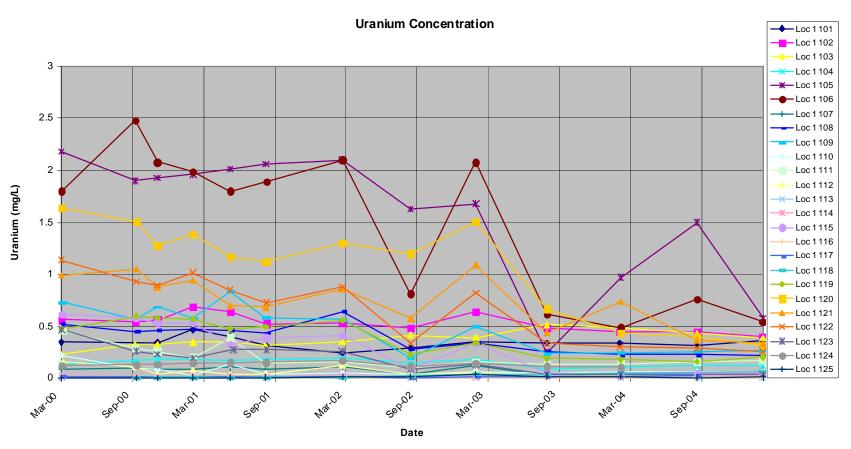
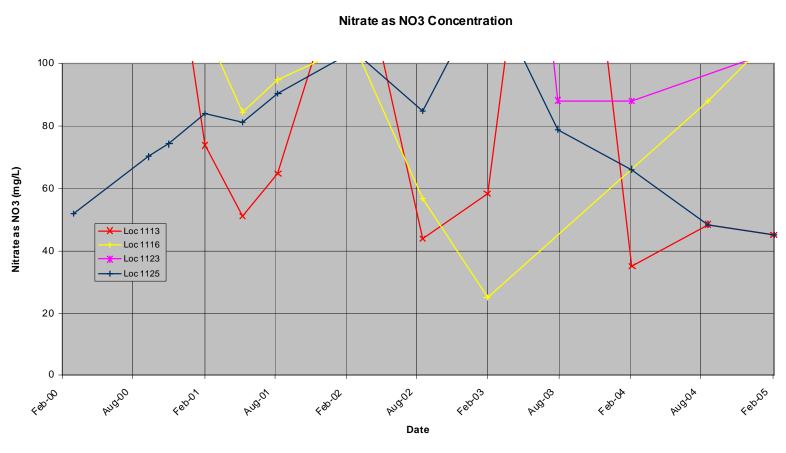


Figure 24. Uranium Concentration Trends at Extraction Wells





Tuba City Disposal Site (TUB01)

Figure 25. Nitrate Concentrations Trends Near Remediation Standard (44 mg/L as NO<sub>3</sub>) at Extraction Wells



#### → Loc 1113 500 X **⊖**−Loc 1125 450 ▲ Loc 1112 400 - Loc 1123 Loc 1103 350 Loc 1114 4 Loc 1117 Loc 1118 Sulfate (mg/L) 300 盔 250 200 150 100 50 0 AUGOZ 4<sup>89:03</sup> AUGO3 480.00 AUG:00 480.01 AUGOT 5-80-02 Feblok AUGOA 480.00 Date

Figure 26. Sulfate Concentrations Trends Near Remediation Standard (250 mg/L) at Extraction Wells

Tuba City Disposal Site (TUB01)

Sulfate Concentration



#### 0.1 - Loc 1101 - Loc 1110 Б ▲ Loc 1112 80.0 **—** Loc 1123 - Loc 1113 **\*** Loc 1114 Loc 1117 Uranium (mg/L) 0.06 Loc 1125 Δ ୬ 0.04 0.02 0 AUGOT fepas AUGIOS 580.00 AUGOO 480.01 580.02 AUGOL Feblat AUGOA feb.05 Date

Tuba City Disposal Site (TUB01)

Uranium Concentration

Figure 27. Uranium Concentrations Trends Near Remediation Standard (0.044 mg/L) at Extraction Wells

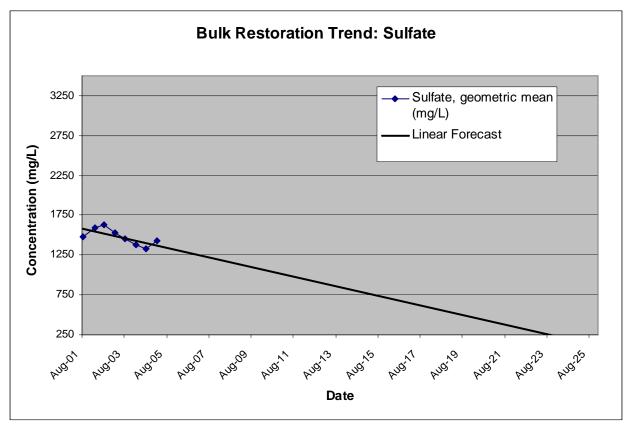


Figure 28. Bulk Restoration Trend for Sulfate

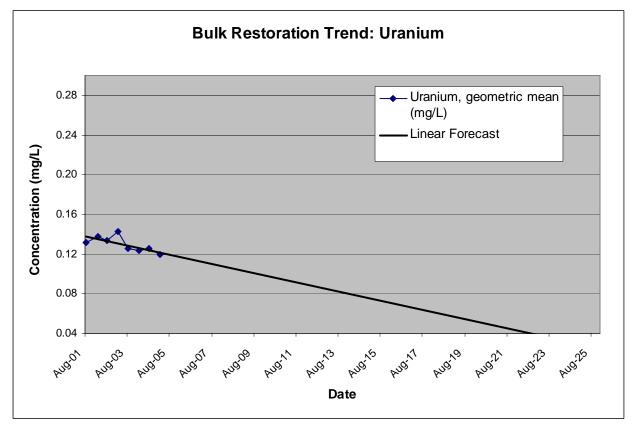


Figure 29. Bulk Restoration Trend for Uranium

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# Appendix A

Tuba City Project Well Data

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### Table A-1. Well Completion Information

			TOP OF	MID SCREEN	BOTTOM OF	TOP OF SCREEN	MID SCREEN	BOTTOM OF	SCREEN	SUMP	WELL
WELL	TYPE	Horizon	SCREEN ELEV	ELEV	SCREEN ELEV	DEPTH	DEPTH	SCREEN DEPTH	LENGTH	LENGTH	DEPTH
0284		A	5079.8	5074.8	5069.8	16.5	21.5	26.5	10.0	1.5	28.0
0285	MW	A	5090.8	5088.3	5085.8	3.0	5.5	8.0	5.0	0.1	8.1
0686		A	5045.5	5025.5	5005.5	60.0	80.0	100.0	40.0	0.1	100.3
0687	MW	A	5047.6	5025.5	5005.5	60.0	80.0	100.0	40.0	0.3	100.3
0688	MW	A	5044.1	5024.1	5004.1	60.0	80.0	100.0	40.0	0.3	100.3
0000	MW	A	5045.8	5035.8	5025.8	58.0	68.0	78.0	20.0	2.0	80.0
						44.0			20.0		
0906	MW	A	5016.9	5006.9	4996.9		54.0	64.0		2.0	66.0
0907	MW	A	5010.7	5000.7	4990.7	66.5	76.5	86.5	20.0		
0928	MW	A	5022.1	5009.6	4997.1	30.0	42.5	55.0	25.0	3.0	58.0
0929	MW	A	5010.4	4990.4	4970.4	48.2	68.2	88.2	40.0		
0940	MW	A	5017.9	5010.4	5002.9	45.0	52.5	60.0	15.0	3.0	68.0
0941	MW	A	5018.0	5008.0	4998.0	45.0	55.0	65.0	20.0	3.0	68.0
0945	MW	A	5028.1	5018.1	5008.1	110.0	120.0	130.0	20.0	3.0	133.0
0946	MW	A	5057.6	5047.6	5037.6	40.0	50.0	60.0	20.0	3.3	63.3
0262	MW	В	4999.2	4979.2	4959.2	60.0	80.0	100.0	40.0	0.3	100.3
0263	MW	В	5000.2	4980.2	4960.2	60.0	80.0	100.0	40.0	0.3	100.3
0265	MW	В	4991.1	4971.1	4951.1	60.0	80.0	100.0	40.0	0.3	100.3
0267	MW	В	4990.8	4970.8	4950.8	60.0	80.0	100.0	40.0	0.3	100.3
0271	MW	В	4984.0	4964.0	4944.0	60.0	80.0	100.0	40.0	0.3	100.3
0281	MW	B	4977.8	4972.8	4967.8	70.5	75.5	80.5	10.0	1.5	82.0
0282	MW	B	4983.3	4978.3	4973.3	74.1	79.1	84.1	10.0	1.5	85.6
0283	MW	B	4984.8	4979.8	4974.8	70.5	75.5	80.5	10.0	1.5	82.0
0205	MW	B	5006.0	4998.5	4991.0	63.0	70.5	78.0	15.0	2.0	80.0
0908	MW	B	5005.3	4997.8	4990.3	52.0	59.5	67.0	15.0	2.0	69.0
0908	MW	B	4990.8	4983.3	4990.3	52.0 65.0	72.5	80.0	15.0	2.0	82.0
0909	MW	B	4990.8 5007.6	4983.3 4957.6	4975.8	97.0	147.0	197.0	100.0	2.0	198.0
0918	MW	B	4986.2	4983.7	4981.2	61.0	63.5	66.0	5.0	2.0	68.0
0925	EXT	B	5005.8	4985.8	4965.8	53.0	73.0	93.0	40.0	0.5	93.5
0926	EXT	B	5018.3	4993.3	4968.3	42.2	67.2	92.2	50.0	3.0	95.2
0933	MW	В	4993.3	4992.3	4991.3	23.0	24.0	25.0	2.0		
0934	MW	В	5013.0	4990.5	4968.0	45.0	67.5	90.0	45.0	3.0	93.0
0935	MW	В	5008.8	4988.8	4968.8	50.0	70.0	90.0	40.0	3.0	93.0
0936	MW	В	5017.9	4997.9	4977.9	42.0	62.0	82.0	40.0	3.0	85.0
0937	MW	В	5020.2	4992.7	4965.2	40.0	67.5	95.0	55.0	3.0	98.0
0938	MW	В	5020.4	4992.9	4965.4	40.0	67.5	95.0	55.0	3.0	98.0
0939	EXT	В	5021.1	4993.6	4966.1	40.0	67.5	95.0	55.0	3.0	98.0
0942	MW	В	5009.5	4999.5	4989.5	54.0	64.0	74.0	20.0	3.0	77.0
0943	MW	В	4994.1	4984.1	4974.1	101.0	111.0	121.0	20.0	3.0	124.0
0944	MW	В	4979.9	4969.9	4959.9	85.0	95.0	105.0	20.0	2.0	107.0
0947	MW	В	4990.0	4980.0	4970.0	105.0	115.0	125.0	20.0	3.3	128.3
1126	EXT	В	4991.9	4971.9	4951.9	60.0	80.0	100.0	40.0	3.3	103.3
1127	EXT	В	4984.2	4964.2	4944.2	72.7	92.7	112.7	40.0	3.3	116.0
1128	EXT	В	4982.3	4962.3	4942.3	72.7	92.7	112.7	40.0	3.3	116.0
1129	EXT	B	4990.9	4975.9	4960.9	68.2	83.2	98.2	30.0	3.3	101.5
1120	EXT	B	4987.3	4962.3	4937.3	71.7	96.7	121.7	50.0	3.3	125.0
1130	EXT	B	4987.3	4902.3	4957.5	59.7	79.7	99.7	40.0	3.3	123.0
1132	EXT	B	5009.1	4978.1	4958.1	49.7	74.7	99.7	50.0	3.3	103.0
1132	EXT	B	4999.4	4984.1	4959.1	49.7 59.7	74.7	99.7	40.0	3.3	103.0
0274		ь С					159.0		20.0		
	MW		4913.6	4903.6	4893.6	149.0		169.0		1.5	170.5
0276	MW	C	4910.0	4900.0	4890.0	154.5	164.5	174.5	20.0	1.5	176.0
0279	MW	C	4922.1	4917.1	4912.1	26.5	31.5	36.5	10.0	1.5	38.0
0280	MW	C	4922.6	4917.6	4912.6	26.5	31.5	36.5	10.0	1.5	38.0
0683	MW	С	4973.2	4948.2	4923.2	95.0	120.0	145.0	50.0	3.0	148.0
0684	MW	С	4943.1	4917.4	4891.8	124.2	149.9	175.5	51.3	2.5	178.0
0685	MW	С	4975.6	4949.7	4923.8	93.7	119.6	145.5	51.8	2.5	148.0
0689		С	4923.9	4903.9	4883.9	55.0	75.0	95.0	40.0	0.3	95.3
0691	MW	С	4921.9	4901.9	4881.9	55.0	75.0	95.0	40.0	0.3	95.3
0903	MW	С	4953.5	4943.5	4933.5	28.0	38.0	48.0	20.0	2.0	50.0
0912	MW	С	4934.7	4914.7	4894.7	123.0	143.0	163.0	40.0	2.0	165.0
0914	MW	С	4930.3	4921.8	4913.3	137.2	145.7	154.2	17.0	2.0	156.2
0917	MW	С	4917.8	4907.8	4897.8	128.0	138.0	148.0	20.0	2.0	150.0
0930	MW	C	4933.0	4918.0	4903.0	20.0	35.0	50.0	30.0	3.0	53.0
0932		C	4942.3	4932.3	4922.3	112.5	122.5	132.5	20.0	2.7	135.2
1008	INJ	C	4926.8	4901.6	4876.4	55.6	80.8	106.0	50.4	2.5	108.5
1116	EXT	C	4964.1	4912.5	4861.0	92.4	143.9	195.5	103.1	2.5	198.0
1117		C	4965.3	4912.3	4862.1	92.3	143.9	195.5	103.1	2.5	198.0
	EXT										
1110		C	4967.9	4915.1	4862.3	89.9	142.7	195.5	105.6	2.5	198.0
1118 0258	MW	D	4894.0	4874.0	4854.0	159.0	179.0	199.0	40.0	0.3	199.3

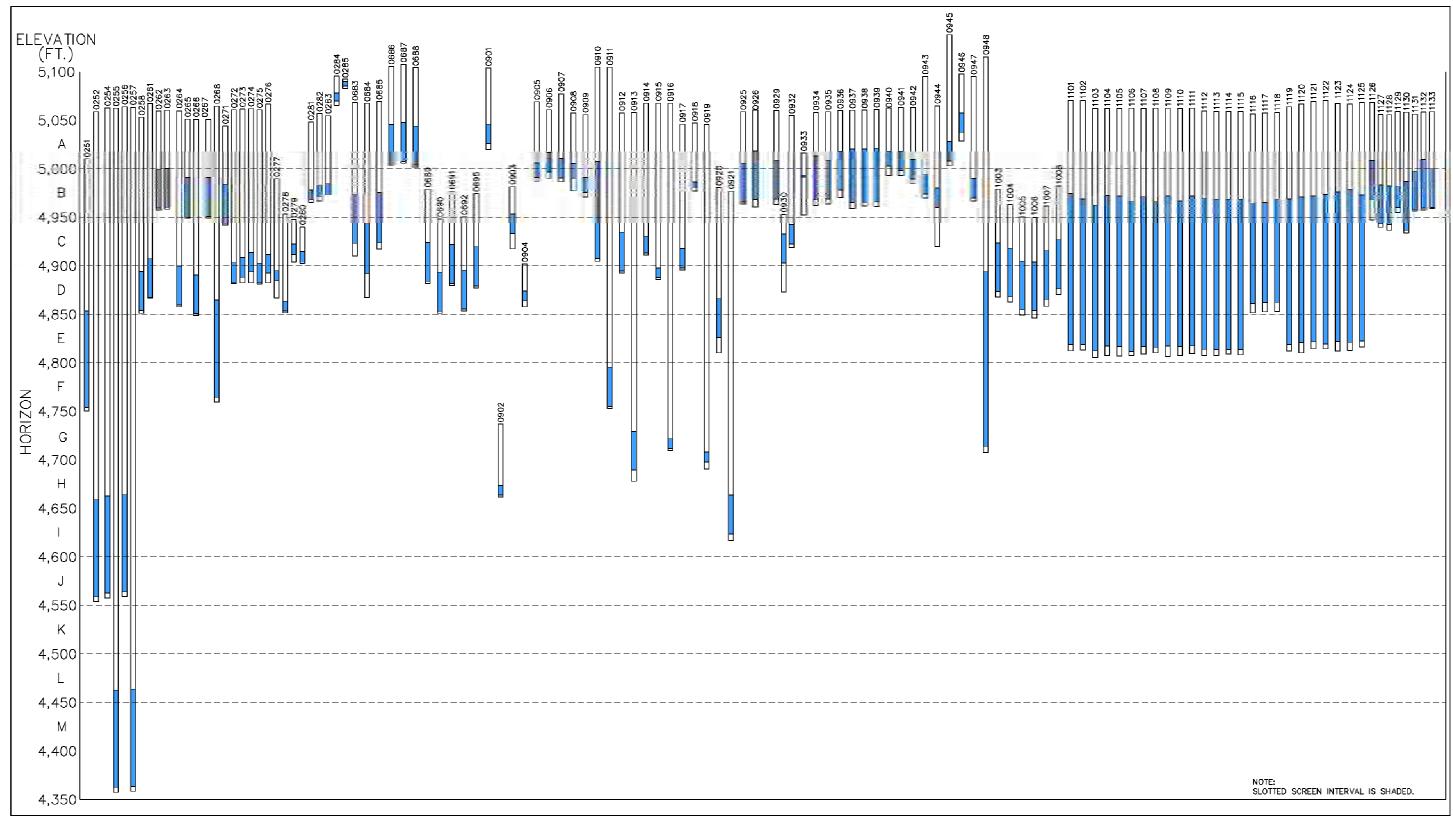
## Table A-1 (continued). Well Completion Information

