



LTSM012581

LBLS 21.00

US Army Corps of Engineers® Buffalo District



# FOR THE BLISS & LAUGHLIN SITE

**BUFFALO, NEW YORK** 

**SEPTEMBER 1998** 

RECORD COPY

## TABLE OF CONTENTS

.

)

1

)

,

REMEDIAL INVESTIGATION, FEASIBILITY STUDY, AND PROPOSED PLAN FOR THE BLISS & LAUGHLIN SITE	l
1. INTRODUCTION       3         1.1 OVERVIEW OF FUSRAP       3         1.2 BACKGROUND       3         1.3 PURPOSE       3         1.4 SITE DESCRIPTION AND SETTING       4	3
2. SITE CHARACTERIZATION RESULTS	5
3. IDENTIFYING AND EVALUATING CLEANUP OPTIONS       3.1         3.1 DESCRIPTION OF ARARs AND TBCs.       3.1.1 Authority         3.1.2 Applicable or Relevant and Appropriate Requirements (ARARs)       3.1.3         3.1.3 To be Considered (TBCs)       10         3.1.4 Other Requirements       10         3.2 SUMMARY OF SITE RISKS       10         3.3 DESCRIPTION OF ALTERNATIVES       13         3.3.1 Alternative 1: No Action       13         3.3.2 Alternative 2: Continued Institutional Controls       13         3.3.3 Alternative 3: Decontamination of Buildings       14	9 9 0 0 0 1 1 1
4. EVALUATION OF ALTERNATIVES       14         4.1 EVALUATION CRITERIA       14         4.2 EVALUATION OF ALTERNATIVES       16         4.2.1 Overall Protection of Human Health and the Environment       16         4.2.2 Compliance with Federal and State Environmental Regulations       17         4.2.3 Long-Term and Short-Term Effectiveness and Permanence       17         4.2.4 Reduction in Toxicity, Mobility, or Volume through Treatment       1         4.2.5 Implementability       1         4.2.6 Cost       1         4.2.7 State and Community Acceptance       2	4667788920
5. SELECTION OF THE PREFERRED ALTERNATIVE	!1
6. COMMUNITY ROLE IN THE SELECTION PROCESS	
7. REFERENCES	
Appendix A BLISS AND LAUGHLIN STEEL CHARACTERIZATION RESULTS A-	
Appendix B COST ESTIMATEB-	-1



## LIST OF FIGURES

,

)

Ļ

,

,

,ł

1

)

Figure	Page
1. Bliss and Laughlin Steel with Reference Grids and Survey Locations	6
2. Overheads Above Special Finishing Area with Survey Locations	
3. Detail of Special Finishing Area with Survey Results and Sampling Locations	8

### LIST OF TABLES

Table	
1 Summary of CERCLA Evaluation Criteria	15

# ACRONYMS AND ABBREVIATIONS

AEC	Atomic Energy Commission
ALARA	As Low As Reasonably Achievable
ARAR	Applicable or Relevant and Appropriate Requirements
BNI	Rechtel National, Incorporated
CERCLA	Comprehensive Environmental Response, Compensation, and Liability Act
CFR	Code of Federal Regulations
cm <sup>2</sup>	square centimeter(s)
COC	Contaminant(s) of Concern
су	cubic yards
DOE	Department of Energy
DOT	Department of Transportation
dpm	disintegrations per minute
ÊE/CA	Engineering Evaluation/Cost Analysis
EPA	Environmental Protection Agency
FUSRAP	Formerly Utilized Sites Remedial Action Program
g	gram(s)
hr	hour
km	kilometer(s)
LOOW	Lake Ontario Ordnance Work
μR	micro Roentgen(s)
m	meter(s)
MED	Manhattan Engineer District
mrem	millirem
NRC	Nuclear Regulatory Commission
NYCRR	New York Codes, Rules, and Regulations
NYSDEC	New York State Department of Environmental Conservation
ORISE	Oak Ridge Institute for Science and Education
ORNL	Oak Ridge National Laboratory
OSWER	Office of Solid Waste and Emergency Response
pCi	picoCuries
Ra	radium
RCRA	Resource Conservation and Recovery Act
RI	Remedial Investigation
SAIC	Science Applications International Corporation
TAGM	Technical Administrative Guidance Memorandum
TBC	To Be Considered
TCLP	Toxicity Characteristic Leaching Procedure
TEDE	Total Effective Dose Equivalent
Th	thorium
U	uranium
USACE	United States Army Corps of Engineers
USEPA	United States Environmental Protection Agency



ļ

)

.

. '

)



### UNITED STATES ARMY CORPS OF ENGINEERS REMEDIAL INVESTIGATION, FEASIBILITY STUDY, AND PROPOSED PLAN FOR THE BLISS & LAUGHLIN SITE BUFFALO, NEW YORK

The United States Army Corps of Engineers (USACE) is conducting the project at the Bliss & Laughlin Site in Buffalo, New York in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act, 42 United States Code 9601et seq. (CERCLA).

On October 13, 1997, the Energy and Water Development Appropriations Act, 1998 was signed into law as Public Law 105-62. Pursuant to this law, the Formerly Utilized Sites Remedial Action Program (FUSRAP) was transferred from the U.S. Department of Energy to the USACE. Under its authority to conduct the Formerly Utilized Sites Remediation Program, the USACE prepared this Remedial Investigation, Feasibility Study, and Proposed Plan for the Bliss & Laughlin Site. The Remedial Investigation, Feasibility Study, and Proposed Plan addresses contamination resulting from operations conducted for the Atomic Energy Commission (AEC). Bliss & Laughlin Steel Company performed machining and straightening operations on uranium rods. The machined rods and turnings were then shipped off-site.

Three alternatives were considered for addressing residual radioactive contamination at the Bliss and Laughlin site. The first Alternative, No Action, assumes the site is abandoned and current institutional controls to limit exposure are lifted. The second alternative, Continuation of Institutional Controls, includes no remediation but continues the use of the site as an industrial facility with periodic monitoring and review. The third, Decontamination of Buildings, would use various decommissioning technologies to remove contamination from the surfaces inside of the buildings to preclude human exposure in areas of elevated radioactivity. Building rubble that exceeded the release criteria would be shipped to an appropriate licensed or permitted disposal facility. Material that does not exceed the release criteria would be left on site or sent to an appropriate disposal facility.

USACE does hereby propose that the final remedial action for the Bliss & Laughlin Site be Alternative 3, Decontamination of Buildings. The alternative is fully protective of human health and the environment, complies with the applicable or relevant and appropriate requirements, and is considered by the USACE to best meet the criteria prescribed by CERCLA, as amended, and the National Contingency Plan (NCP).

USACE invites members of the public to review the proposed plan and the supporting documents which further describe the conditions at the Bliss & Laughlin Site and the basis for the proposal. Those documents may be found in the administrative record for the Bliss & Laughlin Site at the Buffalo and Erie County Public Library-Dudley Branch, 2010 South Park Avenue, Buffalo, New York, 14220, and at the USACE FUSRAP Public Information Center, 1776 Niagara Street, Buffalo, NY, 14207. Members of the public who wish to comment upon this proposed plan may submit their comments to USACE at the following address:



U.S. Army Corps of Engineers Buffalo District FUSRAP Public Information Center 1776 Niagara Street Buffalo, NY 14207-3199

Please refer to this proposed plan or to the Bliss & Laughlin Site in the comments. All comments will be reviewed and considered by USACE in determining the final remedy for the Bliss & Laughlin Site. Comments should be submitted no later than 30 days after the date of this proposed plan.

After the close of the comment period, USACE will review all public comments, as well as the information contained in the Administrative Record file for this site, and any new information developed or received during the course of this comment period, in light of the requirements of CERCLA and the NCP. An authorized official of USACE will then make a final selection of the remedial action to be conducted at this site. This decision will be documented in a Record of Decision, which will be issued to the public, along with a response to all comments submitted regarding this proposed plan.

### **1. INTRODUCTION**

### **1.1 OVERVIEW OF FUSRAP**

This document describes the results of testing and analysis performed and cleanup options for the Bliss & Laughlin site. The site is being addressed under the United States Army Corps of Engineers (USACE) Formerly Utilized Sites Remedial Action Program (FUSRAP). The U.S. Atomic Energy Commission (AEC), a predecessor of the Department of Energy (DOE), established FUSRAP in 1974 to identify, investigate, and remediate or control sites contaminated as a result of activities performed as part of the nation's early atomic energy program. On October 13, 1997, the Energy and Water Development Appropriations Act was signed into law, transferring the responsibility for the administration and execution of FUSRAP from the DOE to the United States Army Corps of Engineers (USACE).

#### **1.2 BACKGROUND**

Bliss & Laughlin is located at 110 Hopkins Street, Buffalo, New York. The site consists of a single large building. In 1952, Bliss & Laughlin Steel Company performed machining and straightening operations on uranium rods for National Lead Company of Ohio, a prime contractor for Atomic Energy Commission (AEC). Uranium rods were shipped from Lake Ontario Ordnance Works (LOOW) to Bliss & Laughlin for machining. Bliss & Laughlin shipped the machined rods directly to Fernald, Ohio, and the turnings from the operations were returned to LOOW for packaging and subsequent shipment to Fernald. In 1972, Ramco Steel, Inc., purchased Bliss & Laughlin Steel Company. Currently, Niagara Cold Drawn Corporation owns and operates the facility.

Based on the nature of operations performed at Bliss & Laughlin, the primary radiological constituent of concern for the site is uranium from the metal rods. Eighteen samples were analyzed to determine the relative abundance of radioisotopes. All samples showed ratios among the uranium isotopes that were similar to natural uranium.

### **1.3 PURPOSE**

The purpose of this Remedial Investigation, Feasibility Study, and Proposed Plan is to document the assessment of the environmental impacts for various actions at the Bliss and Laughlin site in Buffalo, New York. This documentation is required by the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) as a vehicle to inform the public of intended cleanup actions and solicit public input into cleanup decisions. Because this is a small site with only a small amount of contaminated materials the documentation for the cleanup is being combined into a single short document which describes the results of the investigation, the identification and evaluation of alternatives, and the plan proposed by the USACE. Characterization results are described in Appendix A of this report and in the administrative record described in Section 6 of this report.

### **1.4 SITE DESCRIPTION AND SETTING**

Historical records indicate that machining operations were performed in a section of the building called the "Special Finishing Area," which occupies approximately 3,230 square ft of floor space. The floor of the "Special Finishing Area" is concrete and contains several shallow utility trenches. There are no floor drains. The floor surfaces are generally rough and pitted and are covered with a thin layer of oil absorbent material and dried oil and grease. Machining equipment and material storage racks prevent access to some floor areas. The ceiling is approximately 37 feet high and is supported by a framework of steel trusses. The machining area of the building does not have any partition or interior walls. The site is currently used for the forming of steel products and is an active industrial site with equipment such as rolling mills and lots of machine oil.

### 2. SITE CHARACTERIZATION RESULTS

### 2.1 SURVEY AND SAMPLING ACTIVITIES

The results of the radiological and chemical characterization of the Bliss & Laughlin site are described in a 1995 Technical Memorandum (BNI, 1995). Historically, the facility was the site of uranium metal machining. Therefore, the primary radiological constituent of concern is uranium including the radioactive decay products. The site was assigned to FUSRAP based upon a designation survey preformed by the Oak Ridge Institute for Science and Education (ORISE). Using the data reported by ORISE, a survey of the floor area and the overheads in the vicinity of the Special Finishing Area was conducted, and a less intensive survey was performed throughout the rest of the building, with emphasis on areas adjacent to the Special Finishing Area, high traffic areas, and likely areas of material transfer such as locker rooms. Six core samples were drilled through the slab in areas where the potential for constituent migration was the greatest. Additional samples were taken from the dust on overhead beams and material on the floor. One composite sample of floor material was collected and analyzed for Toxicity Characteristic Leaching Procedure (TCLP) characteristics, which included metals, volatile organics, semi-volatile organics, pesticides and herbicides. Some areas were identified that have radioactive material that could result in exposure to radioactivity that exceeds the applicable or relevant and appropriate requirements (ARARs) which are described in the next section.