			TOP OF CASING	GROUND	WELL	BORING	DECOMMISSION	STATE PLANE	STATE PLANE
WELL	TYPE	Horizon	ELEV	ELEV	DIAMETER	STARTED	DATE	EAST	NORTH
0284	MW	A	5098.72	5096.3	2	16-Aug-04		730525	1873562
0285	MW	A	5096.47	5093.8	2	16-Aug-04		731629	1874042
0686	MW	A	5107.97	5105.5	2	28-Mar-00		729978	187341
0687	MW	A	5109.82	5107.6	2	29-Mar-00		731152	187402
)688	MW	A	5106.98	5104.1	2	29-Mar-00		731961	187438
0000	MW	A	5105.46	5103.8	2	16-Oct-84		730185	187591
0906	MW	A	5062.10	5060.9	2	19-Nov-84	(0.1	730838	187218
0907	MW	A	5079.17	5077.2	2	30-Nov-84	19-Apr-88	731252	187292
0928	MW	A	5053.99	5052.1	4	20-Oct-95	24-May-00	729401	1870814
0929	MW	A	5060.82	5058.6	4			728780	1871453
0940	MW	A	5064.77	5062.9	4	01-Nov-95		730130	187239 <sup>-</sup>
0941	MW	A	5065.97	5063.0	4	10-Nov-95		730908	1872398
0945	MW	A	5140.49	5138.1	4	11-Oct-95		730019	187385
0946	MW	A	5100.50	5097.6	4	02-Nov-95		730547	1873582
0262	MW	В	5061.99	5059.2	2	03-Apr-00		731402	1872012
0263	MW	B	5063.10	5060.2	2	04-Apr-00		731565	187175
		1 1							
0265	MW	В	5053.88	5051.1	2	16-Apr-00		730382	1870964
0267	MW	В	5053.40	5050.8	2	14-Apr-00		729329	187070
0271	MW	В	5046.72	5044.0	2	29-Apr-00		728160	1869555
0281	MW	В	5051.00	5048.3	2	11-Aug-04		729714	1870315
0282	MW	В	5060.04	5057.4	2	10-Aug-04		730062	1871168
0283	MW	В	5057.97	5055.3	2	03-Aug-04		730901	187118
0905	MW	В	5072.80	5069.0	2	14-Nov-84	24-May-00	732933	1873200
0908	MW	В	5058.14	5057.3	2	17-Nov-84		729366	1871999
0909	MW	В	5057.17	5055.8	2	18-Nov-84		730927	1871393
0910	MW	B	5106.70	5104.6	4	26-Jul-85		730219	1875840
		B			4				
0918	MW		5049.63	5047.2		15-Aug-85	04.14 00	727294	1868724
0925	EXT	В	5060.87	5058.8	6	21-Oct-95	24-May-00	729452	1872006
0926	EXT	В	5062.85	5060.5	6	25-Oct-95	17-May-00	730790	1872126
0933	MW	В	5018.03	5016.3	4	18-Oct-95	24-May-00	731727	1871341
0934	MW	В	5059.73	5058.0	4	02-Nov-95		730018	1871649
0935	MW	В	5061.50	5058.8	4	28-Oct-95	*	729461	1871978
0936	MW	В	5062.30	5059.9	6	26-Oct-95	*	730055	1872121
0937	MW	В	5062.80	5060.2	4	09-Nov-95	24-May-00	730790	1872116
0938	MW	В	5063.64	5060.4	4	26-Oct-95		730769	1872124
0939	EXT	В	5063.23	5061.1	6	23-Oct-95	16-May-00	731403	1872132
0942	MW	B	5066.45	5063.5	4	03-Nov-95		731642	1872409
	MW	B		5095.1	4	13-Oct-95			
0943		1	5098.05				00.1.1.00	731596	1874034
0944	MW	В	5067.00	5064.9	4	04-Nov-95	28-Jul-99	732199	1873007
0947	MW	В	5097.01	5095.0	4	03-Nov-95		732786	1874642
1126	EXT	В	5051.9 **	5051.9 **	4	09-Sep-04		729517	1870728
1127	EXT	В	5056.9 **	5056.9 **	4	11-Sep-04		730044	1871022
1128	EXT	В	5055.0 **	5055.0 **	4	12-Sep-04		730679	1871294
1129	EXT	В	5059.1 **	5059.1 **	4	30-Aug-04		731237	1871690
1130	EXT	В	5059.0 **	5059.0 **	4	29-Jul-04		731699	1871907
1131	EXT	B	5057.8 **	5057.8 **	4	08-Sep-04		732011	1872106
1132	EXT	B	5058.8 **	5058.8 **	4	31-Aug-04		731310	1872015
	-								
1133	EXT	B	5059.1 **	5059.1 **	4	02-Sep-04		730850	1871827
0274	MW	C	5064.42	5062.6	2	30-Aug-04		731623	1872403
0276	MW	С	5067.55	5064.5	2	01-Sep-04		732081	1873158
0279	MW	С	4951.04	4948.6	2	15-Aug-04		731494	1870132
0280	MW	С	4951.52	4949.1	2	15-Aug-04		731794	1870289
0683	MW	С	5070.64	5068.2	6	31-Aug-99		732661	1872574
0684	MW	С	5070.05	5067.3	6	20-Aug-99		732642	1873521
0685	MW	С	5072.44	5069.3	6	19-Aug-99		732295	1873760
0689	MW	C	4981.63	4978.9	2	31-Mar-00		730439	1869893
0691	MW	C	4979.41	4976.9	2	30-Mar-00		732124	1870872
						30-Mar-00 30-Oct-84			
0903	MW	C	4983.33	4981.5	2			731314	1870829
0912	MW	C	5059.97	5057.7	4	12-Aug-85		729324	1871942
0914	MW	С	5070.10	5067.5	4	16-Aug-85		732723	1872119
0917	MW	С	5048.02	5045.8	4	14-Aug-85		727255	1868642
0930	MW	С	4954.96	4953.0	4	23-Oct-95		731257	1870099
0932	MW	С	5057.32	5054.8	4	29-Oct-95		730900	187140
1008	INJ	C	4980.52	4982.3	6	23-Jul-99		730410	186991
1116	EXT	C	5053.74	5056.5	6	08-Aug-99		730350	187170
1116									
1117	EXT	С	5054.95	5057.6	6	11-Aug-99 12-Aug-99		729981 729756	187168
1118	EXT	C	5055.11	5057.8					

	TYPE	Had	TOP OF	MID SCREEN		TOP OF SCREEN	MID SCREEN	BOTTOM OF	SCREEN	SUMP	WELL
WELL	TYPE	Horizon	SCREEN ELEV		SCREEN ELEV	DEPTH	DEPTH	SCREEN DEPTH	LENGTH	LENGTH	DEPTI
0692	MW	D	4895.6	4875.6		55.0	75.0	95.0	40.0	0.3	95.
0695	MW	D	4919.3	4899.3	and the second sec	55.0	75.0	95.0	40.0	0.3	95.
0904	MW	D	4873.8	4868.8	to the second se	28.0	33.0	38.0	10.0	2.0	40.
0915	MW	D	4897.8	4892.8	and the second s	170.0	175.0	180.0	10.0	2.0	182.
1003	INJ	D	4923.4	4898.4	the second se	55.5	80.5	105.5	50.0	2.5	108.
1004	INJ	D	4918.1	4893.1	4868.1	45.5	70.5	95.5	50.0	2.5	98.0
1005	INJ	D	4904.7	4879.7	4854.7	45.5	70.5	95.5	50.0	2.5	98.0
1006	INJ	D	4903.7	4878.7	4853.7	45.7	70.7	95.7	50.0	2.5	98.2
1007	INJ	D	4915.6	4890.5	and the second se	45.8	70.9	96.0	50.2	2.5	98.5
1101	EXT	D	4974.2	4896.5	Name of Academic Street or Street Stree	96.1	173.8	251.5	155.4	2.5	254.0
1102	EXT	D	4968.8	4893.8	the second s	101.5	176.5	251.5	150.0	2.5	254.0
1103	EXT	D	4962.3	4887.3	4812.3	100.0	175.0	250.0	150.0	2.5	252.5
1104	EXT	D	4972.3	4894.8	4817.3	90.0	167.5	245.0	155.0	3.0	248.0
1105	EXT	D	4972.1	4894.6	4817.1	90.0	167.5	245.0	155.0	3.0	248.0
1106	EXT	D	4966.0	4888.7	4811.4	96.5	173.8	251.1	154.6	2.9	254.0
1107	EXT	D	4971.2	4894.0	4816.8	91.1	168.3	245.5	154.4	2.5	248.0
1108	EXT	D	4966.1	4891.1	4816.1	96.3	171.3	246.3	150.0	2.5	248.8
1109	EXT	D	4972.1	4894.7	4817.3	90.3	167.7	245.1	154.8	2.9	248.0
1110	EXT	D	4966.8	4891.8	4816.8	95.5	170.5	245.5	150.0	2.5	248.0
1111	EXT	D	4971.9	4894.7	4817.5	90.7	167.9	245.1	154.4	2.5	247.6
1112	EXT	D	4969.1	4891.6	4814.1	90.5	168.0	245.5	155.0	2.5	248.0
1113	EXT	D	4968.7	4891.2	4813.7	90.5	168.0	245.5	155.0	2.5	248.0
1114	EXT	D	4968.5	4891.0	4813.6	90.6	168.0	245.5	154.9	2.5	248.0
1115	EXT	D	4968.6	4891.2	4813.7	90.5	168.0	245.5	155.0	2.5	248.0
1119	EXT	D	4968.7	4893.7	4818.7	95.3	170.3	245.3	150.0	2.5	247.8
1120	EXT	D	4971.0	4896.0	4821.0	95.5	170.5	245.5	150.0	2.5	248.0
1121	EXT	D	4972.0	4897.0	4822.0	97.5	172.5	247.5	150.0	2.5	250.0
1122	EXT	D	4973.4	4896.3	4819.2	96.9	174.0	251.1	154.2	2.9	254.0
1123	EXT	D	4976.2	4899.2	4822.2	91.0	168.0	245.0	154.0	3.0	248.0
1124	EXT	D	4978.7	4899.9	4821.1	87.9	166.7	245.5	157.6	2.5	248.0
1125	EXT	D	4972.8	4897.8	4822.8	95.5	170.5	245.5	150.0	2.5	248.0
0251	MW	E	4858.9	4808.9	4758.9	200.0	250.0	300.0	100.0	0.3	300.3
0268	MW	E	4864.5	4814.5	4764.5	200.0	250.0	300.0	100.0	0.3	300.3
0920	MW	E	4866.0	4846.0	4826.0	114.4	134.4	154.4	40.0	2.0	156.4
0948	EXDS	E	4893.9	4803.9	4713.9	221.5	311.5	401.5	180.0	5.0	406.5
0911	MW	F	4795.2	4775.2	4755.2	309.4	329.4	349.4	40.0	2.0	351.4
0913	MW	G	4729.2	4709.2	4689.2	328.7	348.7	368.7	40.0	2.0	370.7
0916	MW	G	4721.7	4716.7	4711.7	345.7	350.7	355.7	10.0	2.0	357.7
0919	MW	G	4707.9	4702.9	4697.9	337.7	342.7	347.7	10.0	2.0	349.7
0902	MW	н	4673.7	4668.7	4663.7	63.0	68.0	73.0	10.0	2.0	75.0
0252	MW	1	4658.9	4608.9	4558.9	400.0	450.0	500.0	100.0	0.4	500.4
0254	MW	1	4662.7	4612.7	4562.7	400.0	450.0	500.0	100.0	0.4	500.4
0256	MW	1	4664.0	4614.0	4564.0	400.0	450.0	500.0	100.0	0.4	500.4
0921	MW	1	4663.7	4643.7	4623.7	313.2	333.2	353.2	40.0	2.0	355.2
0253	MW	M	4458.8	4408.8	4358.8	600.0	650.0	700.0	100.0	0.4	700.4
0255	MW	M	4462.3	4412.3	4362.3	600.0	650.0	700.0	100.0	0.4	700.4
0257	MW	M	4463.4	4413.4	4363.4	600.0	650.0	700.0	100.0	0.4	700.4
0968	EXDS	-	5000.4	4699.9	4399.4	106.0	406.5	707.0	601.0	0.0	707.0
0970	EXDS		5007.7	4705.2	4402.7	100.0	402.5	705.0	605.0	0.0	705.0
0971	EXDS		4985.3	4693.8	4402.3	117.0	408.5	700.0	583.0	0.0	700.0
0972	EXDS		5039.7	4724.7	4409.7	100.0	415.0	730.0	630.0	0.0	730.0
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### Table A-1 (continued). Well Completion Information

WELL	TYPE	Horizon	TOP OF CASING ELEV	GROUND	WELL			STATE PLANE	STATE PLANE
				ELEV	DIAMETER	and the second sec	DATE	EAST	NORTH
0692	MW	D	4953.31	4950.6	2		and the last	731821	187030
0695	MW	D	4976.83	4974.3	2			732566	187089
0904	MW	D	4904.11	4901.8	2			731808	186803
0915	MW	D	5070.84	5067.8	4			732740	187220
1003	INJ	D	4976.58	4978.9	6			732101	187089
1004 1005	INJ	D	4961.55	4963.6	6	and the second s		731892	187054
1005	INJ	D	4947.83	4950.2	6	the second second second second		731496	187016
1008	INJ	D	4947.08	4949.5	6			731233	186991
1101	EXT	D	4958.56	4961.4	6		1	730770	186986
1102	EXT	D	5067.29	5070.4	6	the second s		732223	187297
1102	EXT	D	5066.76	5070.3	6			732225	1872670
1103	EXT	D	5059.56	5062.3	6	And And I where it is not been as a second		731896	187240
1104	EXT	D	5059.57	5062.3	6	and the second s		731527	1872404
1105	EXT	D	5059.33	5062.1	6			731304	187240
1107	EXT	D	5059.73	5062.5	6			731081	1872400
1107	EXT	D	5059.51	5062.3	6			730858	187239
And in case of the local data	EXT	D	5059.62	5062.4	6			730634	1872396
1109		D	5059.64	5062.4	6			730410	1872394
1110	EXT	D	5059.47	5062.3	6			730187	187239
1111	one was such in the second second second		5059.87	5062.6	6	And the second sec		729993	1872392
1112	EXT	D	5057.08	5059.6	6			730494	1872064
1113	EXT	D	5058.54	5059.2	6	and the second as the second s		730196	187206
1114	EXT	D	5056.25	5059.1	6			729896	187205
1115	EXT	D	5056.36	5059.2	6			729596	187205
1119	EXT	D	5061.19	5064.0	6			731894	1872667
1120	EXT	D	5063.60	5066.5	6	the second s		731891	1872963
1121	EXT	D	5066.61	5069.5	6			731889	1873267
1122	EXT	D	5067.31	5070.3	6			732221	1873269
1123	EXT	D	5064.54	5067.2	6	the second s		732508	1873222
1124	EXT		5063.86	5066.6	6	Contract of the local division in the second s		732512	1872972
1125	EXT	D	5065.47	5068.3	6	and the similar includes and the		732515	187267
0251	MW MW	E	5061.25	5058.9	2			730215	1871999
0268		E	5067.24	5064.5	2	CONTRACTOR DISTANCEMENTS OF A DESCRIPTION OF A DESCRIPTIO		732301	1872430
0920	MW EXDS	E	4982.97	4980.4	4	the second secon		731262	1870737
0948		E	5117.80	5115.4	4	A		733915	1875516
0911	MW	F	5106.96	5104.6	4	and the second sec		730265	1875920
0913	MW	G	5060.16	5057.9	4	and the second rest of the second sec		729327	1871871
0916	MW		5070.00	5067.4	4			732811	1872146
0919	MW	G H	5048.56	5045.6	4			727353	1868654
0902	MW		4737.42	4736.7	2	and the second s		730179	1862292
0252	MW		5061.30	5058.9	4	the second secon		730232	1871993
0254	MW		5065.38	5062.7	4			730951	187241
0256	MW		5066.58	5064.0	4	to an and the second		732277	1872437
0921	MW	M	4979.08	4976.9	4			731379	1870742
0255	MW	M	5061.11	5058.8	4		11-Apr-01	730213	1871974
0255	MW	M	5064.89	5062.3	4	and the second state of th		730947	1872387
0257	EXDS		5066.40	5063.4	4			732278	1872414
0968	EXDS		5107.00	5106.4	10			730180	1875689
0970	EXDS		5109.53	5107.7	10	the summary set of the		730653	1876567
0971	EXDS		5104.00	5102.3	10	term the second second second		731590	1878306
0912	EXUS		5141.07	5139.7	10			728031	1877986
								METER PLANE	
	-				ALL DIMENS	IONS IN FEET	EXCEPT WELL DIA	METER IN INCHE	S
	-				ALL DEPTHS	ARE RELATIV	E TO GROUND SU	HFACE	
	-				MW	MONITODWO	11		
	1				EXT	MONITOR WE	TER REMEDIATION	EXTRACTION	-1.1
					INJ .	GROUNDWAT	ER REMEDIATION	EXTRACTION WE	2LL
					EXDS	OTHER SUPP		INJECTION WEL	
	1				**	APPROXIMAT			



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Figure A-1. Well Completions Schematic