### 2.2 SURVEY RESULTS

Several areas on the floor and on the rafters were identified where radioactivity exceeds the ARARs described in Section 3.1. Some areas of a filled in trench are suspect and will require further characterization as part of the remediation activities. The characterization tried to identify areas significantly different from background levels and compared the results with criteria in the DOE Orders. The results are shown in Figures 1, 2, and 3 which are reproduced from the Technical Memorandum (BNI, 1995) and summarized below. A copy of this Technical Memorandum (BNI, 1995) is included in Appendix A.

- Two locations out of 45 surveyed on the overheads above the special finishing area were above 5000 dpm/100 sq cm beta/gamma. The highest reading of those two locations was 6318 dpm/100 sq cm beta/gamma.
- The surface contamination on the floor in the special finishing area is limited to approximately 19 meters by nine meters of floor, some of it obstructed by machinery. Ten locations exceeded 15,000 dpm/100 sq cm direct beta/gamma with a range from 17,000 to 280,000 dpm/100 sq cm.
- No subsurface soil samples showed evidence of contamination. One sample from a core taken through a filled-in trench showed elevated uranium levels. This material appears to be limited to debris deposited in the trench prior to sealing with concrete. The soil collected below this material was not above criteria.
- The remainder of the building was surveyed as extensively as building conditions allowed, and showed no evidence of additional contaminated areas.
- A composite TCLP sample from the floor in the Special Finishing Area showed no RCRA hazardous constituents.

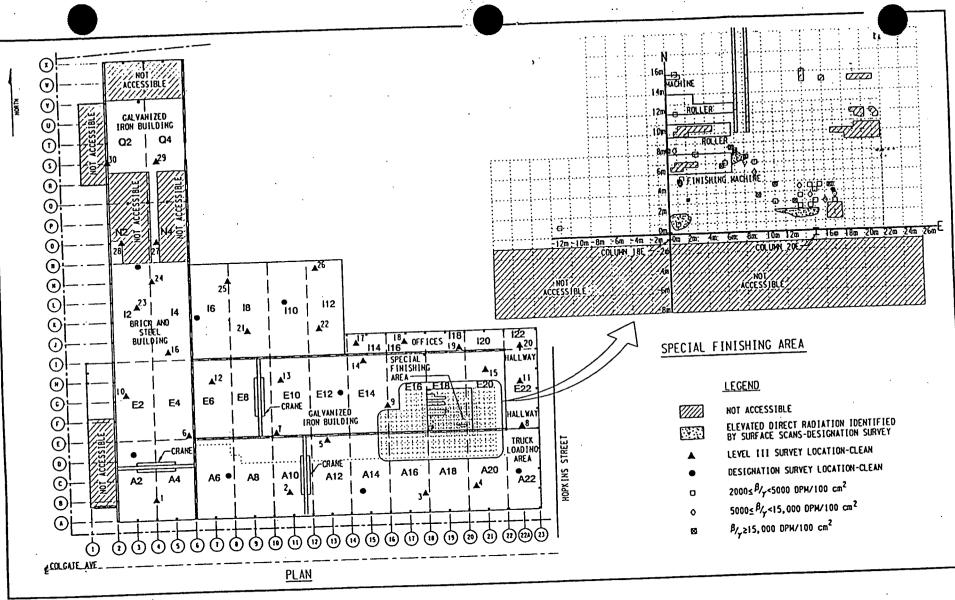


Figure 1 Bliss and Laughlin Steel with Reference Grids and Survey Locations

1285 002.004

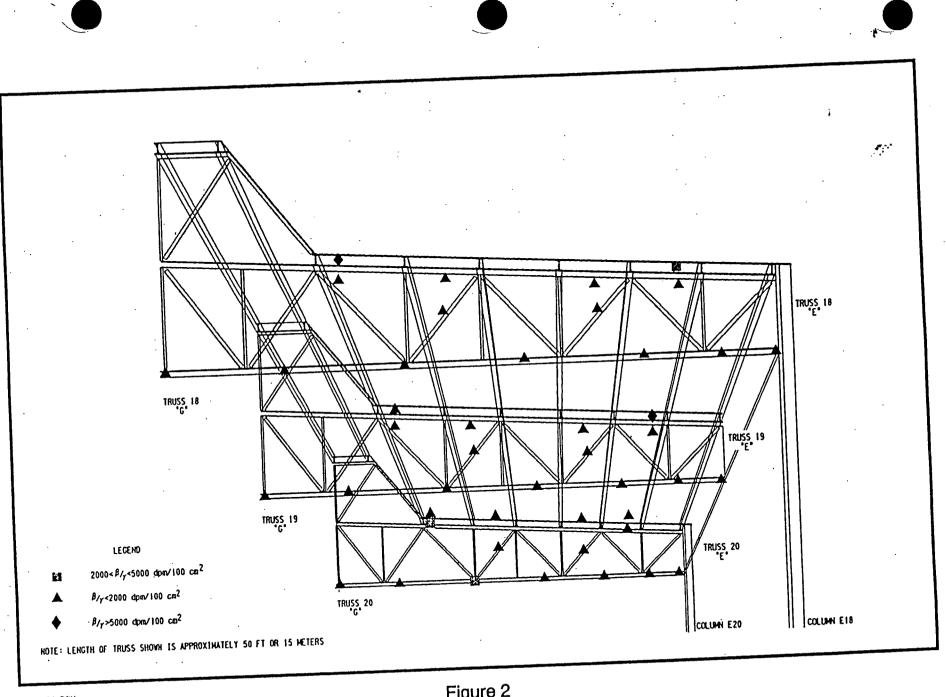


Figure 2 Overheads Above Special Finishing Area with Survey Locations

1281-004.DGN

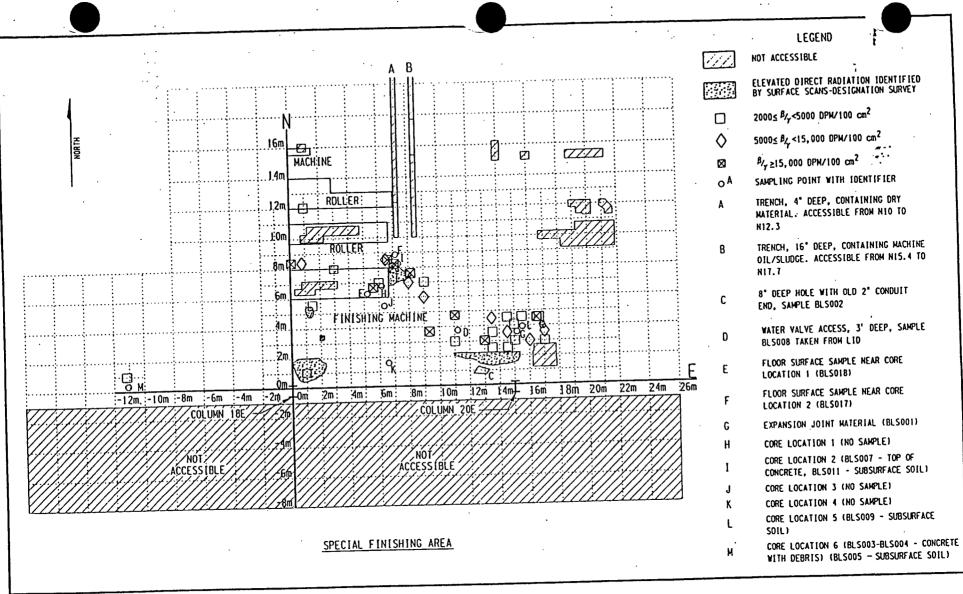


Figure 3 Detail of Special Finishing Area with Survey Results and Sampling Locations

1201003.0CM

### 3. IDENTIFYING AND EVALUATING CLEANUP OPTIONS

Three alternatives were considered. The first, No Action, is required by CERCLA to establish a baseline for comparison to the other alternatives. The second alternative is Continued Use of Institutional Controls. The third alternative is Decontamination of Buildings. This section describes the ARARs and TBCs, describes the alternatives in detail, and evaluates the alternatives for effectiveness, implementability, and cost.

### 3.1 DESCRIPTION OF ARARs AND TBCs.

### 3.1.1 Authority

Authority for responding to releases or threats of release from an impacted site is provided by Section 104 of CERCLA. In 1997, Congress authorized the USACE to manage FUSRAP. This includes authorization to undertake such investigation, surveys, testing, or other data gathering deemed necessary to identify the existence, extent, and nature of contaminants of concern (COC) present at the Bliss and Laughlin site including the extent of threats to human health and the environment. In addition, USACE is authorized to undertake planning, engineering, and other studies and investigations appropriate to direct response actions to prevent, limit, or mitigate potential risks associated with this site.

### 3.1.2 Applicable or Relevant and Appropriate Requirements (ARARs)

Applicable requirements are those cleanup standards, standards of control, and other substantive environmental protection requirements, criteria, or limitations promulgated under federal environmental or state environmental or facility siting laws that specifically address a hazardous substance, pollutant, contaminant, remedial action, location or other circumstance at a CERCLA site. An applicable requirement directly and fully addresses an element of the remedial action.

Relevant and appropriate requirements are those cleanup standards, standards of control, and other substantive environmental protection requirements, criteria or limitations promulgated under federal environmental or state environmental or facility siting laws that while not "applicable" to a hazardous substance, pollutant, contaminant, remedial action, location or other circumstance at a CERCLA site, address problems or situations sufficiently similar to those encountered at the CERCLA site that their use is suited to the particular site.

Only those state standards that are promulgated, are identified by the state in a timely manner, and are more stringent that federal requirements may be applicable or relevant and appropriate.

USACE has determined that the following regulation is an ARAR, as that term is defined in CERCLA.

Subpart E of 10 CFR 20 is considered relevant and appropriate to the removal action. This CFR provides standards for determining the extent to which sites must be remediated before decommissioning of a site can be considered complete and the license terminated. The standards for human exposure for both unrestricted use (workers and members of the public) and for restricted use with institutional controls are: 25 mrem/yr total effective dose equivalent (TEDE) and as low as reasonably achievable (ALARA). The amount (or concentration) of radioactive materials which would result in this dose depends on the future land use and exposure scenario. This requirement would be applicable if the uranium machining was done commercially with a license issued by the NRC. For the Bliss and Laughlin site, a license was not required because the work was done for the government. Therefore, the standards in Subpart E of 10 CFR 20 are considered relevant and appropriate to the removal action because the activities and contaminants are similar to those which require a license under 10 CFR 40 from the Nuclear Regulatory Commission or an agreement state and therefore subject to the license termination criteria in 10 CFR Part 20. The proposed approach to meet the 25 mrem/yr total effective dose equivalent and as low as reasonably achievable standard for unrestricted future use is described in section 3.3.3.

Standards for the tailings from uranium mills in 40 CFR 192 were considered, but are not considered ARARs because the contaminant at the Bliss & Laughlin site is uranium from the machining of uranium metal and is not similar to the mill tailings which contain large quantities of radium and other materials.

### 3.1.3 To be Considered (TBCs)

To-be-Considered (TBCs) are non-promulgated advisories, criteria, or guidance issued by a federal or state government that may be useful in developing CERCLA remedies that are not legally binding and do not have the status of potential ARARs. Because an ARAR has been identified, no TBCs are designated for this action.

### 3.1.4 Other Requirements

While not ARARS or TBCs, other environmental, safety, and occupational health standards will be followed when implementing this removal action. Examples include Occupational Safety and Health Administration Standards, and Resource Conservation and Recovery Act (RCRA) Land Disposal Restrictions.