S0179700

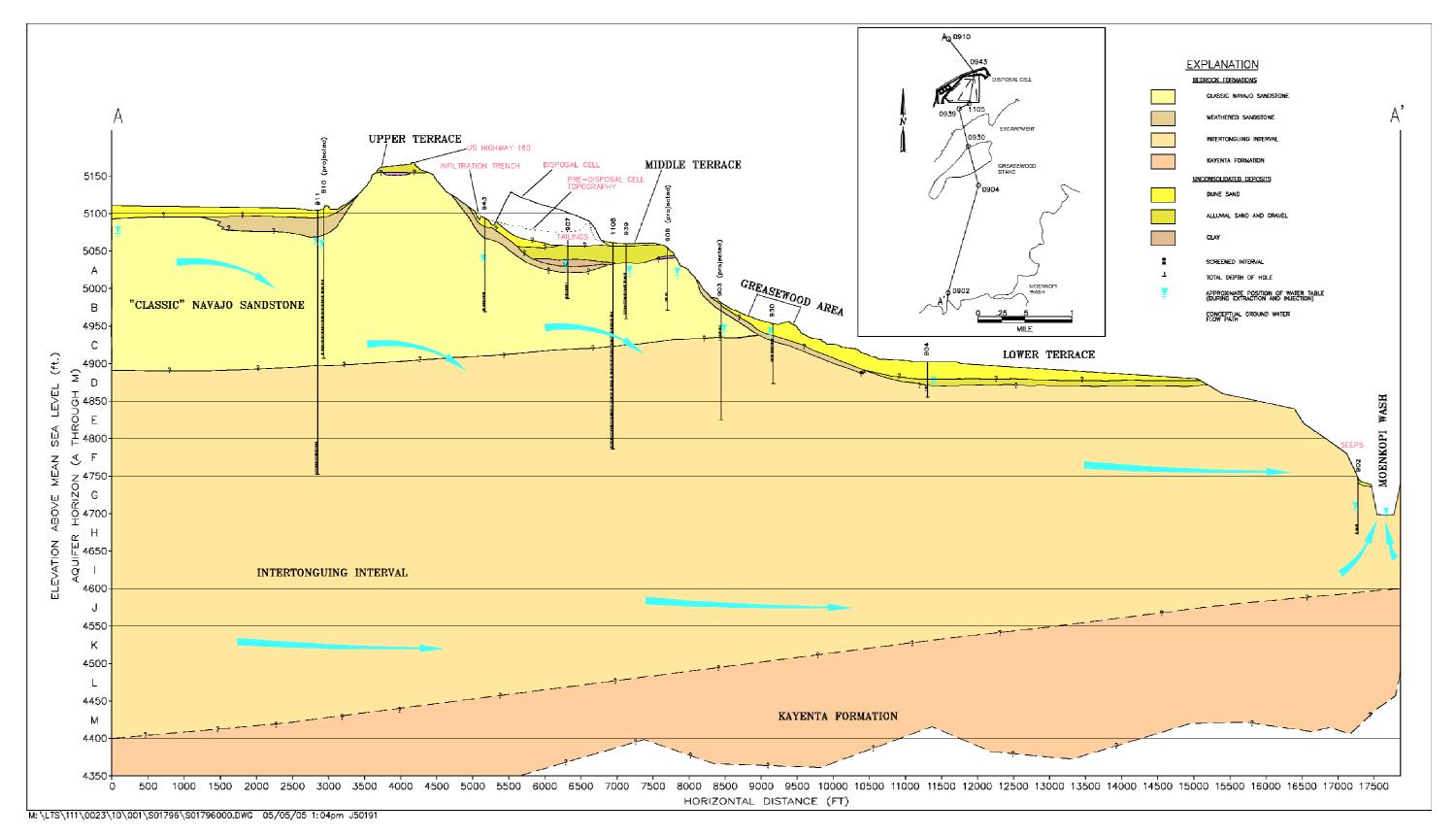


Figure A-2. Conceptual Model of the Site Hydrogeology

### Table A-2. Extraction Well Operation Summary—March 2004 through March 2005

TUBA	CITY EXTRACT	ION WELL C	PERATIONALS	SUMMARY: MA	RCH 2004 THF	ROUGH MAR						
	Mar-04 Total Time On	28.82	dave	q1		a3	Apr-04 Total Time On	29.97	dave			q3
Vell	Total Time		Gallons	gpm	q2 gpm	q3 gpm	Total Time	OST	Gallons	q1 gpm	q2 gpm	gpn
101	26.39	92%	201,345	5.3	4.9	4.5	29.97	100%	246,613	5.7	5.7	5.7
102	27.19	94%	218,507	5.6	5.3	4.9	29.96	100%	235,135	5.4	5.4	5.4
103	27.30	95%	252,458	6.4	6.1	5.7	29.95	100%	277,906	6.4	6.4	6.4
104	27.18	94%	167,683	4.3	4.0	3.8	29.97	100%	172,911	4.0	4.0	4.0
105	14.46	50%	214,388	10.3	5.2	4.8	14.94	50%	221,997	10.3	5.1	5.1
106	18.95	66%	112,722	4.1	2.7	2.5	17.44	58%	75,777	3.0	1.8	1.8
107	25.91	90%	148,146	4.0	3.6	3.3	29.97	100%	158,977	3.7	3.7	3.7
1108	27.30	95%	185,771	4.7	4.5	4.2	29.97	100%	201,853	4.7	4.7	4.7
1109	27.30	95%	95,480	2.4	2.3	2.1	29.97	100%	98,234	2.3	2.3	2.3
1110	24.84	86%	141,352	4.0	3.4	3.2	26.10	87%	139,673	3.7	3.2	3.2
1111	27.30	95%	156,559	4.0	3.8	3.5	29.97	100%	166,638	3.9	3.9	3.9
1112	13.92	48%	83,335	4.2	2.0	1.9	13.48	45%	82,197	4.2	1.9	1.9
1113	18.37	64%	101,407	3.8	2.4	2.3	18.72	62%	99,809	3.7	2.3	2.3
1114	26.73	93%	201,388	5.2	4.9	4.5	29.85	100%	214,936	5.0	5.0	5.0
1115	27.30	95%	245,728	6.2	5.9	5.5	29.97	100%	267,764	6.2	6.2	6.2
1116	0.00	0%	0	0.0	0.0	0.0	0.00	0%	0	0.0	0.0	0.0
1118		93%	54.936	1.4	1.3	1.2	3.29	11%		1.7	0.0	0.0
1119	26.93 27.30	93%	127,575	3.2	3.1	2.9	29.97	100%	8,051	3.2	3.2	3.2
1120	9.51	33%	31,002	2.3	0.7	0.7	8.28	28%	137,831	1.5	0.4	0.4
1121	26.24	91%	177,929	4.7	4.3	4.0	29.95	100%	197,947	4.6	4.6	4.6
1122	27.30	95%	130,969	3.3	3.2	2.9	29.97	100%	132,933	3.1	3.1	3.1
1123	12.91	45%	16,015	0.9	0.4	0.4	12.78	43%	15,346	0.8	0.4	0.4
1124	27.17	94%	165,957	4.2	4.0	3.7	29.97	100%	172,956	4.0	4.0	4.0
1125	27.17	94%	149,425	3.8	3.6	3.3	29.96	100%	158,429	3.7	3.7	3.7
		total gallons	3,380,078						3,502,022			
		rating q gpm	81.5						81.1			
		days/month	31						30			
	avg mo	onthly q gpm	76						81			
		av	g well q gpm	3.9	3.3	3.0				3.8	3.2	3.2
	May-04						Jun-04					
	Total Time On	29.65	davs	q1	q2	q3	Total Time On	27.62	days	q1	q2	q3
Well	Total Time	OST		gpm	gpm	gpm	Total Time	OST	Gallons	gpm	gpm	gpm
1101	29.65	100%	239,097	5.6	5.6	5.4	25.90	94%	212,103	5.7	5.3	4.9
1102	29.64	100%	221,770	5.2	5.2	5.0	27.58	100%	199,460	5.0	4.6	4.6
1103	29.64	100%	273,580	6.4	6.4	6.1	27.56	100%	251,638	6.3	5.8	5.8
1104	29.64	100%	174,268	4.1	4.1	3.9	27.61	100%	166,606	4.2	3.9	3.9
1105	15.58	53%	235,556	10.5	5.5	5.3	14.89	54%	228,802	10.7	5.3	5.3
1106	0.00	0%	0	0.0	0.0	0.0	4.92	18%	16,615	2.3	0.4	0.4
1107	29.64	100%	160,947	3.8	3.8	3.6	27.61	100%	150,662	3.8	3.5	3.5
1108	29.64	100%	198,165	4.6	4.6	4.4	27.58	100%	184,691	4.7	4.3	4.3
1109	29.64	100%	99,606	2.3	2.3	2.2	27.61	100%	97,037	2.4	2.2	2.2
1110	26.54	90%	142,082	3.7	3.3	3.2	26.93	98%	140,633	3.6	3.3	3.3
1111 1112	29.64	100%	161,708 85,179	3.8	3.8	3.6	27.60	100%	149,226	3.8	3.5	3.5
1112	14.14	48%	101,170	3.7	2.0	2.3	13.63	66%	84,030 98,327	3.8	2.3	2.3
1114	29.52	100%	214,036	5.0	5.0	4.8	26.86	97%	201,292	5.2	4.7	4.7
1115	29.64	100%	264,558	6.2	6.2	5.9	27.61	100%	245,317	6.2	5.7	5.7
1116	0.00	0%	0	0.0	0.0	0.0	0.00	0%	0	0.0	0.0	0.0
1117	0.00	0%	0	0.0	0.0	0.0	0.00	0%	0	0.0	0.0	0.0
1118	0.00	0%	0	0.0	0.0	0.0	0.00	0%	0	0.0	0.0	0.0
1119	29.64	100%	135,429	3.2	3.2	3.0	27.59	100%	125,245	3.2	2.9	2.9
1120	9.79	33%	54,994	3.9	1.3	1.2	11.73	42%	116,031	6.9	2.7	2.7
1121	29.64	100%	191,214	4.5	4.5	4.3	27.58	100%	180,293	4.5	4.2	4.2
1122	29.64	100%	129,453	3.0	3.0	2.9	27.60	100%	120,600	3.0	2.8	2.8
1123	12.35	42%	15,026	0.8	0.4	0.3	11.57	42%	14,296	0.9	0.3	0.3
1124	29.64	100%	168,198	3.9	3.9	3.8	27.61	100%	155,784	3.9	3.6	3.6
1125	29.63			3.7	3.6	3.5	27.45	99%	143,650	3.6	3.3	3.3
		total gallons							3,282,335			
		rating q gpm	80.2						82.5			
		days/month	31						30			Obsil total obsil to
	avg mo	onthly q gpm av	g well g gpm	3.7	3.2	3.1			76	3.9	3.1	3.0
			5 ···· 4 5p.··									0.0
	Jul-04						Aug-04					
	Total Time On	18.13	davs	q1	q2	q3	Total Time On	27.15	davs	q1	q2	q3
Nell	Total Time	OST		gpm	gpm	gpm	Total Time	OST		gpm	gpm	gpm
1101	18.11	100%	160,257	6.1	6.1	3.6	27.14	100%	237,360	6.1	6.1	5.3
		100%	133,501	5.1	5.1	3.0	27.12	100%	195,115	5.0	5.0	4.4

### Table A-2 (continued). Extraction Well Operation Summary—March 2004 through March 2005

TUBA	CITY EXTRACT	ON WELL O	PERATIONAL S	SUMMARY: M	ARCH 2004 TH	ROUGH MAR	CH 2005					
103	18.07	100%	165,576	6.4	6.3	3.7	27.06	100%	247,916	6.4	6.3	5.6
104	18.09	100%	121,855	4.7	4.7	2.7	27.07	100%	170,879	4.4	4.4	3.1
105	16.59	92%	73,282	3.1	2.8	1.6	26.94	99%	116,902	3.0	3.0	2.
1106	18.09	100%	73,453	2.8	2.8	1.6	27.14	100%	102,032	2.6	2.6	2.3
107	18.09	100%	103,965	4.0	4.0	2.3	27.06	100%	146,982	3.8	3.8	3.
108	18.04	100%	121,815	4.7	4.7	2.7	27.00	99%	180,070	4.6	4.6	4.0
109	17.93	99%	71.005	2.8	2.7	1.6	27.13	100%	98,705	2.5	2.5	2.
110	17.94	99%	104,731	4.1	4.0	2.3	27.09	100%	144,387	3.7	3.7	3.1
1111	17.98	99%	99,368	3.8	3.8	2.2	27.12	100%	144,622	3.7	3.7	3.2
1112	15.28	84%	64,267	2.9	2.5	1.4	23.63	87%	78.597	2.3	2.0	1.8
1113	7.34	41%	34,007	3.2	1.3	0.8	9.64	36%	38,251	2.8	1.0	0.9
1114	15.85	87%	120,264	5.3	4.6	2.7	24.39	90%	159,769	4.5	4.1	3.6
1115	17.93	99%	152,977	5.9	5.9	3.4	27.14	100%	223,578	5.7	5.7	5.0
1116	14.72	81%	88,472	4.2	3.4	2.0	27.14	100%	157,591	4.0	4.0	3.5
1117	14.73	81%	153,195	7.2	5.9	3.4	27.13	100%	281,086	7.2	7.2	6.3
1118	14.73	81%	74,320	3.5	2.8	1.7	19.80	73%	112,150	3.9	2.9	2.5
1119	18.00	99%	90,280	3.5	3.5	2.0	27.11	100%	127,825	3.3	3.3	2.1
1120	13.55	75%	156,382	8.0	6.0	3.5	19.12	70%	203,751	7.4	5.2	4.6
1121	18.00	99%	123,307	4.8	4.7	2.8	26.99	99%	183,732	4.7	4.7	4.
1122	18.00	99%	87.014	3.4	3.3	1.9	27.14	100%	124.619	3.2	3.2	2.8
1123	4.14	23%	4.286	0.7	0.2	0.1	7.36	27%	6,491	0.6	0.2	0.1
1124	12.97	72%	81,951	4.4	3.1	1.8	0.00	0%	2	0.0	0.2	0.0
1124	12.97	99%	102,833	4.4	3.9	2.3	26.91	99%	156,487	4.0	4.0	3.6
1120		total gallons	2,562,362	4.0	3.3	2.3	20.31	3370	3.638.897	+.0	4.0	3.5
			Colorante provincialization resistant of grant provinces						ten providi interes planto instato branito di Presi pre			
		rating q gpm	98.2						93.1			
		days/month	And and a second s						31			
	avg mo	onthly q gpm	57 g well q gpm	4.3	3.9	2.3			62	4.0	3.7	3.3
		av	g wen q gpm	4.0	3.5	2.5				4.0	3.7	0.0
	0						0.1.01					
	Sep-04	10.15	dava				Oct-04	45.10	1			
	Total Time On	13.46		q1	q2	q3	Total Time On	15.48		q1	q2	q
Vell	Total Time	OST	Gallons	gpm	gpm	gpm	Total Time	OST	Gallons	gpm	gpm	gpn
1101	13.42	100%	117,148	6.1	6.0	2.7	15.41	100%	138,626	6.2	6.2	3.1
1102	13.42	100%	98,372	5.1	5.1	2.3	15.42	100%	120,502	5.4	5.4	2.7
1103	13.39	100%	123,133	6.4	6.4	2.9	15.39	99%	142,499	6.4	6.4	3.2
1104	13.42	100%	90,508	4.7	4.7	2.1	15.40	99%	127,818	5.8	5.7	2.9
1105	13.42	100%	101,351	5.2	5.2	2.3	15.42	100%	116,318	5.2	5.2	2.6
1106	13.42	100%	49,919	2.6	2.6	1.2	15.42	100%	71,032	3.2	3.2	1.6
1107	13.42	100%	76,903	4.0	4.0	1.8	15.38	99%	96,473	4.4	4.3	2.2
1108	13.31	99%	90,199	4.7	4.7	2.1	14.88	96%	109,332	5.1	4.9	2.4
1109	13.42	100%	50,633	2.6	2.6	1.2	15.42	100%	69,710	3.1	3.1	1.6
1110	13.39	99%	79,678	4.1	4.1	1.8	15.41	100%	115,961	5.2	5.2	2.6
1111	13.42	100%	71,809	3.7	3.7	1.7	15.42	100%	89,586	4.0	4.0	2.0
1112	12.00	89%	47.464	2.7	2.4	1.1	15.40	100%	83,261	3.8	3.7	1.9
1113	6.55	49%	25,818	2.7	1.3	0.6	11.73	76%	45,543	2.7	2.0	1.0
1114	13.40	100%	92,869	4.8	4.8	2.1	15.38	99%	119,029	5.4	5.3	2.7
1115	13.42	100%	112,409	5.8	5.8	2.6	15.41	100%	137.116	6.2	6.1	3.1
1116	13.42	100%	76,866	4.0	4.0	1.8	15.41	100%	86,203	3.9	3.9	1.9
1117	13.42	100%	138,971	7.2	7.2	3.2	15.41	100%	159,966	7.2	7.2	3.6
1118	12.84	95%	74,759	4.0	3.9	1.7	15.42	100%	88,584	4.0	4.0	2.0
1119	13.42	100%	65,110	3.4	3.4	1.5	15.42	100%	86,309	3.9	3.9	1.9
1120	9.60	71%	124,124	9.0	6.4	2.9	15.17	98%	238,933	10.9	10.7	5.4
121	13.42	100%	92,718	4.8	4.8	2.1	15.42	100%	115,219	5.2	5.2	2.0
122	13.42	100%	65.575	3.4	3.4	1.5	15.42	100%	88,632	4.0	4.0	2.0
123	5.90	44%	5,173	0.6	0.3	0.1	10.42	69%	9,744	0.6	0.4	0.1
1124	0.00	0%	0	0.0	0.0	0.0	0.00	05%	0	0.0	0.0	0.0
1124	13.41	100%	80,650	4.2	4.2	1.9	15.42	100%	100.136	4.5	4.5	2.1
120			1,952,157	4.2	4.2	1.2	10.42	10070	2,556,530	4.0	4.0	2
		total gallons										
	oper	ating q gpm	100.7						114.7			
		days/month	30						31			
	avy mo		g well q gpm	4.2	4.0	1.8			57	4.7	4.6	2.3
	avg mo	onthly q gpm av	45 g well q gpm	4.2	4.0	1.8			57	4.7	4.6	
	Nov-04						Dec-04					
	Total Time On	23.31	davs	q1	q2	q3	Total Time On	24.23	davs	q1	q2	
		OST				gpm	Total Time	0ST	Gallons			q
Noll	Total Time	031		gpm 6.1	gpm 6.1	4.7	24.15	100%	204.056	gpm 5.9	gpm 5.8	gpr 4.
	Total Time	100%					24.15	10070	204.000	0.9		4.
1101	23.25	100%	203,946									
1101 1102	23.25 23.25	100%	171,778	5.1	5.1	4.0	24.15	100%	172,369	5.0	4.9	3.9
1101 1102 1103	23.25 23.25 23.26	100% 100%	171,778 215,886	5.1 6.4	5.1 6.4	4.0 5.0	24.15 24.15	100% 100%	172,369 222,418	5.0 6.4	4.9 6.4	3.9 5.0
1101 1102 1103 1104	23.25 23.25 23.26 23.24	100% 100% 100%	171,778 215,886 150,253	5.1 6.4 4.5	5.1 6.4 4.5	4.0 5.0 3.5	24.15 24.15 24.15	100% 100% 100%	172,369 222,418 145,489	5.0 6.4 4.2	4.9 6.4 4.2	3.9
Well 1101 1102 1103 1104 1105 1106	23.25 23.25 23.26	100% 100%	171,778 215,886 150,253 173,744	5.1 6.4	5.1 6.4	4.0 5.0	24.15 24.15	100% 100%	172,369 222,418	5.0 6.4	4.9 6.4	