### **3.2 SUMMARY OF SITE RISKS**

The contamination at the Bliss & Laughlin Site could result in adverse health effects if the building is used without restrictions to minimize exposures. The levels of contamination at the Bliss & Laughlin site are high enough to exceed the 25 mrem/yr standard in the ARAR for a typical building occupancy scenario. Therefore, scenarios are possible where individuals could be exposed to this material for extended periods of time resulting in an unacceptable risk. If the institutional controls were not continued, there would be no restrictions on the uses that could be made of the buildings and the materials in the buildings and scenarios resulting in higher doses would be possible.

As long as the use of the property is used as an industrial facility and provisions are made for periodic monitoring and reviews, the potential for adverse health effects would be mitigated. The typical scenarios for building occupancy used by the Nuclear Regulatory Commission result in the primary exposure path being inhalation with ingestion being a significant pathway. At the Bliss & Laughlin Site, the potential for exposure through these pathways is greatly reduced because of the large amount of oil and oil adsorbent used in the steel processing. Without remediation, scenarios are possible where the risk of cancer could exceed the risk range, i.e., be larger than 1 chance in 10,000. Again, inhalation is a possible pathway of concern even though current building use limits exposures via this pathway. Without remediation, the dose via the inhalation pathway could be as much as 100 mrem/yr or more. With remediation, the dose would be well below the ARAR and within the CERCLA risk range.

### **3.3 DESCRIPTION OF ALTERNATIVES**

### 3.3.1 Alternative 1: No Action

This alternative assumes that the facility is abandoned and institutional controls are discontinued. Under this alternative, it is assumed that there are no impediments to access. The controls would no longer exist and there would be no security guards or fences to exclude intruders. No signs warning of the hazards would be posted.

## 3.3.2 Alternative 2: Continued Institutional Controls

This alternative would continue the use of institutional controls at the site. These would include:

- Continued use of this site as an industrial facility,
- Maintaining signs and fencing,
- Continued maintenance and monitoring,
- Restriction of future use by acquisition of real estate interest or other means, and
- Periodic inspections by the Government to enforce any such restrictions.

The continued use of the site as an industrial facility with periodic monitoring and reviews would control the amount and duration of potential exposures. This alternative includes compliance with the controls by current and future building owners, including possible use of a restrictive covenant or other deed restriction to meet the restricted use criteria in the ARARs.

## 3.3.3 Alternative 3: Decontamination of Buildings.

Under this alternative the contamination on the floors, walls, and overhead appurtenances will be removed using appropriate decontamination technologies to a level sufficient to meet the ARAR. The technologies that may be employed include vacuuming,  $CO_2$  blasting, soft media blasting, etc. Contamination can be removed using either aggressive (Blastrac, VacuBlast, needle

guns, scabblers, chipping hammers, etc.) or non-aggressive (absorbent cloth and vermiculite, nuclear grade vacuum cleaners, paint remover, etc.) techniques.

Dust would be controlled during the performance of decontamination activities by spraying water or using other methods. Air monitors would be installed for work area monitoring. Any water generated or collected during the performance of work would be contained, sampled, analyzed, and disposed appropriately.

A licensed/permitted disposal facility would be used. Waste packaging would be performed in accordance with all applicable federal, state, and local laws and regulations. Shipping containers shall meet Department of Transportation (DOT) requirements. Only a few shipments are anticipated because of the small volume expected. Any lead-based paint removed from the building surfaces would be stored, handled, and disposed in accordance with all applicable regulations. Surveys would be conducted to check for cross contamination and to verify that the release criteria have been met.

The USACE proposes to (1) remove contamination above the levels in Regulatory Guide 1.86, (2) for ALARA purposes, to perform an additional attempt at decontamination of areas greater than 2,000 dpm/100 cm<sup>2</sup> (averaged over not more than 1 m<sup>2</sup>), and (3) to perform post remedial surveys and analyses to assure compliance with the ARAR. These three steps are discussed below.

The first step is to determine removals that will meet the 25 mrem/yr standard. Uranium contamination would be removed to levels that meet the ARAR for unrestricted use of 25 mrem/yr TEDE. Calculations were made to correlate the 25 mrem/yr in the ARAR with the uranium measurements at the Bliss and Laughlin facility. The standard scenarios used by the NRC for building occupancy (NUREG-1500 and NUREG-5512) show that average levels of 1500 dpm/100 cm<sup>2</sup> over large areas could result in exposures equal to the ARAR of 25 mrem/yr. For this scenario, the inhalation pathway contributes 84% of the dose. The ingestion pathway contributes 14% and the external gamma pathway contributes less than 1%. The inhalation and ingestion are likely very conservative in terms of current operations, but allow for possible changes in operations in the future. An evaluation was also made to compare the standards in Regulatory Guide 1.86 which are for much smaller areas. Decontamination to the levels in Regulatory Guide 1.86 should result in average levels in the special finishing area below the 1500 dpm/100 cm<sup>2</sup> large area average and below the 25 mrem/yr ARAR level. Regulatory Guide 1.86 recommends the following as acceptable surface contamination levels:

- $5,000 \text{ dpm}/100 \text{ cm}^2$  averaged over not more than  $1 \text{ m}^2$ ,
- $15,000 \text{ dpm}/100 \text{ cm}^2 \text{ maximum for any } 100 \text{ cm}^2 \text{ area, and}$
- $1,000 \text{ dpm}/100 \text{ cm}^2$  removable contamination averaged over not more than  $1 \text{ m}^2$ .

The second step is to evaluate as low as reasonably achievable levels. The USACE proposes to conduct an additional decontamination to achieve as low as reasonably achievable levels. This additional decontamination will be done as part of the cleanup action. The cleanup team will attempt removal of contamination from areas with levels above 2,000 dpm/cm<sup>2</sup> (i.e., 2,000 dpm/cm<sup>2</sup> averaged over not more than 1 m<sup>2</sup> versus the 5,000 dpm/cm<sup>2</sup> in the Regulatory Guide). The

decontamination efforts are anticipated to remove most of the contamination and result in dose levels well below the 25 mrem/yr level.