#### Table A-2 (continued). Extraction Well Operation Summary—March 2004 through March 2005

TUDA	CITY EXTRACTION			I IBABAA DV- BAA	BOU 2004 TU		011 2005					
10BA (	23.25	100%	132.224	3.9	3.9	3.1	24.15	100%	133,364	3.8	3.8	3.0
1108	23.13	99%	166.931	5.0	5.0	3.9	24.15	100%	172,253	5.0	4.9	3.9
1109	23.25	100%	89,642	2.7	2.7	2.1	24.15	100%	83,802	2.4	2.4	1.9
1110	23.17	99%	127,371	3.8	3.8	2.9	23.80	98%	124,826	3.6	3.6	2.8
1111	23.25	100%	126,853	3.8	3.8	2.9	24.15	100%	126,452	3.6	3.6	2.8
1112	22.47	96%	76,490	2.4	2.3	1.8	23.53	97%	71,915	2.1	2.1	1.6
1113	14.51	62%	52,869	2.5	1.6	1.2	18.40	76%	62,667	2.4	1.8	1.4
1114	23.25	100%	155,525	4.6	4.6	3.6	24.15	100%	157,076	4.5	4.5	3.5
1115	23.25	100%	192,316	5.7	5.7	4.5	24.15	100%	197,158	5.7	5.7	4.4
1116	23.25	100%	133,356	4.0	4.0	3.1	24.15	100%	136,383	3.9	3.9	3.1
1117	23.25	100%	240,336	7.2	7.2	5.6	24.15	100%	248,614	7.1	7.1	5.6
1118	23.18	99%	132,592	4.0	4.0	3.1	24.15	100%	138,874	4.0	4.0	3.1
1119	23.25	100%	111,068	3.3	3.3	2.6	24.15	100%	104,490	3.0	3.0	2.3
1120	15.83	68%	195,579	8.6	5.8	4.5	15.17	63%	177,313	8.1	5.1	4.0
1121	23.22	100%	160,271	4.8	4.8	3.7	24.05	99%	162,598	4.7	4.7	3.6
1122	23.26	100%	112,183	3.3	3.3	2.6	24.15	100%	109,936	3.2	3.2	2.5
1123	9.85	42%	8,436	0.6	0.3	0.2	10.86	45%	8,886	0.6	0.3	0.2
1124	0.00	0%	0	0.0	0.0	0.0	0.00	0%	0	0.0	0.0	0.0
1125	23.26	100%	137,836	4.1	4.1	3.2	24.15	100%	141,310	4.1	4.1	3.2
		al gallons	3,348,914					1	3,354,076			
		ing q gpm	99.8						96.1			
		sys/month	30						31			
	avg mont		78						75		2.0	
		avg	y well q gpm	4.2	4.0	3.1				4.0	3.8	3.0
	Jan-05						Feb-05					
	Total Time On	27.55	dave				Total Time On	24.98	lave	- 1	-2	-2
Well	Total Time On	27.55 OST	Gallons	q1	q2	q3	Total Time On	24.98 C	Gallons	q1	q2	q3
1101	27.46	100%	230,448	gpm 5.8	gpm 5.8	gpm 5.3	15.69	63%	124,621	gpm 5.5	gpm 3.5	gpm 3.1
1102	27.46	100%	192,551	4.9	4.9	4.5	24.91	100%	170.022	4.7	4.7	4.2
1103	27.46	100%	253,131	6.4	6.4	5.9	24.91	100%	228,914	6.4	6.4	5.7
1104	27.40	100%	162,336	4.1	4.1	3.8	24.91	100%	144,596	4.0	4.0	3.6
1105	27.45	100%	248,236	6.3	6.3	5.7	24.91	100%	231,318	6.4	6.4	5.7
1106	27.47	100%	82.990	2.1	2.1	1.9	24.91	100%	71,908	2.0	2.0	1.8
1107	27.46	100%	150,142	3.8	3.8	3.5	24.92	100%	134,706	3.8	3.7	3.3
1108	27.43	100%	194,600	4.9	4.9	4.5	24.90	100%	176,173	4.9	4.9	4.4
1109	27.46	100%	94,891	2.4	2.4	2.2	24.91	100%	81,176	2.3	2.3	2.0
1110	26.96	98%	137,199	3.5	3.5	3.2	24.42	98%	123,618	3.5	3.4	3.1
1111	27.46	100%	138,956	3.5	3.5	3.2	24.91	100%	123,607	3.4	3.4	3.1
1112	27.38	99%	77,410	2.0	2.0	1.8	24.86	100%	68,846	1.9	1.9	1.7
1113	25.31	92%	80,040	2.2	2.0	1.9	24.25	97%	76,242	2.2	2.1	1.9
1114	27.46	100%	174,551	4.4	4.4	4.0	24.91	100%	162,478	4.5	4.5	4.0
1115	27.47	100%	222,278	5.6	5.6	5.1	24.91	100%	209,648	5.8	5.8	5.2
1116	27.46	100%	154,833	3.9	3.9	3.6	24.91	100%	143,992	4.0	4.0	3.6
1117	27.46	100%	280,851	7.1	7.1	6.5	3.49	14%	19,812	3.9	0.6	0.5
1118	27.46	100%	157,045	4.0	4.0	3.6	24.91	100%	151,328	4.2	4.2	3.8
1119	27.46	100%	116,810	3.0	2.9	2.7	24.91	100%	105,532	2.9	2.9	2.6
1120	16.56	60%	189,720	8.0	4.8	4.4	14.70	59%	166,071	7.8	4.6	4.1
1121	27.42	100%	184,842	4.7	4.7	4.3	24.87	100%	165,560	4.6	4.6	4.1
1122	27.46	100%	121,966	3.1	3.1	2.8	24.91	100%	108,926	3.0	3.0	2.7
1123	14.64	53%	11,697	0.6	0.3	0.3	14.95	60%	10,798	0.5	0.3	0.3
1124	0.00	0%	0	0.0	0.0	0.0	12.03	48%	91,372	5.3	2.5	2.3
1125	26.47	96%	159,392	4.2	4.0	3.7	24.91	100%	136,625	3.8	3.8	3.4
		al gallons	3.816,916					i	3.227.888			
		ing q gpm	96.2						89.7			
		ys/month	30						28			
	avg mont		88 well q gpm	4.0	3.8	3.5			80	4.1	3.6	3.2
	Mar-05											
	Total Time On	30.54		q1	q2	q3		-				
Well	Total Time	OST	Gallons	gpm	gpm	gpm						
1101	27.90	91%	271,428	6.8	6.2	6.1						
1102	30.34	99%	191,512	4.4	4.4	4.3						
1103	30.45	100%	277,772	6.3	6.3	6.2						
1104	30.45	100%	166,811	3.8	3.8	3.7						
1105	30.45	100%	274,606	6.3	6.2	6.2						
1106	30.45	100%	80,668	1.8	1.8	1.8						
1107	30.45	100%	160,017	3.6	3.6	3.6						
1108	30.45	100%	209,306	4.8	4.8	4.7						
	30.45	100%	93,320	2.1	2.1	2.1						
1109				3.3	3.3	3.2						
11109 11110 11111	29.91 30.45	98% 100%	145,536	3.3	3.3	3.3		1		1		

### Table A-2 (continued). Extraction Well Operation Summary—March 2004 through March 2005

1113	29.85	98%	78,659	1.8	1.8	1.8		
1114	30.45	100%	190,799	4.4	4.3	4.3		
1115	30.45	100%	249,497	5.7	5.7	5.6		
1116	30.45	100%	170,174	3.9	3.9	3.8		
1117	29.51	97%	129,734	3.1	2.9	2.9		
1118	30.46	100%	177,878	4.1	4.0	4.0		
1119	30.45	100%	126,071	2.9	2.9	2.8		
1120	16.66	55%	173,492	7.2	3.9	3.9		
1121	30.45	100%	194,309	4.4	4.4	4.4		
1122	30.45	100%	121,113	2.8	2.8	2.7		
1123	14.94	49%	9,845	0.5	0.2	0.2		
1124	30.45	100%	220,324	5.0	5.0	4.9		
1125	30.37	99%	144,378	3.3	3.3	3.2		
	tota	al gallons	4,077,677					
	operatin	ng q gpm	92.7					
	day	/s/month	31					
	avg month	ly q gpm	91					
		avg	well q gpm	3.9	3.7	3.7	 	 
	on = number of d							
	number of days			e; excludes off	-cycle time		 	 
	eam time) = total		total time				 	 
	taneous pumpin						 	 
	ive pumping rate			1e				 
13 = effecti	ive pumping rate	e during m	onth				 	 

## Appendix B

Ground Water Sample Results for February 2004 and the Baseline Period for Contaminants Requiring Remediation This page intentionally left blank

Well Number	Horizon	Baseline Molybdenum Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Molybdenum Concentration (mg/L)	Feb 2005 Molybdenum Concentration (mg/L)
0284	Α			NS	Dry
0285	A			NS	Dry
0686	A	0.0015U	2002	0.0014	0.0011U
0687	A	0.0113	2002	0.0017	0.0015
0688	A	0.0015U	2002	0.0029	0.0016
0901	A	0.00078	2001	0.00065BU	0.00054BU
0906	A	0.0137	2002	0.028	0.017
0929	A	0.0015U	2002	0.00047BU	0.00046BU
0940	A	0.0015U	2002	NS	NS
0941	A	0.0284	2002	0.063	0.021
0945	A	0.0015U	2002	0.0011	NS
0946	A			0.0025	0.0024
0001	В		-	NS	NS
0262	В	0.432	2001	0.58	0.64
0263	В	0.192	2001	0.059	0.042
0265	В	0.00046	2001	0.00064BU	0.00047BU
0267	В	0.0015U	2002	0.00053BU	0.00041BU
0271	В	0.0015U	2002	0.00041BU	NS
0281	В			NS	0.0031
0282	В			NS	0.0048
0283	В			NS	0.003
0908	B	0.0015U	2002	0.0004BU	0.00044BU
0909	В	0.0015U	2002	0.00049BU	0.00032BU
0910	B	0.00100	2002	NS	0.00052BU
0918	B			NS	0.00052B0 NS
0934	B	0.0015U	2002	0.00038BU	0.00035BU
0935	B	0.0015U	2002	NS	NS
0936	B	0.0015U	2002	0.0013	0.0012U
0938	B	0.001U	1999	NS	NS
0942	B	0.021	2002	0.025	0.018
0943	B	0.0015U	2002	0.0005BU	0.00035BU
0947	B	0.0015U	2002	NS	NS
1126	B	0.00100	2002	NS	NS
1127	B			NS	NS
1128	B			NS	NS
1129	B			NS	NS NS
1130	B	-		NS	NS
1131	B			NS	NS
1132	B			NS	NS
1133	B			NS	NS
0274	C			NS	and a fact that the second
0276	C			NS	0.00058BU
0279	C			NS	0.00063BU
0279	c				0.0038
0683	C	0.0015U	2002	NS	0.00063BU
0684	c	0.00150	2002	0.00066BU 0.00077BU	NS NS

Well Number	Horizon	Baseline Molybdenum Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Molybdenum Concentration (mg/L)	Feb 2005 Molybdenum Concentration (mg/L)
0685	С	0.0015U	2002	0.00054BU	NS
0689	С	0.0015U	2002	0.00049BU	NS
0691	С	0.0015U	2002	0.00035BU	0.0004BU
0903	С	0.0015U	2002	0.00053BU	0.00045BU
0912	C	0.0003U	2001	0.00044BU	NS
0914	C	0.00081	2001	0.00078BU	NS
0917	C	0.0013	2001	NS	0.00057BU
0930	C	0.0015U	2002	0.00037BU	0.00035BU
0932	C	0.0018U	2002	0.0014	0.00063BU
1008	C	0.0004U	2000	NS	0.0005BU
1116	С	0.0015U	2002	0.00033BU	NS
1117	C	0.0015U	2002	0.00034BU	NS
1118	С	0.0015U	2002	NS	NS
0258	D	0.00063	2000	NS	0.00053BU
0261	D	0.0026	2001	0.00069BU	NS
0264	D	0.0031	2001	0.00077BU	0.00052BU
0266	D	0.00058	2001	0.00054BU	0.00049BU
0272	D			NS	0.00038BU
0273	D			NS	0.027
0275	D		+	NS	0.0006BU
0277	D			NS	0.0016
0278	D			NS	0.00053BU
0690	D	0.0015U	2002	0.00069BU	0.00056BU
0692	D	0.0015U	2002	0.00063B	0.00055BU
0695	D	0.0015U	2002	0.00068BU	NS
0904	D	0.00077	2001	NS	0.0006BU
0915	D	0.00054	2001	NS	NS
1003	D	0.0004U	2000	NS	0.00034BU
1004	D	0.0004U	2000	0.00051BU	0.00046BU
1005	D	0.0004U	2000	NS	NS
1006	D	0.0004U	2000	NS	0.0004BU
1007	D	0.0004U	2000	NS	0.00035BU
1101	D	0.0015U	2002	0.00058BU	NS
1102	D	0.0015U	2002	0.00042BU	NS
1103	D	0.0015U	2002	0.00098BU	NS
1104	D	0.0916	2002	0.043	NS
1105	D	2.96	2002	1.5	NS
1106	D	1.26	2002	0.44	NS
1107	D	0.16	2002	0.014	NS
1108	D	0.0015U	2002	0.00045BU	NS
1109	D	0.0015U	2002	0.00038BU	NS
1110	D	0.0015U	2002	0.00098BU	NS
1111	D	0.0015U	2002	0.00029BU	NS
1112	D	0.0015U	2002	0.00037BU	NS
1113	D	0.0015U	2002	0.00036BU	NS
1114	D	0.0027	2002	0.00099BU	NS

Well Number	Horizon	Baseline Molybdenum Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Molybdenum Concentration (mg/L)	Feb 2005 Molybdenum Concentration (mg/L)
1115	D	0.0015U	2002	0.00038BU	NS
1119	D	0.0053	2002	0.00082BU	NS
1120	D	0.0815	2002	0.025	NS
1121	D	0.105	2002	0.039	NS
1122	D	0.0015U	2002	0.00068BU	NS
1123	D	0.0015U	2002	NS	NS
1124	D	0.0015U	2002	NS	NS
1125	D	0.0015U	2002	0.00048BU	NS
0251	E	0.0015U	2002	0.00054BU	0.00044BU
0268	E	0.0015U	2002	0.00084BU	0.00051BU
0920	E	0.0003U	2001	NS	0.00049BU
0911	F			NS	0.00039BU
0913	G	0.0003U	2001	0.00038BU	NS
0916	G	0.00096	2001	NS	NS
0919	G			NS	0.00074BU
0902	Н			NS	NS
0252	1	0.0015U	2002	0.00082BU	0.00036BU
0254	1	0.164	2002	0.059	0.055
0256	1	0.0015U	2002	0.00099BU	0.00055BU
0921	1	0.0003U	2001	NS	0.00037BU
0255	М	0.0043	2000	0.059	0.071
0257	M	0.00041	2000	0.042U	0.044

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B=Result is between the IDL and CRDL NS=Not sampled U=Analytical result below detection limit

Well Number	Horizon	Baseline Nitrate Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Nitrate Concentration (mg/L)	Feb 2005 Nitrate Concentration (mg/L
0284	A			NS	Dry
0285	A			NS	Dry
0686	A	32.2	2002	16	16
0687	A	60.6	2002	7.5	12
0688	A	35.1	2002	39	43
0901	A	13	2001	14	14
0906	A	1470	2002	1510	1590
0929	A	69.5	2002	71	62
0940	A	1800	2002	NS	NS
0941	A	358	2002	576	708
0945	A	12.7	2002	12	NS
0946	A			23	25
0001	В	and prove the second		NS	NS
0262	В	380	2001	487	487
0263	В	1140	2001	841	753
0265	В	720	2001	430	487
0267	В	1640	2002	1550	1510
0271	B	15.6	2002	16	NS
0281	B		LOOL	NS	89
0282	B			NS	487
0283	B			NS	487
0908	B	651	2002	664	664
0909	B	485	2002	531	576
0910	B	100	2002	NS	10
0918	B			NS	NS
0934	B	2320	2002	2260	2170
0935	B	525	2002	NS	The second se
0936	B	2950	2002	2120	615 2430
0938	B	1450	1999	NS	NS
0942	B	1360	2002	1460	1680
0943	B	22.1	2002	330	210
0947	B	12.5	2002	NS	NS
1126	B	12.0	2002	NS	and some the second state of the second state
1127	B			NS	1143 400
1128	B			NS	400
1129	B			NS	the second se
1130	B			NS	578
1131	B			NS	1179
1132	B			NS	1535
1133	B				1203
0274	C			NS	692
0274	C			NS	15
0278	c			NS	14
0279	C			NS	28
0280	C	14.1	0000	NS	10
0683	C	<u> </u>	2002	<u> </u>	NS

Well Number	Horizon	Baseline Nitrate Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Nitrate Concentration (mg/L)	Feb 2005 Nitrate Concentration (mg/L)
0685	С	14.3	2002	10	NS
0689	C	14.3	2002	14	NS
0691	C	298	2002	170	200
0903	C	54.8	2002	49	42
0912	C	403	2001	280	NS
0914	C	13	2001	12	NS
0917	C	15.7	2001	NS	16
0930	C	50.9	2002	62	66
0932	C	25.3	2002	25	26
1008	C	15.7	2000	NS	14
1116	C	106	2002	89	109
1117	C	225	2002	340	NS
1118	C	164	2002	NS	588
0258	D	15	2000	NS	15
0261	D	14	2001	15	NS
0264	D	24.3	2001	40	38
0266	D	14	2001	15	15
0272	D			NS	17
0273	D			NS	190
0275	D			NS	1060
0277	D			NS	14
0278	D			NS	14
0690	D	12.5	2002	13	13
0692	D	12.5	2002	13	13
0695	D	25.4	2002	27	NS
0904	D	5.13	2001	NS	4
0915	D	14.1	2001	NS	NS
1003	D	176	2000	NS	220
1004	D	49.1	2000	21	44
1005	D	14.5	2000	NS	NS
1006	D	14.1	2000	NS	10
1007	D	15.3	2000	NS	15
1101	D	438	2002	443	485
1102	D	650	2002	620	601
1103	D	1120	2002	1020	1062
1104	D	993	2002	531	580
1105	D	648	2002	531	219
1106	D	614	2002	200	185
1107	D	1060	2002	210	178
1108	D	1410	2002	664	641
1109	D	798	2002	410	425
1110	D	227	2002	180	174
1111	D	421	2002	390	391
1112	D	617	2002	150	127
1113	D	143	2002	49	45
1114	D	228	2002	200	214

Well Number	Horizon	Baseline Nitrate Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Nitrate Concentration (mg/L)	Feb 2005 Nitrate Concentration (mg/L)
1115	D	766	2002	290	284
1119	D	468	2002	487	534
1120	D	493	2002	270	228
1121	D	573	2002	210	195
1122	D	954	2002	270	226
1123	D	643	2002	NS	104
1124	D	781	2002	NS	NS
1125	D	104	2002	49	45
0251	E	426	2002	16	17
0268	E	15.4	2002	39	62
0920	E	14.8	2001	NS	15
0911	F			NS	10
0913	G	12.4	2001	12	NS
0916	G	11.6	2001	NS	NS
0919	G			NS	6.2
0902	н			NS	NS
0252	I	15.3	2002	10	11
0254	1	354	2002	440	487
0256	1	189	2002	39	49
0921	1	11	2001	NS	11
0255	M	9.6	2000	0.04U	0.04U
0257	M	6.9	2000	0.04U	0.04U

NS=Not sampled

U=Analytical result below detection limit

Well Number	Horizon	Baseline Selenium Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Selenium Concentration (mg/L)	Feb 2005 Selenium Concentration (mg/L
0284	A			NS	Dry
0285	A			NS	Dry
0686	A	0.0088	2002	0.0051	0.0036
0687	A	0.0145	2002	0.0003	0.00046
0688	A	0.0033	2002	0.0057	0.015
0901	A	0.0024	2001	0.0021	0.0017
0906	A	0.0335	2002	0.02	0.017
0929	A	0.0028	2002	0.0022	0.0022
0940	A	0.105	2002	NS	NS
0941	A	0.0348	2002	0.048	0.055
0945	A	0.0035	2002	0.0031	NS
0946	A			0.0037	0.0047
0001	В			NS	NS
0262	В	0.0621	2001	0.061	0.065
0263	В	0.0632	2001	0.04	0.032
0265	B	0.0071	2001	0.0037	0.0036
0267	B	0.0532	2002	0.048	0.043
0271	B	0.0016	2002	0.0012	NS
0281	B	0.0010	LUUL	NS	0.00098
0282	B			NS	0.0035
0283	B			NS	0.0088
0908	B	0.0163	2002	0.022	0.023
0909	B	0.0224	2002	0.022	0.023
0910	B	0.0224	2002	NS	0.001
0918	B			NS	NS
0934	B	0.0116	2002	0.0089	0.0097
0935	B	0.0195	2002	NS	NS
0936	B	0.0869	2002	0.053	0.054
0938	В	0.0432	1999	NS	NS
0942	B	0.0348	2002	0.037	0.039
0943	В	0.0021	2002	0.01	the second design of the secon
0947	B	0.0019	2002	NS	0.0089 NS
1126	B	0.0013	2002	NS	115
1127	B			NS	
1128	B			NS	
1129	B			NS	the state of the last
1130	B			NS	
1131	B			and a second sec	
1132	B			NS NS	
1133	B			and the second s	
0274	C			NS	0.0011
0276	c			NS	0.0011
0279	c			NS NS	0.0012
0279	c				0.00066
0280	C	0.0000	2002	NS	0.0016
0000	U	0.0022	2002	0.0015	NS