The third step is to assure compliance with the ARAR. The compliance with the ARAR will be confirmed by measurements and a final calculation using the measurements from the site after the remediation is completed. In the unlikely event that post-remediation analysis indicates the potential for exposures above the 25 mrem/yr TEDE level, additional decontamination will be performed.

ļ

## 4. EVALUATION OF ALTERNATIVES

## **4.1 EVALUATION CRITERIA**

The alternatives described above were evaluated using CERCLA criteria to determine the most favorable actions for cleanup of the Bliss & Laughlin Site. These criteria are described below. They were established to ensure that the remedy is protective of human health and the environment, meets regulatory requirements, is cost effective, and uses permanent solutions and treatment to the maximum extent practicable. The results of the evaluation of alternatives to remediate the Bliss & Laughlin Site are described below.

# Table 1. Summary of CERCLA Evaluation Criteria

3

ł

j,

)

)

2

Ĵ

Overall Protection of Human Health and the Environment	addresses whether an alternative provides adequate protection and describes how risks are eliminated, reduced, or controlled through treatment, engineering controls, or institutional controls
Compliance with Federal and State Environmental Regulations	addresses if a remedy would meet all of the ARARs of other Federal and State environmental laws
Long-Term Effectiveness and Permanence	addresses the impacts of an alternative to protect human health and the environment over time, once the cleanup goals have been met
Short-Term Effectiveness and Environmental Impacts	addresses the impacts to the community and site workers during cleanup including the amount of time it takes to complete the action
Reduction in Toxicity, Mobility, or Volume through Treatment	addresses the anticipated performance of treatment tant permanently and significantly reduces toxicity, mobility, or volume of waste
Implementability	addresses the technical and administrative feasibility of an alternative, including the availability of materials and services required for cleanup
Cost	compares the differences in cost, including capital, operation, and maintenance costs
State Acceptance	evaluates whether the State agrees with, opposes, or has no comment on the preferred alternative.
Community Acceptance	addresses the issues and concerns the public may have regarding each of the alternatives

### 4.2 EVALUATION OF ALTERNATIVES

### 4.2.1 Overall Protection of Human Health and the Environment

### Potential Health Effects

Alternative 1, No Action, could result in adverse health effects if the building is used without restrictions to minimize exposures. Radioactivity exceeds the ARARs in several areas of the building. With No Action scenarios are possible where individuals could be exposed to this material for extended periods of time resulting in an unacceptable risk. Because the No Action alternative assumes no institutional controls remain in place, there would be no restrictions on the uses that could be made of the buildings and the materials in the buildings.

Alternative 2, Continued Use of Institutional Controls, would continue to control the risks by restricting the use of the property as an industrial facility and provide for periodic monitoring and reviews. As long as these controls remain effective, the potential for adverse health effects could be controlled. In a few isolated areas of the building, the potential would continue to exist for an employee to receive doses above the ARARs.

Alternative 3, Building Decontamination of Buildings, would eliminate the potential for exposure. However, the potential for exposure to workers during remedial activities increases due to the handling of the radioactive material. Remediation workers may be directly exposed to radioactive materials, and radioactive dust could become airborne, allowing it to be inhaled by workers. These effects can be' mitigated, however, by requiring remediation workers to wear protective equipment and by using appropriate dust suppression measures. These techniques have been very effective in controlling the spread of radioactive materials in previous work. The USACE plans to perform the decontamination on weekends and other times that would limit the impact to workers and operations of the plant. Monitoring would also be performed inside the construction area to ensure adequate protection of the remediation workers.

Shipment of the debris to a disposal facility will entail some risk to the community due to the potential for transportation accidents. The risks are principally associated with vehicle operation and not the characteristics of the material being shipped. The risks to the community from exposure to the contaminated wastes during transport are negligible compared with the risk of traffic accidents.

Transportation risks for this removal action are due to the potential for injuries or fatalities due to truck or rail accidents. Cashwell et al. (1986) have compiled the risks per kilometer. Risks are reduced by using shorter shipping distances. Because only a small volume of material is anticipated, only a few shipments will be required for Alternative 3.

## Potential Environmental Impacts

Under the No Action alternative, minor additional environmental impacts are expected due to building deterioration which may result in the uncontrolled release of radioactive material to the environment. These impacts are expected to be minor because, although surfaces in the building exceed criteria, the actual volume of radioactive materials is likely to be very low. These impacts would be controlled for the short term by using the institutional controls of Alternative 2.

Under the Building Decontamination alternative, no additional environmental impacts are expected from decontamination activity inside the building. These impacts would be reduced by employing dust control and other preventative measures during implementation.

# 4.2.2 Compliance with Federal and State Environmental Regulations

No Action would not comply with ARARs. Alternative 2, Continued Use of Institutional Controls, would provide compliance by continuing the industrial use of the site and providing monitoring and periodic reviews. However, the potential would continue to exist for a few workers to receive doses above the ARARs. Alternative 3, Decontamination, would be conducted in a manner that complies with ARARs. Post remedial surveys and analyses would be performed to assure compliance with the ARARs.

All alternatives would be conducted in accordance with other applicable environmental, safety, and occupational health requirements.

# 4.2.3 Long-Term and Short-Term Effectiveness and Permanence

Alternative 1, No Action, would not involve any reduction in the amount of radioactivity at the site. In addition, it would increase potential for human exposure or environmental release. The potential for human exposure to radiation would persist in the short and long term in Alternative 1. In the long term, and in the absence of any additional maintenance work, migration of the radioactive materials to the environment is possible because the radioactive surfaces in the building may not be adequately controlled in the future to prevent migration. Radioactive materials could eventually become airborne as dust, as the building deteriorates or in the event of a fire. The potential risk to human health from the building could also increase in the future if adequate safeguards are not maintained.

Alternative 2, Continued Institutional Controls would be effective in the short term. However, providing effective institutional controls for long periods (e.g. greater than 100 years) is difficult. Alternatives 3 would be effective in reducing short and long term health risks and would eliminate radioactive materials at the site. Alternatives 3 would comply with current ARARs. Radioactive wastes would be shipped to appropriately licensed or permitted facilities. This alternative would also eliminate the potential for migration to the environment.



# 4.2.4 Reduction in Toxicity, Mobility, or Volume through Treatment

None of the alternatives provides treatment on site for the materials to be removed. Materials which are removed will include treatment to meet the standards of any off-site disposal facility.

### 4.2.5 Implementability

All Alternatives are implementable. Although Alternative 3, Decontamination of Buildings, is technically more complex than Alternatives 1 and 2, similar projects have been successfully completed at other sites throughout the country; therefore, no technical barriers to implementation of Alternative 3 are foreseen. Radioactive wastes generated during the activities would be disposed at currently existing licensed/permitted disposal facilities. The decontamination technologies called for in Alternative 3 are readily available. These include processes such as blasting, Blastrac, needle guns scabblers, vacuums, paint remover, and cloth cleaning.

### Technical Feasibility

Technical feasibility is not applicable to the No Action Alternative. For alternative 2, institutional controls are already implemented. Although no technical impediments to implementation exist, the use of the area as an industrial facility with proper health and safety programs would need to be continued.

Radiological decontamination technologies called for in Alternative 3, Decontamination of Buildings, are available. Many standard decontamination procedures exist and have been used at FUSRAP and other cleanup sites. Consideration will be given to decommissioning equipment and procedures that would reduce waste and improve worker safety. Processes such as  $CO_2$  blasting, media blasting, Blastrac, needle guns, scabblers, vacuums, paint remover, and cloth cleaning are readily available. One complexity for alternative 3 is due to the need to work around ongoing activities. Thus, the work will likely be done on holidays or weekends.

## Availability of Services and Materials

All of the services and materials required to implement Alternatives 2 and 3 are readily available. Adequate commercial disposal capacity for the radioactive waste generated is available. No services or materials are required for Alternative 1.

### Administrative Feasibility

Alternative 1, No Action, would not require any permits and no activities are included for coordination. Alternative 2 continues the use of institutional controls which provides for the use of the buildings as an industrial facility.



Alternative 3, Decontamination of Buildings, would be readily implementable. Shipment of any waste generated and excavated soils would comply with any requirements for manifests, advance notification, and permitting in a timely manner.

### 4.2.6 Cost

Alternative 1, No Action, would have no cost. Alternative 2, Continued Institutional Controls, is estimated to cost about \$350,000 (mainly for monitoring and reviews over the next 30 years). Alternative 3, Building Decontamination, is estimated to cost approximately \$400,000 (\$350,000 to \$430,000). Costs are in 1998 dollars. Costs could vary due to uncertainty in the amount of material, the actual disposal location and transportation distances, and other factors. However, the cost estimates represent a reasonable comparison of the alternatives. The cost range for Alternative 3, Building Decontamination, reflects cleanup volumes ranging from 6 cubic yards ( the current best estimate) to 20 cy. The larger volume allows for possible volume increases if material is found in the trench or other areas.

Under Alternative 1, No Action, USACE would not incur any cost for implementation. Although Alternative 2, Continued Institutional Controls, would have limited costs in addition to normal operation as an industrial facility the costs continue for a long period. The cost estimate of \$350,000 includes six 5-year reviews at about \$15,000 each; Institutional controls, surveillance and monitoring for 30 years at about \$530/month, and project management at about \$750/yr. Alternative 3 would cost approximately \$400,000. The cost for alternative 3 will vary depending on if additional contamination is found during remediation. For a cleanup volume of 6 cy ( the current best estimate) the cleanup is estimated to cost approximately \$350,000. The higher estimate of \$430,000 assumes 20 cy of material which allows for possible volume increases if material is found in the trench or other areas. Principle costs include:

	WBS <sup>*</sup> , Activities	Cost (rounded to thousands)
-	32XX, studies and design	\$64,000
•	331XX01 & 331XX21, mob and demobilization	\$10,000
•	331XX02, monitoring, sampling and analysis	\$18,000
•	331XX03, site work including equip relocation, & office	\$68,000
•	•	\$ 4,000
•	331XX17, D&D	\$15,000
•	331XX19, transportation and disposal	,
•	331XX2201, supervision, safety & health, eng., waste mgm	\$129,000
•	331XX9X, other including mgr., data, CR, permits	\$31,000
•	333XX, construction management	\$18,000
•	34XXX, HTRW (post construction)	\$10,000

\* The Work Breakdown Structure (WBS) and the cost estimate are shown in Appendix B.



# 4.2.7 State and Community Acceptance

١

)

ł

The last two criteria, acceptability to the state and local community, will be evaluated after public input is received.

# 5. SELECTION OF THE PREFERRED ALTERNATIVE

The USACE prefers Alternative 3, Decontamination of Buildings. This alternative is protective of human health and the environment and eliminates the continuing costs for monitoring and periodic reviews. Radioactive materials generated during remedial activities will be disposed at appropriate existing licensed or permitted disposal facilities. Samples would be collected from the materials for analysis to ensure that materials meet the acceptance criteria of the disposal facility(ies). Decontamination to as low as reasonably achievable levels will be conducted by (1) removal of contamination at levels above those in Regulatory Guide 1.86, (2) performing additional decontamination attempts for areas with levels above 2,000 dpm/100 cm<sup>2</sup> (i.e., 2,000 dpm/cm<sup>2</sup> averaged over not more than  $1 \text{ m}^2$  versus the 5,000 dpm/100 cm<sup>2</sup> in the Regulatory Guide), and (3) post remediation measurements and calculations to assure that the remediated site meets the 25 mrem/yr ARAR. This action would complete the remediation of the Bliss and Laughlin site.

Radioactive materials would be packaged and shipped according to the acceptance criteria of the disposal facility as well as applicable Department of Transportation requirements. Materials would be shipped from the facility by rail or truck. The disposal location(s) will be selected after bids have been evaluated.

Engineering controls will be used during the decontamination activities to prevent the spread of radioactivity and to facilitate collection of any spilled material.