Well Number	Horizon	Baseline Selenium Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Selenium Concentration (mg/L)	Feb 2005 Selenium Concentration (mg/L)
0685	С	0.0017	2002	0.0013	NS
0689	C	0.0014	2002	0.001	NS
0691	C	0.0046	2002	0.0019	0.0023
0903	C	0.0023	2002	0.0014	0.0013
0912	C	0.0137	2001	0.0083	NS
0914	С	0.0016	2001	0.00081	NS
0917	С	0.0017	2001	NS	0.00092
0930	C	0.002	2002	0.0017	0.0015
0932	С	0.0019	2002	0.0009	0.0011
1008	C	0.0015	2000	NS	0.00083
1116	С	0.0018	2002	0.0016	NS
1117	C	0.0028	2002	0.01	NS
1118	C	0.0028	2002	NS	NS
0258	D	0.0018	2000	NS	0.0012
0261	D	0.0021	2001	0.0012	NS
0264	D	0.0018	2001	0.0011	0.0012
0266	D	0.0013	2001	0.00086	0.00078
0272	D			NS	0.00082
0273	D			NS	0.016
0275	D			NS	0.021
0277	D			NS	0.001
0278	D			NS	0.00085
0690	D	0.0014	2002	0.001	0.00094
0692	D	0.0022	2002	0.0015	0.0014
0695	D	0.0019	2002	0.0015	NS
0904	D	0.0131	2001	NS	0.015
0915	D	0.0019	2001	NS	NS
1003	D	0.003	2000	NS	0.0025
1004	D	0.0021	2000	0.0018	0.0014
1005	D	0.0014	2000	NS	NS
1006	D	0.0013	2000	NS	0.00086
1007	D	0.0013	2000	NS	0.00088
1101	D	0.0188	2002	0.027	NS
1102	D	0.0121	2002	0.021	NS
1103	D	0.0613	2002	0.037	NS
1104	D	0.0344	2002	0.019	NS
1105	D	0.0871	2002	0.067	NS
1106	D	0.0925	2002	0.029	NS
1107	D	0.0903	2002	0.011	NS
1108	D	0.0704	2002	0.031	NS
1109	D	0.0372	2002	0.015	NS
1110	D	0.0081	2002	0.0058	NS
1111	D	0.0172	2002	0.016	NS
1112	D	0.0154	2002	0.0038	NS
1113	D	0.0025	2002	0.0011	NS
1114	D	0.0035	2002	0.0047	NS

Well Number	Horizon	Baseline Selenium Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Selenium Concentration (mg/L)	Feb 2005 Selenium Concentration (mg/L)
1115	D	0.0362	2002	0.0079	NS
1119	D	0.029	2002	0.017	NS
1120	D	0.0563	2002	0.023	NS
1121	D	0.0455	2002	0.017	NS
1122	D	0.0558	2002	0.017	NS
1123	D	0.0449	2002	NS	NS
1124	D	0.0186	2002	NS	NS
1125	D	0.0025	2002	0.0019	NS
0251	E	0.0035	2002	0.00071	0.00067
0268	E	0.0018	2002	0.0012	0.0013
0920	E	0.0014	2001	NS	0.00095
0911	F			NS	0.0007
0913	G	0.00063	2001	0.00047	NS
0916	G	0.001	2001	NS	NS
0919	G			NS	0.00019
0902	н			NS	NS
0252	1	0.00092	2002	0.00056	0.00052
0254	1	0.0531	2002	0.046	0.04
0256	1	0.0031	2002	0.0008	0.00081
0921	I	0.00091	2001	NS	0.00059
0255	M	0.0011	2000	0.00027	0.000079B
0257	M	0.0013	2000	0.00017	0.000092B

B=Result is between the IDL and CRDL NS=Not sampled

Well Number	Horizon	Baseline Sulfate Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Sulfate Concentration (mg/L)	Feb 2005 Sulfate Concentration (mg/L
0284	A			NS	Dry
0285	A			NS	Dry
0686	A	98.6	2002	120	110
0687	A	329	2002	19	35
0688	A	40	2002	110	230
0901	A	26.2	2001	31	30
0906	A	1660	2002	1700	1900
0929	A	28.1	2002	26	26
0940	A	7550	2002	NS	NS
0941	A	745	2002	710	890
0945	A	32.1	2002	34	NS
0946	A			94	100
0001	В		The second secon	NS	NS
0262	В	931	2001	1000	1000
0263	В	1990	2001	1900	2100
0265	В	1520	2001	800	810
0267	В	3680	2002	3500	3700
0271	В	16.4	2002	16	NS
0281	В		LUUL	NS	62
0282	B			NS	790
0283	B			NS	530
0908	B	2430	2002	2600	3000
0909	B	666	2002	590	680
0910	B		2002	NS	16
0918	B			NS	NS
0934	B	7360	2002	2300	2300
0935	B	2690	2002	NS	the second
0936	B	4360	2002	2500	2506
0938	B	2120	1999	NS	NS
0942	B	3030	2002	2900	3000
0943	B	29	2002	520	3000
0947	B	18.7	2002	NS	NS
1126	B	10.7	2002	NS	3583
1127	B			NS	
1128	B			NS	570
1129	B			NS	506
1130	B			NS	1308
1131	B			NS	1993
1132	B			NS	1931
1133	B				1972
0274	C			NS NS	555
0274	c			NS	15
0279	C			terrent state and the state of	18
0279	c			NS	36
0280	C	21.6	2000	NS	21
0684	C	18	2002	18 17	NS NS

Well Number	Horizon	Baseline Sulfate Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Sulfate Concentration (mg/L)	Feb 2005 Sulfate Concentration (mg/L
0685	C	26.2	2002	16	NS
0689	C	13.7	2002	14	NS
0691	C	587	2002	330	340
0903	C	76.5	2002	61	51
0912	C	846	2001	560	NS
0914	C	15.6	2001	15	NS
0917	C	13.9	2001	NS	15
0930	C	59.8	2002	70	80
0932	C	30.2	2002	26	26
1008	C	13	2000	NS	13
1116	С	176	2002	99	139
1117	С	255	2002	690	NS
1118	C	163	2002	NS	1488
0258	D	17.4	2000	NS	1400
0261	D	18.2	2001	20	NS
0264	D	37.7	2001	59	56
0266	D	10.9	2001	11	11
0272	D	10.0	2001	NS	12
0273	D			NS	
0275	D			NS	210
0277	D			NS	2100
0278	D			NS	23
0690	D	13.8	2002	13	14
0692	D	20.8	2002	19	13
0695	D	50.4	2002	54	20
0904	D	96.5	2002	NS State	NS
0915	D	17.8	2001	NS	120
1003	D	302	2001	NS	NS
1004	D	66.2	2000	31	410
1004	D	12.7	2000	NS	68
1006	D	12.2	2000	and the second se	NS
1007	D	11.7	2000	NS	13
1101	D	960	and the second se	NS	12
1102	D	1320	2002	1200	1303
1102	D	2570	2002	1300	1267
1103	D		2002	2000	2007
1104	D	1870	2002	950	978
1105	D	1590	2002	1200	484
1106	D	1050	2002	420	356
		1200	2002	250	217
1108	D	3400	2002	1700	1521
1109	D	3280	2002	1100	1151
1110	D	512	2002	340	340
1111	D	988	2002	890	1021
1112	D	1140	2002	200	190
1113	D	136	2002	38	37
1114	D	328	2002	280	333

Table B-4 (continued). Baseline, August 2004 and Febr	ruary 2005 Sulfate Concentrations
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Well Number	Horizon	Baseline Sulfate Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Sulfate Concentration (mg/L)	Feb 2005 Sulfate Concentration (mg/L)
1115	D	1930	2002	400	448
1119	D	1560	2002	870	1068
1120	D	2330	2002	1300	1166
1121	D	2590	2002	1400	1560
1122	D	2960	2002	1000	903
1123	D	1240	2002	NS	207
1124	D	1170	2002	NS	NS
1125	D	165	2002	76	69
0251	E	617	2002	13	14
0268	E	17.4	2002	55	99
0920	E	12.7	2001	NS	13
0911	F			NS	8.8
0913	G	8.43	2001	8.2	NS
0916	G	13.5	2001	NS	NS
0919	G			NS	3.6
0902	H			NS	NS
0252	1	19.2	2002	6.6	6.8
0254	1	505	2002	530	560
0256	1	368	2002	68	84
0921	1	8.52	2001	NS	7.6
0255	M	102	2000	4100	4400
0257	M	13.4	2000	340	370

NS=Not sampled

Well Number	Horizon	Baseline Uranium Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Uranium Concentration (mg/L)	Feb 2005 Uranium Concentration (mg/L)
0284	A			NS	Dry
0285	A			NS	Dry
0686	A	0.0021	2002	0.0007E	0.0003
0687	A	0.0208	2002	0.000046B	0.000039BU
0688	A	0.002	2002	0.0016	0.0012
0901	A	0.0026	2001	0.0023	0.0023
0906	A	0.951	2002	0.89	0.83
0929	A	0.0012	2002	0.00098	0.001
0940	A	0.546	2002	NS	NS
0941	A	0.0886	2002	0.076	0.049
0945	A	0.0031	2002	0.0034	NS
0946	A			0.00022	0.00016
0262	B	0.379	2001	0.53	0.56
0263	В	0.485	2001	0.23	0.19
0265	B	0.0897	2001	0.045	0.045
0267	B	0.0731	2002	0.088	0.085
0271	В	0.0014	2002	0.0012	NS
0281	В			NS	0.0061
0282	В			NS	0.054
0283	В			NS	0.034
0908	В	0.122	2002	0.12	0.027
0909	В	0.0389	2002	0.029	0.035
0910	В			NS	0.00076
0918	B			NS	0.00070
0934	В	0.312	2002	0.32	0.28
0935	B	0.0868	2002	NS	0.111
0936	B	0.267	2002	0.47	0.47
0938	В	0.21	1999	NS	NS
0942	В	0.246	2002	0.27	0.27
0943	В	0.0049	2002	0.2	0.2
0947	B	0.0024	2002	NS	NS
1126	B			NS	0.069
1127	B			NS	0.027
1128	B			NS	0.035
1129	B			NS	0.643
1130	B			NS	0.2606
1131	B			NS	0.472
1132	В			NS	1.477
1133	B			NS	0.0665
0274	C			NS	0.000
0276	C			NS	0.0013
0279	C			NS	0.0025
0280	C			NS	0.0025
0683	C	0.0012	2002	0.00091	NS
0684	C	0.0019	2002	0.000	NS
0685	C	0.0012	2002	0.00097	NS

Well Number	Horizon	Baseline Uranium Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Uranium Concentration (mg/L)	Feb 2005 Uranium Concentration (mg/L)
0689	C	0.0011	2002	0.00086	NS
0691	C	0.0657	2002	0.03	0.031
0903	C	0.0022	2002	0.0018	0.0014
0912	C	0.0342	2001	0.025	NS
0914	C	0.0013	2001	0.00045	NS
0917	C	0.0013	2001	NS	0.00055
0930	C	0.0023	2002	0.0026	0.0026
0932	C	0.0016	2002	0.0012	0.00099
1008	C	0.001	2000	NS	0.00083
1116	C	0.0081	2002	0.0073	0.0093
1117	C	0.0151	2002	0.03	NS
1118	C	0.0098	2002	NS	0.066
0258	D	0.0018	2000	NS	0.00092
0261	D	0.0018	2001	0.00089	NS
0264	D	0.0033	2001	0.003	0.0027
0266	D	0.0019	2001	0.0012	0.0013
0272	D			NS	0.00095
0273	D			NS	0.056
0275	D			NS	0.44
0277	D			NS	0.0033
0278	D			NS	0.00084
0690	D	0.0018	2002	0.0014	0.0014
0692	D	0.0015	2002	0.0012	0.0011
0695	D	0.002	2002	0.0019	NS
0904	D	0.0044	2001	NS	0.0041
0915	D	0.0017	2001	NS	NS
1003	D	0.0205	2000	NS	0.029
1004	D	0.0053	2000	0.0025	0.0072
1005	D	0.0013	2000	NS	NS
1006	D	0.0014	2000	NS	0.00073
1007	D	0.0012	2000	NS	0.00083
1101	D	0.245	2002	0.32	0.369
1102	D	0.533	2002	0.45	0.398
1103	D	0.355	2002	0.44	0.391
1104	D	0.194	2002	0.12	0.12
1105	D	2.1	2002	1.5	0.578
1106	D	2.1	2002	0.76	0.543
1107	D	0.118	2002	0.041	0.037
1108	D	0.646	2002	0.23	0.218
1109	D	0.565	2002	0.26	0.275
1110	D	0.0528	2002	0.065	0.066
1111	D	0.161	2002	0.16	0.178
1112	D	0.13	2002	0.037	0.036
1113	D	0.0149	2002	0.004	0.0046
1114	D	0.0277	2002	0.028	0.032
1115	D	0.41	2002	0.05	0.053

Well Number	Horizon	Baseline Uranium Concentration (mg/L)	Year Sampled, Baseline	Aug 2004 Uranium Concentration (mg/L)	Feb 2005 Uranium Concentration (mg/L)
1119	D	0.555	2002	0.16	0.206
1120	D	1.3	2002	0.4	0.318
1121	D	0.857	2002	0.37	0.337
1122	D	0.878	2002	0.29	0.263
1123	D	0.261	2002	NS	0.041
1124	D	0.171	2002	NS	NS
1125	D	0.0176	2002	0.011	0.011
0251	E	0.0481	2002	0.0013	0.0012
0268	E	0.0014	2002	0.0077	0.015
0920	E	0.0017	2001	NS	0.00095
0911	F			NS	0.00085
0913	G	0.0016	2001	0.00091	NS
0916	G	0.0014	2001	NS	NS
0919	G			NS	0.000044BU
0902	Н			NS	NS
0252		0.0024	2002	0.0015	0.0013
0254		0.209	2002	0.1	0.089
0256		0.0775	2002	0.0097	0.01
0921		0.0047	2001	NS	0.0046
0255	M	0.0029	2000	0.0019	0.0017
0257	M	0.0037	2000	0.018	0.018

B=Result is between the IDL and CRDL

 $\ensuremath{\mathsf{E=}\mathsf{Estimate}}$  value because of interference, see case narrative NS=Not sampled

U=Analytical result below detection limit

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Appendix C

Monitor Well Water Level Hydrographs

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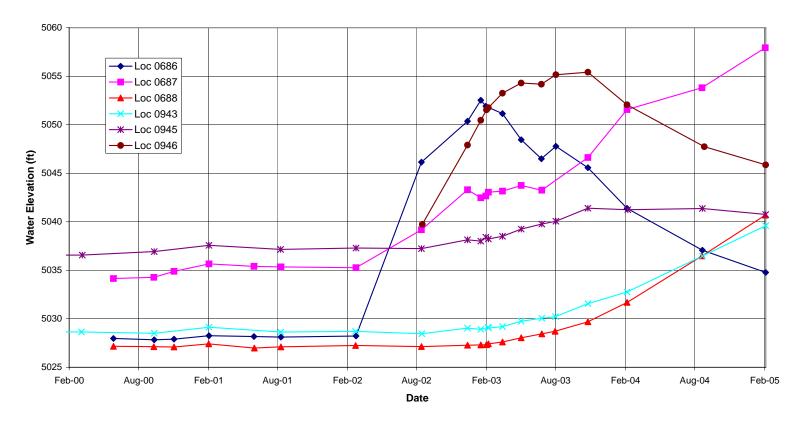
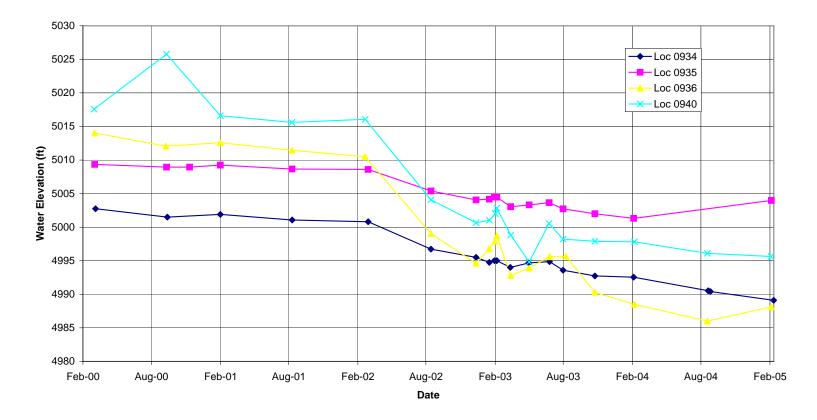
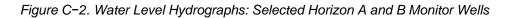


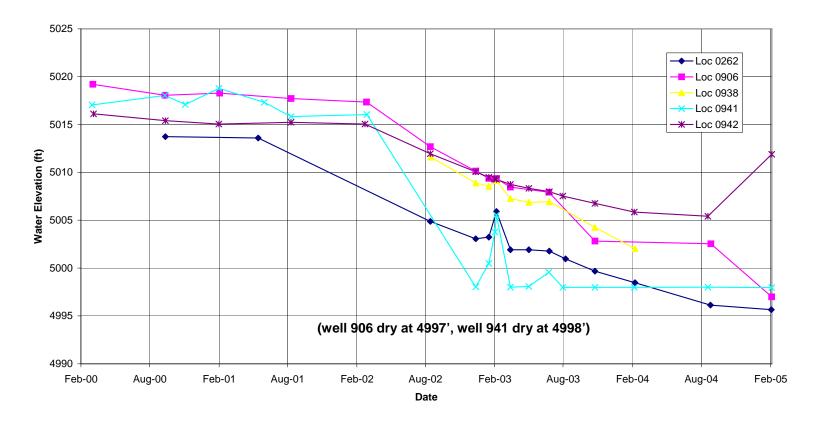
Figure C-1. Water Level Hydrographs: Monitor Wells at Infiltration Trench













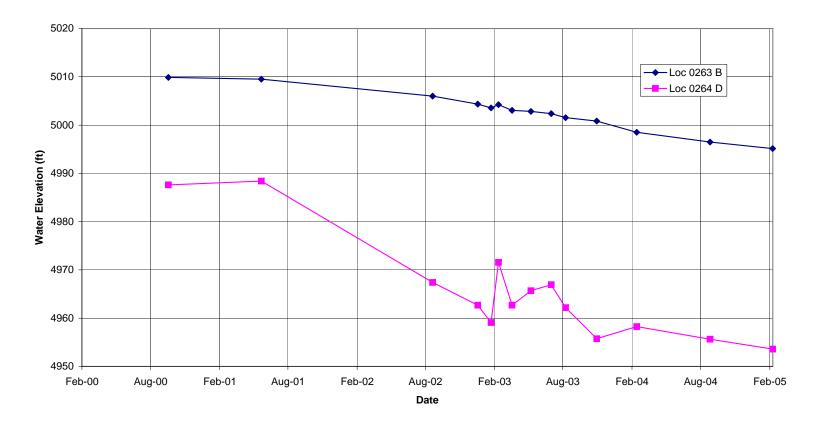
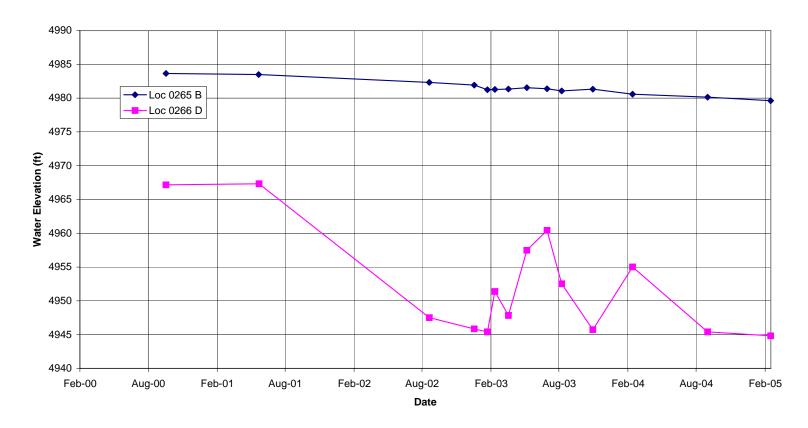
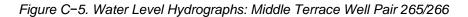


Figure C-4. Water Level Hydrographs: Middle Terrace Well Pair 263/264









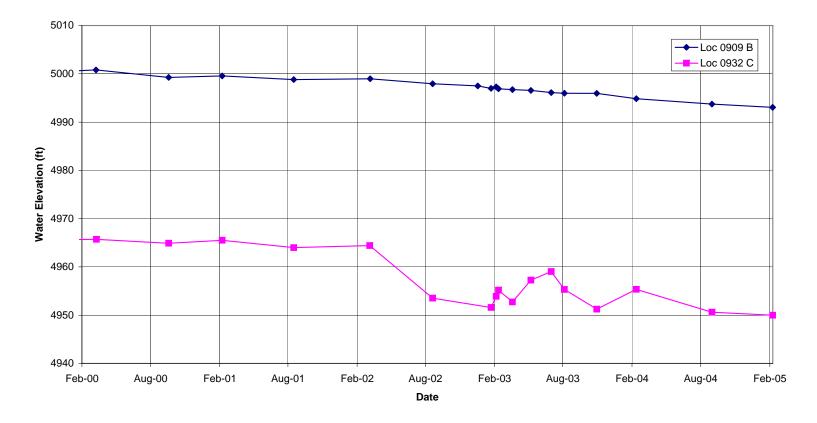
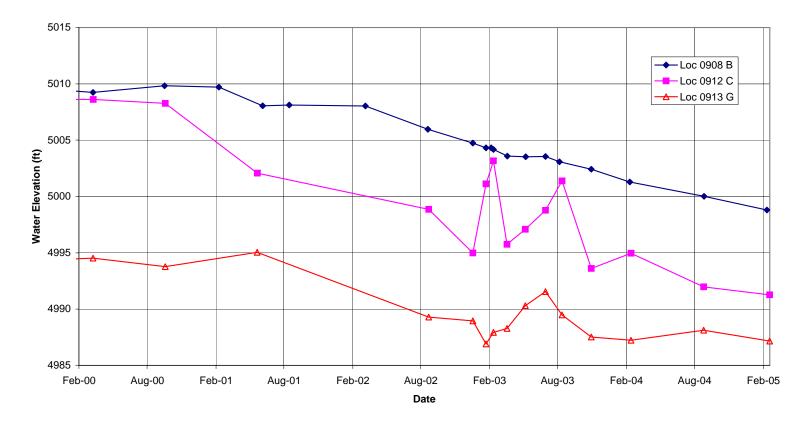


Figure C-6. Water Level Hydrographs: Middle Terrace Well Pair 909/932







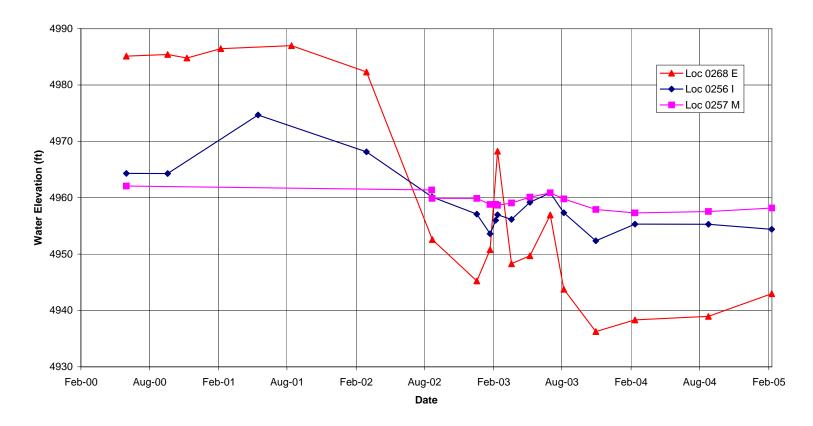
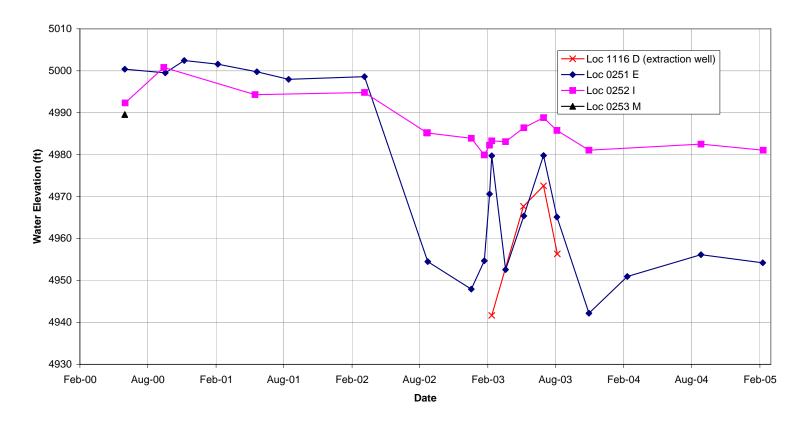


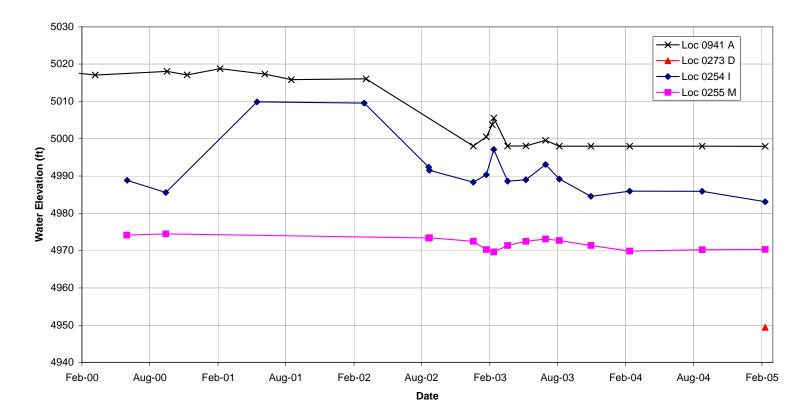
Figure C-8. Water Level Hydrographs: Middle Terrace Well Cluster 268/256/257

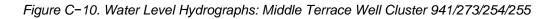




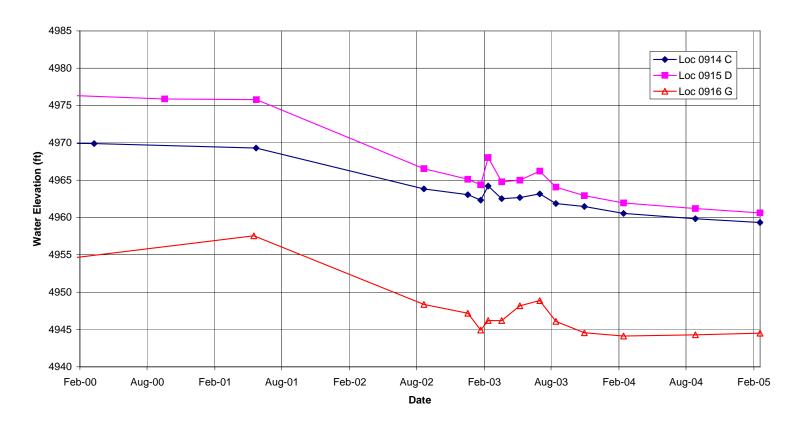
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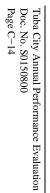












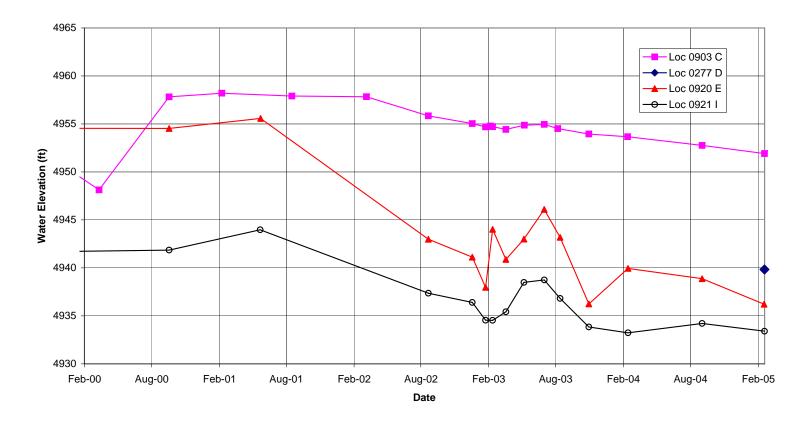


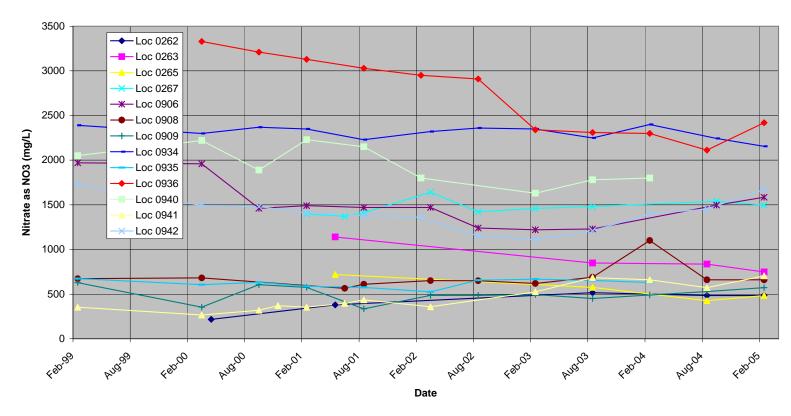
Figure C-12. Water Level Hydrographs: Lower Terrace Well Cluster

Appendix D

**Contaminant Concentration Trends at Monitor Wells** 

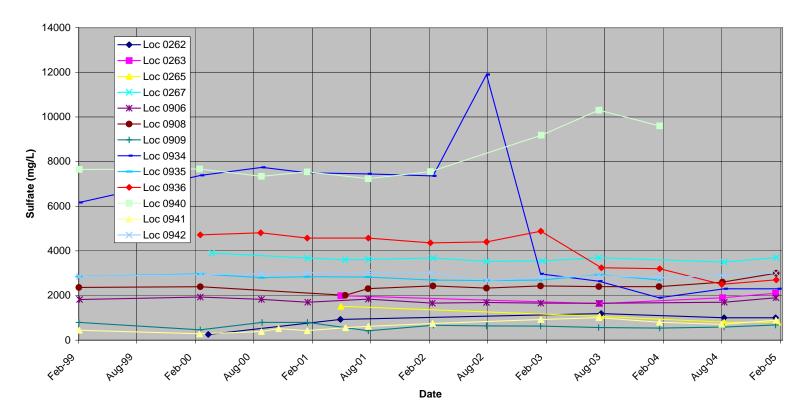
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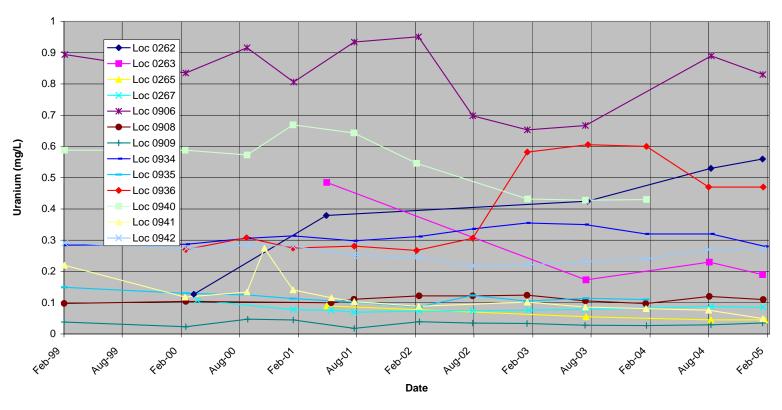




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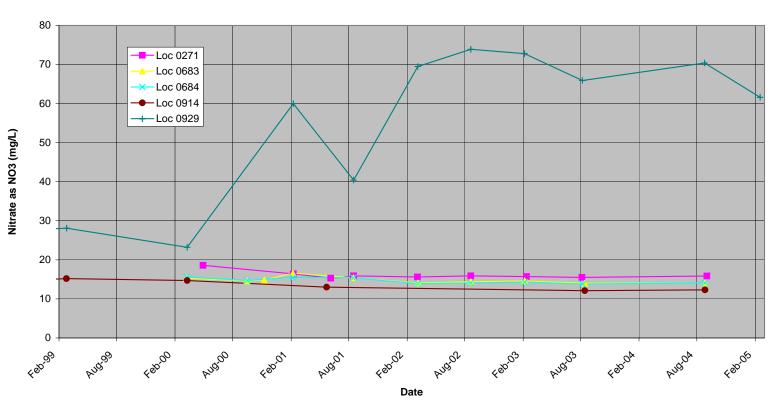


D-2. Horizons A and B Monitor Wells, Sulfate Concentration

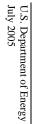


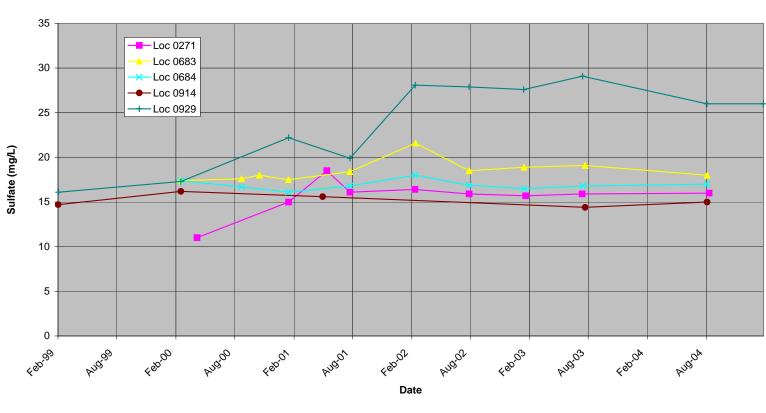
D-3. Horizons A and B Monitor Wells, Uranium Concentration





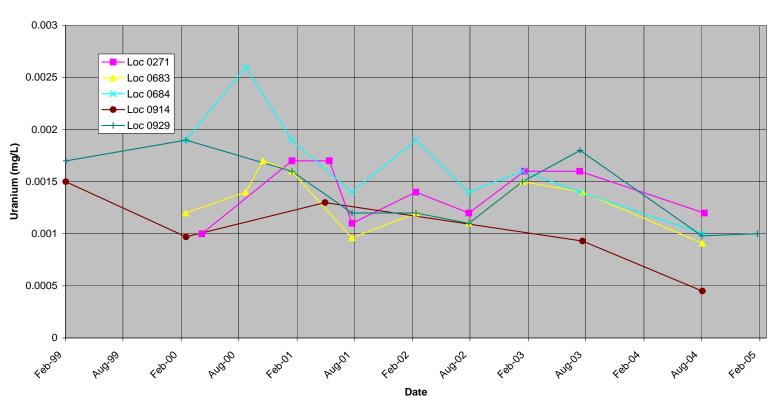
D-4. Horizons A and B Sentinel Wells, Nitrate as NO<sub>3</sub> Concentration



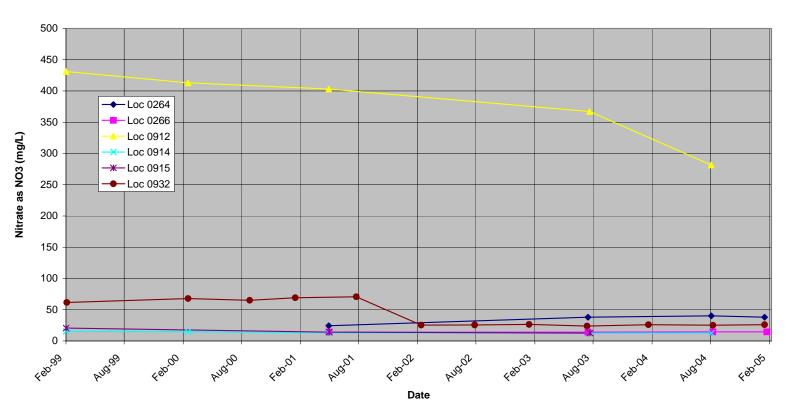


D-5. Horizons A and B Sentinel Wells, Sulfate Concentration

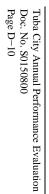


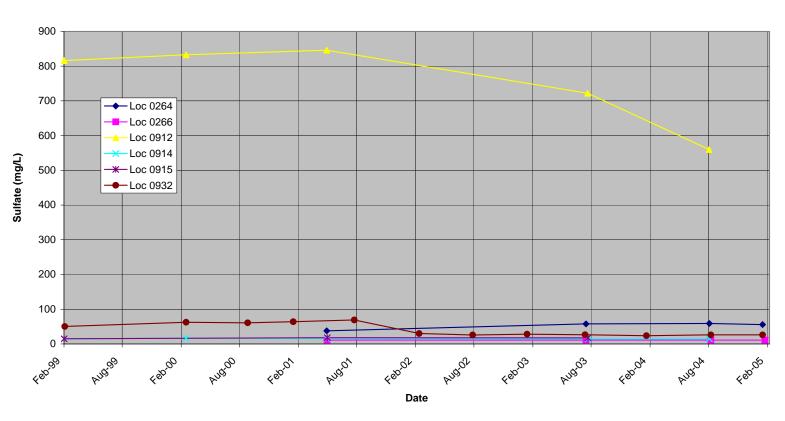


D-6. Horizons A and B Sentinel Wells, Uranium Concentration

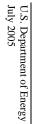


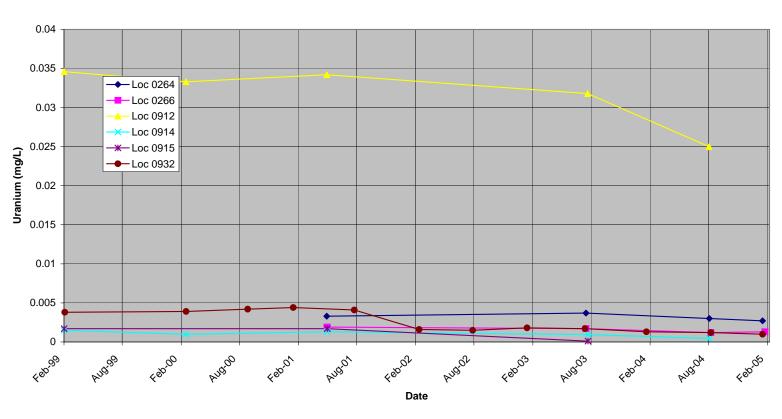
D-7. Horizons C and D Monitor Wells, Nitrate as NO<sub>3</sub> Concentration





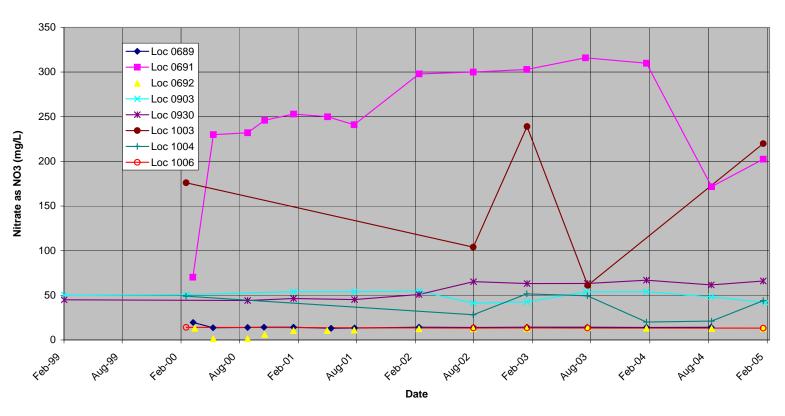
D-8. Horizons C and D Monitor Wells, Sulfate Concentration





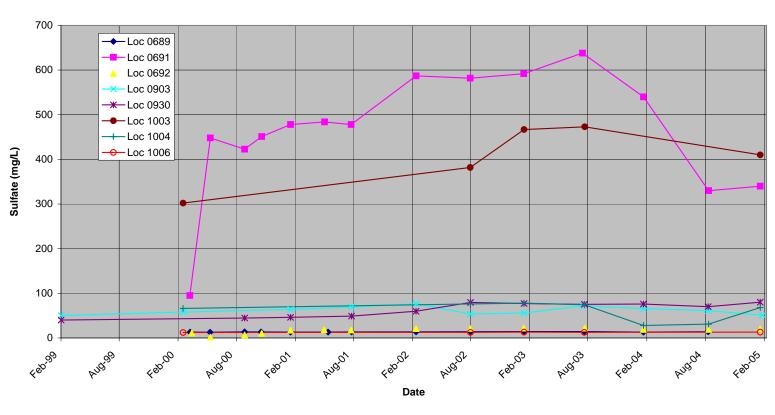
D-9. Horizons C and D Monitor Wells, Uranium Concentration





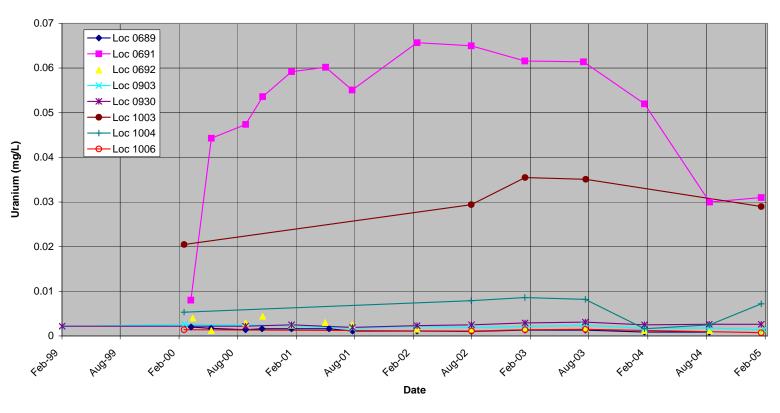
D-10. Lower Terrace Monitor Wells, Nitrate as NO<sub>3</sub> Concentration



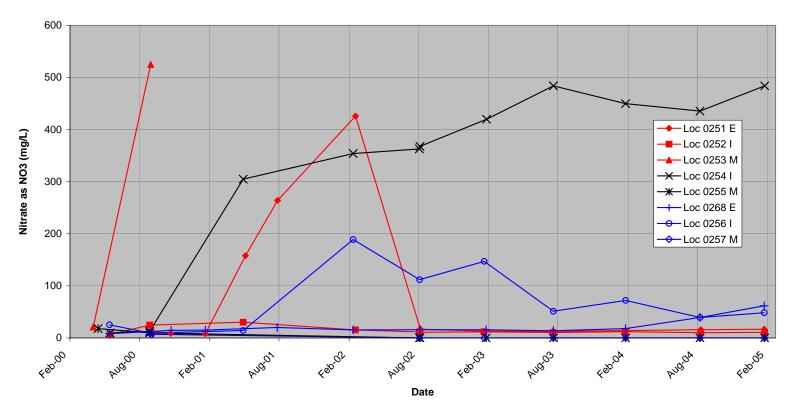


D-11. Lower Terrace Monitor Wells, Sulfate Concentration

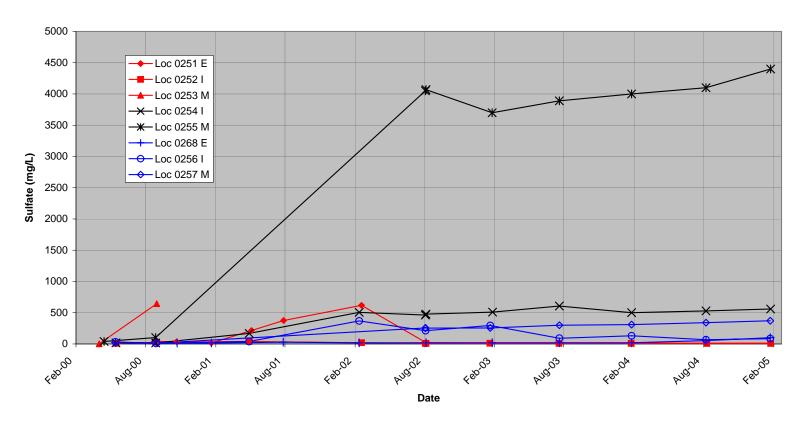




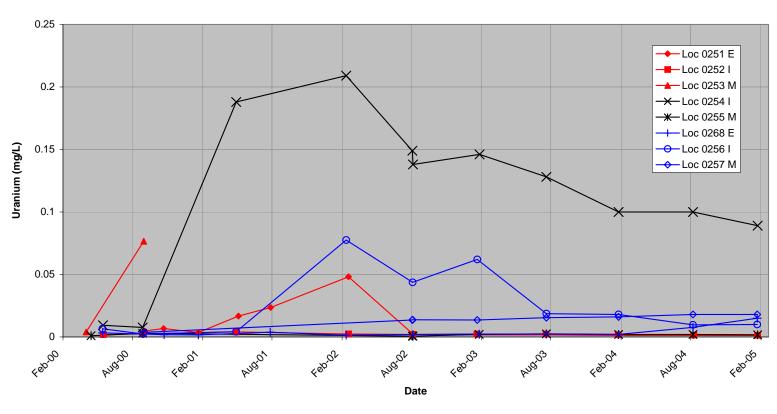
D-12. Lower Terrace Monitor Wells, Uranium Concentration



D-13. Deep Monitor Wells, Nitrate as NO<sub>3</sub> Concentration



D-14. Deep Monitor Wells, Sulfate Concentration



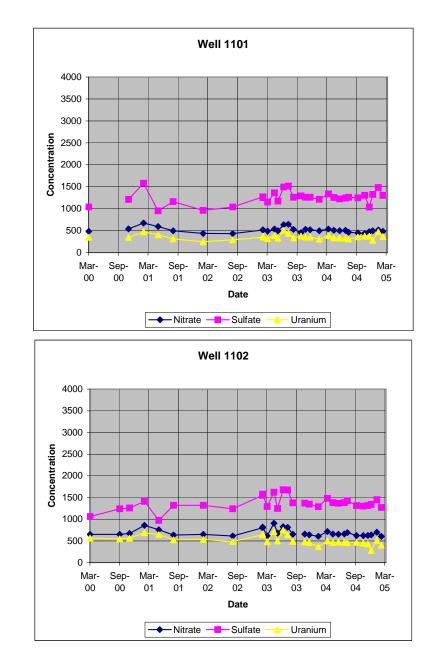
D-15. Deep Monitor Wells, Uranium Concentration

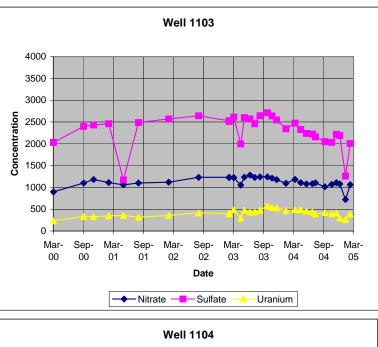
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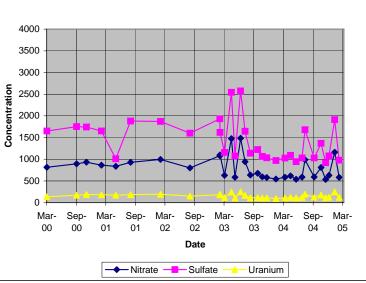
Appendix E

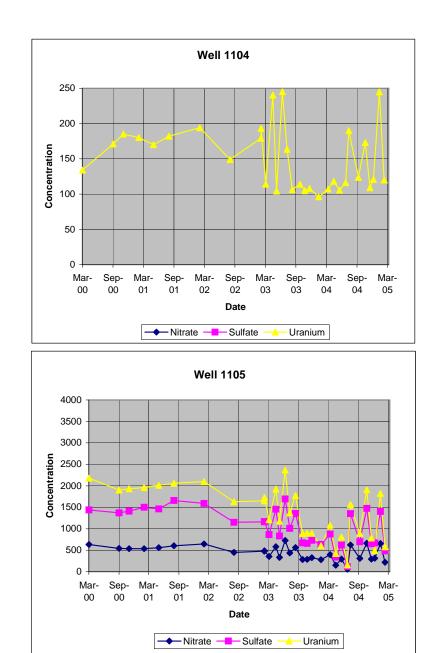
**Contaminant Concentrations at Extraction Wells** 

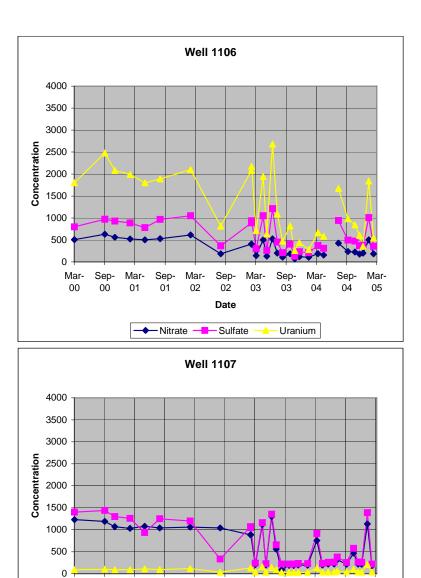
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Sep-

00

Mar-

00

Mar-

01

Sep-

01

Mar-

02

→ Nitrate → Sulfate

Sep-

02

Date

Mar-

03

Sep-

03

- Uranium

Mar-

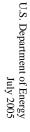
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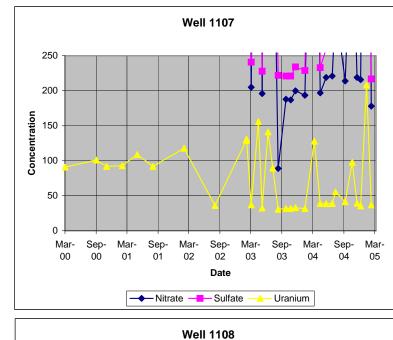
Sep-

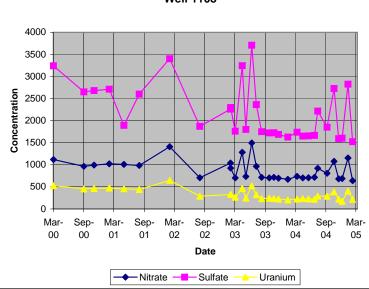
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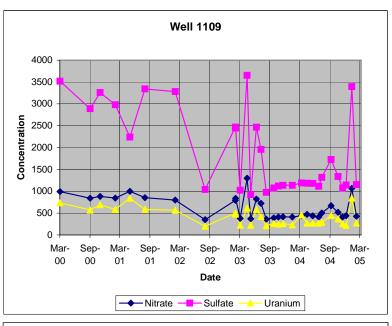
Mar-

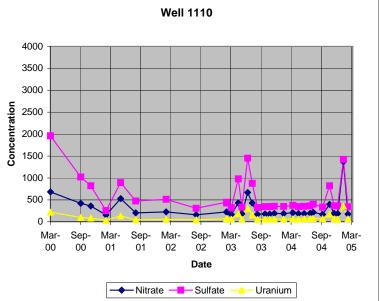
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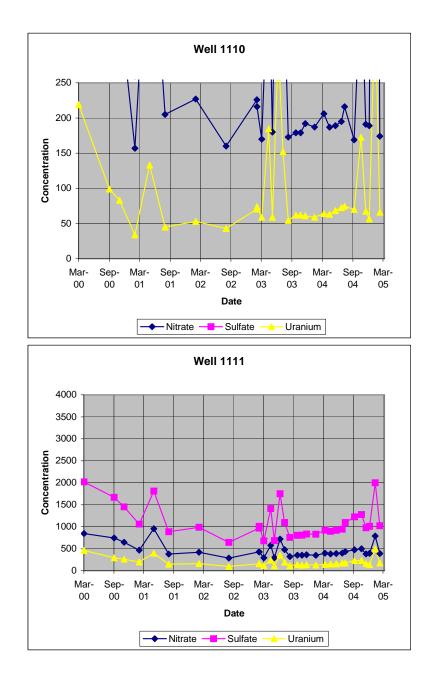


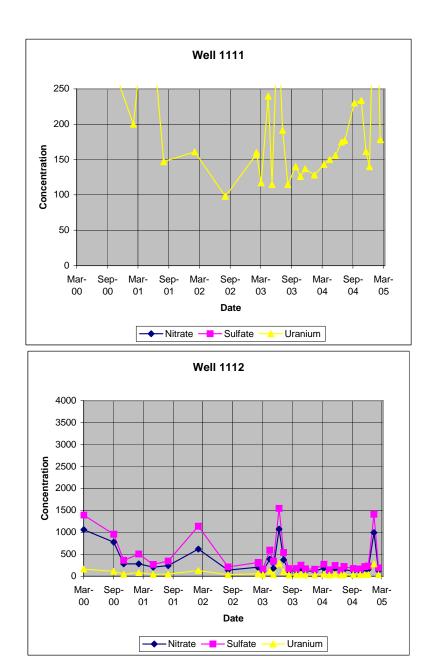




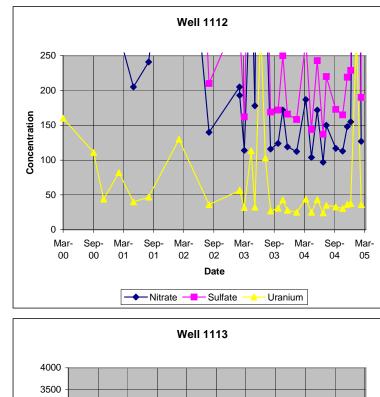


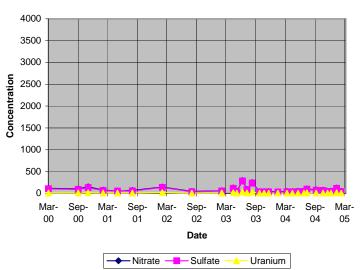


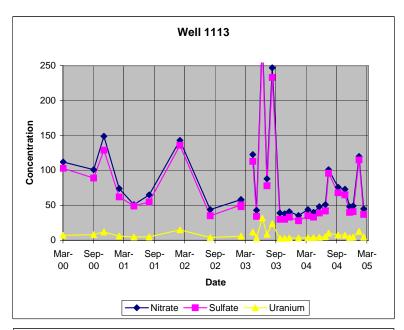


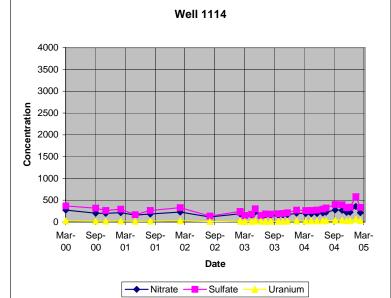


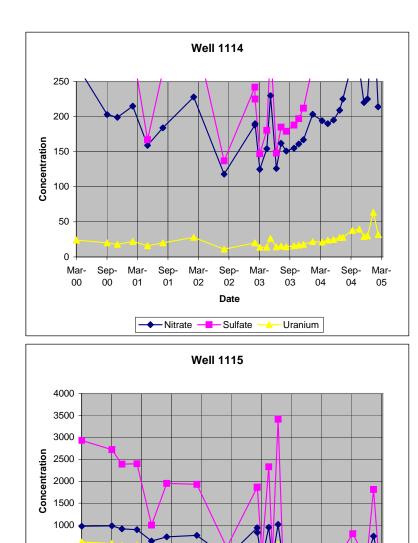
U.S. Department of Energy July 2005

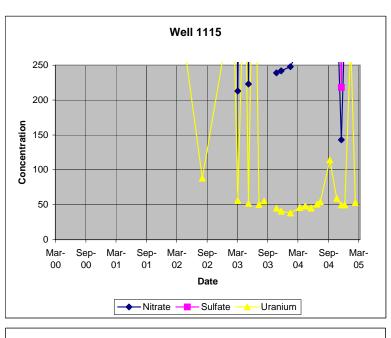


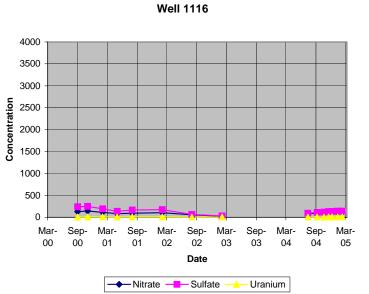












500

0

Mar-

00

Sep-

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01

Mar- Sep- Mar-

01

Sep-

02

Date

02

→ Nitrate → Sulfate

Mar-

03

Sep-

03

Uranium

Mar-

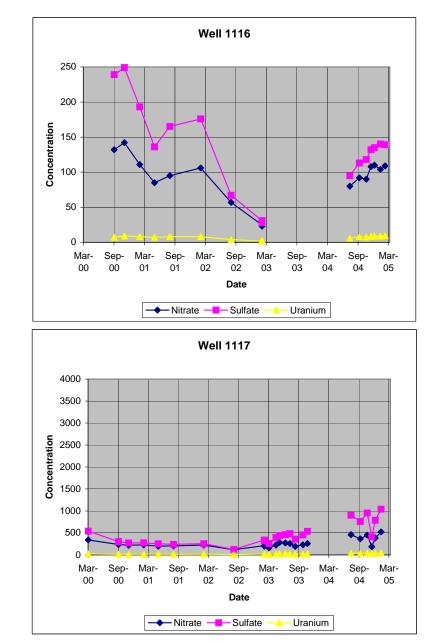
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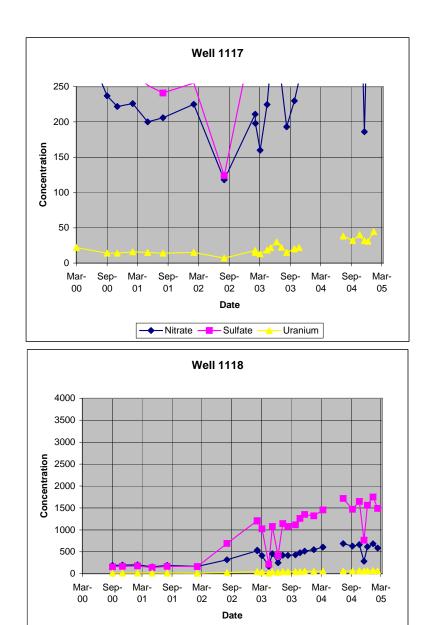
Sep-

04

Mar-

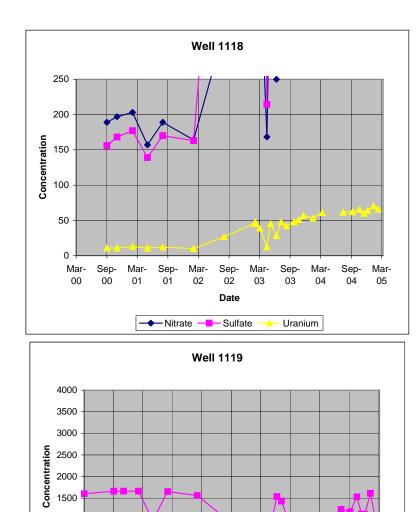
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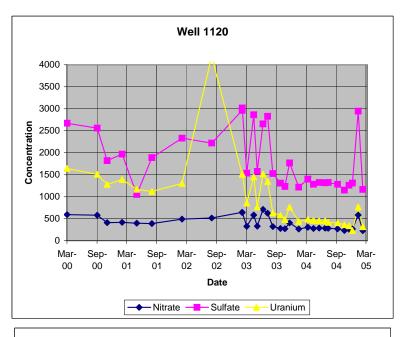


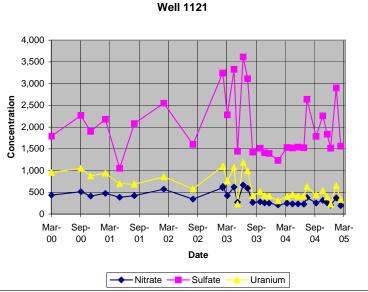


Nitrate — Sulfate

Uranium







1000

500

0

Mar-

00

Sep-

00

Sep-

01

Mar-

01

Sep-

02

Date

Mar-

03

Sep-

03

Uranium

Mar-

04

Mar-

02

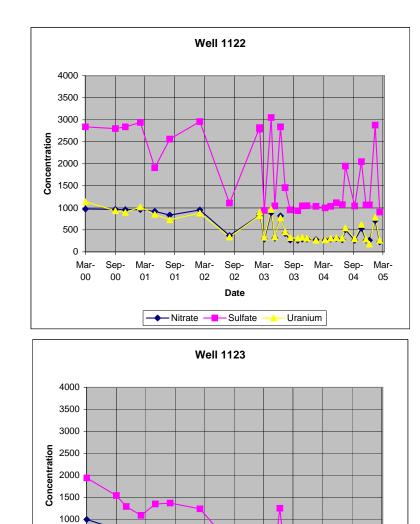
Nitrate — Sulfate

Sep-

04

Mar-

05



Sep-

03

Uranium

Mar-

04

Mar-

03

Sep-

04

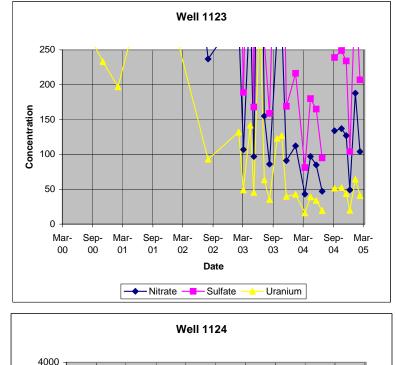
Mar-

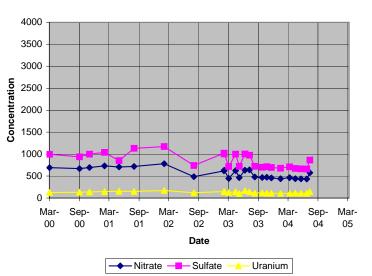
05

Sep-

02

Date





500

0

Mar-

00

Sep-

00

Mar-

01

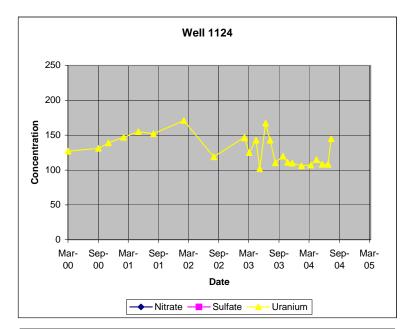
Sep-

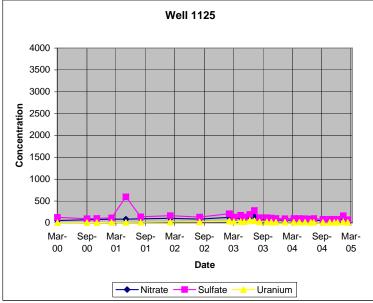
01

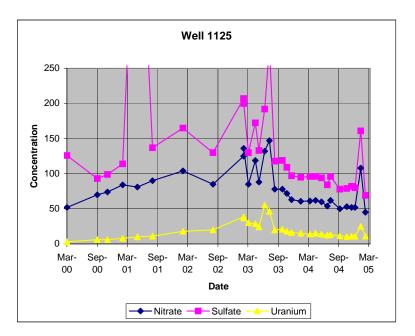
Mar-

02

→ Nitrate → Sulfate







## Appendix F

**Estimated Initial Mass of Dissolved Contamination and Initial Volume of Contaminated Ground Water**  This page intentionally left blank

## **Calculation** Set **Tuba City Site**

Year 2005 Annual Performance Evaluation Report Period of Review: March 2004 through March 2005

11

Objective: estimate the baseline volume of contaminated groundwater of the Middle Terrace; estimate the baseline mass of dissolved nitrate, sulfate, and uranium in the groundwater

Method:

1) estimate the area of the plume from baseline contaminant maps separately for Horizons A and B combined and Horizons C and D combined

a) estimate the vertical thickness of contamination for Horizons A and B combined and Horizons C and D combined
a) assume 25% porosity and compute the separate plume volumes for Horizons A and B combined and Horizons C and D combined
compute separate concentration averages for sulfate and uranium for Horizons A and B combined and Horizons C and D combined from baseline contaminant maps

5) multiply concentration average by plume volume to determine contaminant mass for Horizons A and B combined and Horizons C and D combined 6) sum the volume and mass estimates

## Calcualtion:

1:											
	1) man a	rea of cont	aminant plume								
	Horizons	A and B	plume length (n	ortheast to south							
			plume width		1,800 ft						
			area		7,200,000 ft^2						
	Horizons	C and D	plume length (ne	ortheast to south	west 2,500 ft						
			plume width		1,800 ft						
			area		4,500,000 ft^2						
		10.160.0									
		ess of cont									
	Horizons	A and B	25	ft		Horizo	ons C and D				
	thickness	Horizon A	50	ft		thickn	ess Horizon C	50	ft		
		Horizon B	75				ess Horizon D	25			
		bined thickr					combined thickness	75			
				on A not optimate	ed during baseline period						
				on A not saturate	ed during baseline period		re thickness of Horizon			and a start of the	
	Honzor	n B is fully sa	aturated			Hon	izon D not contaminate	d at many lo	cations, assun	ne 50% contamina	ted thickness
		Sec.									
		volumes									
	Horizons	A and B	volume of contai	minated groundy	water 135,000,000 ft^3		135,000,000 ft^3				
					1,012,500,000 gal	1.0	013,000,000 gal				
					3,832,312,500 L		832,000,000 L				
						-,-	Contraction of the				
	Horizons	C and D	volume of contai	minated around	water 28,125,000 ft^3		28,000,000 ft^3				
			and the or soliton	giounda							
					210,937,500 gal		211,000,000 gal				
					798,398,438 L		798,000,000 L				
		و المنظر المراجع									
		ne concent	rations			11.2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
	Horizons		and a second	And the second	Same And		ons C and D				
	well	Horizon	U mg/L		nitrate mg/L as NO3	well	Horizon		sulfate mg/L	N mg/L as NO3	
	262	в	0.379	931	380	1101	D	0.245	960	438	
	263	в	0.485	1990	1140	1102	D	0.533	1320	650	
	265	в	0.090	1520	720	1103	D	0.355	2570	1120	
	267	в	0.073	3680	1640	1104	D	0.194	1870	993	
	906	A									
			0.951	1660	1470	1105	D	2.100	1590	648	
	908	в	0.122	2430	651	1106	D	2.100	1050	614	
	909	в	0.040	666	485	1107	D	0.118	1200	1060	
	934	B	0.312	7360	2320	1108	D	0.646	3400	1410	
	936	в	0.267	4360	2950	1109	D	0.565	3280	798	
	940	A	0.546	7550	1800	1110	D	0.053	512	227	
	941	A	0.089	745	358	1111	D	0.161	988	421	
	942	В	0.246	3030	1360		D				
	944	B	0.950	1590		1112		0.130	1140	617	
					1010	1113	D	0.053	250	143	
	geometric	: mean mg/L	0.231	2174	1028	1114	D	0.040	328	228	
						1115	D	0.410	1930	766	
						1116	D	0.040	250	106	
						1117	D	0.040	255	225	
						1118	D	0.040	250	164	
						1119	D	0.555	1560	468	
						1120	D				
								1.3	2330	493	
						1121	D	0.849	2590	535	
						1122	D	0.878	2960	954	
						1123	D	0.261	1240	643	
						1124	D	0.171	1170	781	
						1125	D	0.04	250	104	
						912	c	0.04	846	403	
							geometric mean mg/L		1020	464	
							geomotio moan mg/L	0.2.14	1020	404	
	5) maes	calculation				61 4-4	al valuma and martin				
	Horizons			004			al volume and masse				
	Horizons	A and B	mass uranium	884 kg		total	volume contaminated	groundwat	er	163,000,000	
			100.000 A 100.00	1,949 lb						1,222,500,000	
			mass sulfate	8,330,201 kg						4,627,162,500	L
				18,359,764 lb							
			mass N as NO3	3,940,636 kg	3	total	mass uranium			1,055	kg
				8,685,162 lb						2,326	
										-1020	
	Horizons	C and D	mass uranium	171 kg	1	total	mass sulfate			9,144,511	ka
		2 4114 6		377 lb		Istal	inado ounate				
			mass sulfate	814,310 kg						20,154,502	in .
			mass sunate	014,510 Kg	1						

total mass nitrate as NO3

mass sulfate 1,794,738 lb 370,337 kg 816,223 lb mass N as NO3

4,310,973 kg

9,501,384 lb

Calculation	Set						I a second a second		
<b>Tuba City S</b>	ite								
	ormance Evalu	ation Report							
		004 through March 200	5						
i chica of ita	Them indicated								
Objective:	estimate aquifer	cleanup times							
						1			
Method:	compare mass a	nd volume removed as of A	April 1, 2005 to esti	mates of initial contami	nant inventory; pred	ict cleanup time calculated	d removal rates to date		
Calculation:		al contaminant volume and							
	estimate #2: initia	al contaminant volume and	mass estimates re	calculated for March 20	004 - March 2005 Pe	orformance Evaluation Re	port		
Estimate #1									1
	initial mass lb	cumulative removed lb	% removed		initial vol gal	cumulative removed gal	# pore vols removed	% plume vol removed	
Nitrate	12,400,000	459,000	4		3.40E+09			4	
Suifate	17,900,000	1,123,000	6		2.70E+09	135,900,000	0.050	5	
Uranium	2,800	325	12		3.00E+09	135,900,000	0.045	5	
	1								
	mass removal			# yrs		pore volume	1-pore volume	1-pore volume	#
	rate % per yr	cleanup time, yrs	cleanup date	until cleanup		removal rate % / yr		cleanup date	
Nitrate	1.3	76	2078	73		1.4	70	2072	until oroun
Sulfate	2.2	45	2047	42		1.8	56	2058	
Uranium	4.1	24	2026	21		1.6	62	2064	
t1=	15-Jun-02					1			
t2=	01-Apr-05								
t2 - t1=	2.8	yrs							
Estimate #2									
Lounde HL	initial mass lb	cumulative removed lb	% removed		initial vol gal	cumulative removed gal	# pore vols removed	% nlume vol removed	
Nitrate	9,500,000	459,000	5		1.20E+09	135,900,000		11	
Sulfate	20,000,000	1,123,000	6		1.20E+09		0.113	11	
Uranium	2,300	325	14		1.20E+09		0.113	11	
	mass removal			# yrs		pore volume	1-pore volume	4	
Projection	rate % per yr	cleanup time, yrs	cleanup date	until cleanup		removal rate % / yr	cleanup time, yrs	1-pore volume cleanup date	# until clear
Nitrate	1.7	58	2060	55		4.0	cleanup unie, yrs	2027	unui ciea
Sulfate	2.0	50	2052	47		4.0	25	2027	
Uranium	5.1	20	2022	17		4.0	25	2027	
t1=	15-Jun-02		LULL			4.0	20	2021	
t2=	1-Apr-05								
t2 - t1=		Vire							

Appendix G

Aquifer Restoration Index Calculation

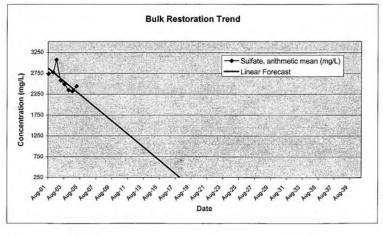
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Calculation Set Tuba City Site Annual Performance Evaluation Report Period of Review: March 2004 through March 2005

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Objective:	develop a	bulk concentra	ation index for	measuring	restoration	progress fo	or sulfate								
Method:		e an average o e the compute			ninant for a	given samp	ling date/e	vent for a s	elected gro	oup of monit	or wells wit	hin the cont	aminant plume		
Calculation:	no historica	ne selected monitor wells below have the most comprehensive data set and are located throughout the contaminant plume in Horizons A and B; o historical data exists for Horizons C and D within the contaminant plume ote: where data are absent in the table below, concentrations are carried forward from the previous date as shown in <b>bold italic</b>													
	Sulfate (m	ng/L)												Sulfate,	Sulfate,
date_sampled	Loc 0262	Loc 0263 Lo	oc 0265	Loc 0267	Loc 0906	Loc 0908	Loc 0909	Loc 0929	Loc 0934	Loc 0936	Loc 0940	Loc 0941	Loc 0942	arithmetic mean (mg/L)	geometric mean (mg/L)
08/16/2001	931	1990	1520	3620	1840	2310	419	19.9	7450	4570	7230	620	3030 baseline	2735	1482
03/06/2002	931	1990	1520	3680	1660	2430	666	28.1	7360	4360	7550	745	3030 baseline	2765	1594
08/20/2002	931	1990	1520	3530	1690	2330	637	27.9	11900	4400	7550	745	2680	3072	1625
02/06/2003	931	1990	1520	3550	1660	2430	629	27.6	2970	4880	9180	920	2790	2575	1524
08/06/2003	1190	1640	1070	3690	1650	2400	564	29.1	2640	3240	10300	1010	2890	2486	1453
02/12/2004	1190	1640	1070	3690	1650	2400	540	29.1	1900	3200	9600	800	2800	2347	1375
08/31/2004	1000	1900	800	3500	1700	2600	590	26	2300	2500	9600	710	2900	2317	1331
02/10/2005	1000	2100	810	3700	1900	3000	680	26	2300	2700	9600	890	3000	2439	1426



250			Sulfate, geometric mean (mg/L)
750			-Linear Forecast
250			
750			
150	$\sim$		
50	$\sim$		
250		$\sim$	

21 yr 18 yr

t1=	15-Jun-02		t1= 15-Jun-02
t2=	1-Apr-05		t2= 1-Apr-05
t2 - t1=	2.8 yr		t2 - t1 = 2.8 yr
t3=	Aug-18		t3= Aug-23
projected cleanup time from t1=		16 yr	projected cleanup time from t1=
projected cle	eanup time from t2=	13 yr	projected cleanup time from t2=

U.S. Department of Energy July 2005

Calcula	tion Set															
Tuba Ci																
		nance Eva	luation	Report												
				rough Ma	rch 2005											
Objectiv	e: d	ievelop a b	ulk conce	ntration inde	ex for meas	suring resto	ration prog	ress for ura	anium							
Method:		() compute	an averar	ne concentr	ation of a c	ontaminant	for a giver	samoling	date/event t	for a select	ed aroup of	monitor we	alls within th	e contaminant plume		
Method.				uted average			TOT & given	i ocampang			ou group of					
Calculati	n	no historical	I data exis	sts for Horiz	ons C and	D within the	e contamina	ant plume				minant plun hown in <b>bo</b>		ns A and B;		
		Jranium m		absolution											Uranium,	Uranium,
date sar				Loc 0265	Loc 0267	Loc 0906	Loc 0908	Loc 0909	Loc 0929	Loc 0934	Loc 0936	Loc 0940	Loc 0941	Loc 0942	arithmetic mean (mg/L)	geometric mean (mg/L)
08/16/20	01	0.3790	0.4850	0.0897	0.0696	0.9340	0.1110	0.0178	0.0012	0.2980	0.2810	0.6430	0.1030	0.2510 baseline	0.2818	0.1316
03/06/20	02	0.3790	0.4850	0.0897	0.0731	0.9510	0.1220	0.0389	0.0012	0.3120	0.2670	0.5460	0.0886	0.2460 baseline	0.2769	0.1378
08/20/20	02	0.3790	0.4850	0.0897	0.0742	0.6980	0.1220	0.0349	0.0011	0.3360	0.3060	0.5460	0.0886	0.2180	0.2599	0.1336
02/06/20	03	0.3790	0.4850	0.0897	0.0765	0.6530	0.1240	0.0333	0.0015	0.3550	0.5820	0.4320	0.1020	0.2210	0.2718	0.1428
08/06/200	03	0.4250	0.1730	0.0551	0.0784	0.6670	0.1060	0.0279	0.0018	0.3500	0.6060	0.4280	0.0858	0.2320	0.2489	0.1261
02/12/20	04	0.4250	0.1730	0.0551	0.0784	0.6670	0.0970	0.0270	0.0018	0.3200	0.6000	0.4300	0.0810	0.2400	0.2458	0.1238
08/31/20	04	0.5300	0.2300	0.0450	0.0880	0.8900	0.1200		0.0010	0.3200	0.4700	0.4300	0.0760	0.2700	0.2692	0.1256

0.2800

0.4700

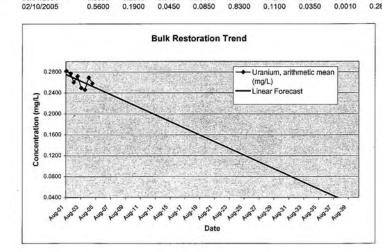
0.4300

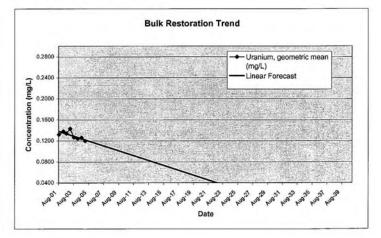
20 yr

17 yr

0.0490

0.2700





. . .

0.2581

0.1191

t1=	15-Jun-02		t1=	15-Jun-02	
t2=	1-Apr-05		t2=	1-Apr-05	
t2-t1=	2.8 yr		t2 - t1=	2.8 yr	
t3=	Aug-37		t3=	Aug-22	
	anup time from t1= 35 yr anup time from t2= 32 yr		projected cleanup time from t1= projected cleanup time from t2=		
projectou ch	carlop arrie from az-	52 9	projociou		

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