The proposed alternative will include:

- preparation of detailed work instructions and a health and safety plan; (1)
- characterization of suspect areas including the filled in trench to confirm the presence or (2) absence of contamination;
- site preparation including construction of lay-down areas and preparation of designated (3) storage areas for managing wastes generated during building decontamination activities;
- decontamination of specified areas using techniques such as vacuuming, media blasting, (4) cleaning, and/or chemical methods;
- sampling and analysis of wastes generated during remedial activities to demonstrate (5) compliance with waste acceptance criteria;
- loading and packaging of radioactive materials for shipment to the disposal facilities; (6)
- shipment of the materials to the disposal facility(ies); (7)
- restoration activities, as required; and (8)
- post remedial surveys and analyses to assure compliance with the unrestricted release criteria (9) in the ARARs and to evaluate if the action meets the TBCs.



# 6. COMMUNITY ROLE IN THE SELECTION PROCESS

USACE invites members of the public to review the proposed plan and the supporting documents which further describe the conditions at the Bliss & Laughlin Site and the basis for the proposal. Those documents may be found in the administrative record for the Bliss & Laughlin Site at the Buffalo and Erie County Public Library-Dudley Branch, 2010 South Park Avenue, Buffalo, New York, 14220, and at the USACE FUSRAP Public Information Center, 1776 Niagara Street, Buffalo, New York, 14207. Members of the public who wish to comment upon this proposed plan may submit their comments to USACE at the following address:

U.S. Army Corps of Engineers Buffalo District FUSRAP Public Information Center 1776 Niagara Street Buffalo, NY 14207-3199

Ţ)

1

Please refer to this proposed plan or to the Bliss & Laughlin Site in the comments. All comments will be reviewed and considered by USACE in determining the final remedy for the Bliss & Laughlin Site. Comments should be submitted no later than 30 days after the date of this proposed plan.

After the close of the comment period, USACE will review all public comments, as well as the information contained in the Administrative Record file for this site, and any new information developed or received during the course of this comment period, in light of the requirements of CERCLA and the NCP. An authorized official of USACE will then make a final selection of the remedial action to be conducted at this site. This decision will be documented in a Record of Decision, which will be issued to the public, along with a response to all comments submitted regarding this proposed plan.

### 7. REFERENCES

10 CFR (Code of Federal Regulations) 835. Occupational Radiation Protection; Final Rule.

40 CFR 192. Health and Environmental Protection Standards for Uranium and Thorium Mill Tailings.

AEC (Atomic Energy Commission) Regulatory Guide 1.86. Termination of Operating Licenses for Nuclear Reactors.

BNI, 1995. FUSRAP Technical Memorandum: Bliss and Laughlin Steel Characterization Results, May 11.

Cashwell, J.W., et al., 1986. Transportation Impacts of the Commercial Radioactive Waste Management Program, SAND-85-2715, Albuquerque, New Mexico, April.

NYSDEC, 1993. New York Department of Environmental Conservation Technical Administrative Guidance Memorandum (TAGM) 4003.

)

NUREG-1500. Dailey, M.C., et al., Working Draft Regulatory Guide on Release Criteria for Decommissioning: NRC Staff's Draft for Comment, Nuclear Regulatory Commission, Appendix A-2.

NUREG-5512. Kennedy, W. E. and Strenge, D. L., Residual Radioactive Contamination from Decommissioning, U.S. Nuclear Regulatory Commission, October 1992.

Appendix A BLISS AND LAUGHLIN STEEL CHARACTERIZATION RESULTS

)

١

1

)



128.95-		<b>\</b> -
NO <u>(1</u> )	Rev. No.	$\overline{\chi}$

DATE: \_\_\_\_\_

## FUSRAP TECHNICAL MEMORANDUM

- TO: Eric T. Newberry
- FROM: Laura M. Artates
- DATE: May 11, 1995

SUBJECT: Bliss and Laughlin Steel Characterization Results

Project Manager Approval Project Engineer Approval Prepared By j.M. Mitches

### SCOPE

This Technical Memorandum presents the results of the radiological and chemical characterization of the Bliss and Laughlin Steel site. Historically, the facility was the site of uranium metal machining; therefore, the primary radiological constituent of concern is U-238. The site was assigned to FUSRAP based upon a designation survey performed by the Oak Ridge Institute for Science and Education. Using the data reported in the ORISE designation survey (ORISE, 1992) a survey of the floor area and the overheads in the vicinity of the Special Finishing Area was conducted, and a less intensive survey was performed throughout the rest of the building, with emphasis on areas adjacent to the Special Finishing Area, high traffic areas, and likely areas of material transfer such as locker rooms. Six core samples were drilled through the slab in areas where the potential for constituent migration was the greatest. Additional samples were taken from the dust on overhead beams and material on the floor. One composite sample of floor material was collected and analyzed for TCLP Total, which included metals, volatile organics, semi-volatile organics, pesticides, and herbicides.

### PROCEDURES

To aid in identification of areas within the building the north-south support column lines were numbered 1 to 23 from west to east and the east-west column lines were labeled A to X from south to north (Figure 1). Each section of the floor is designated by the letter and number of the SW corner column of that section. All sampling locations and areas of significant findings were identified such that the location can be referenced to the SW corner of a section. All fixed point measurements were performed to measure levels of alpha and beta-gamma radiation, although the conditions in the building (i.e. oil-covered floors) were expected to cause significant shielding of alpha radiation.

Three different levels of survey were performed on different areas of the floor. A Level I survey consisting of a 1-meter<sup>2</sup> five-point survey was conducted in the areas where elevated surface readings were identified (the Special Finishing Area). This survey was to clearly define the areas of elevated surface activity. A Level II survey consisting of a 100% scan using a floor monitor was conducted over a six-meter wide area surrounding all Level I survey areas. This survey was to verify that all elevated areas were bounded. A Level III survey, covering at least 50% of the floors in the remainder of the building, was performed to verify that no other areas of the building floors were radiologically elevated. Surface scan readings were considered to be elevated if they were twice background (Table 1) as used in the Level II and Level III surveys. Additional surveys were performed and samples were collected in the Special Finishing Area to determine the scope for potential remediation planning.

### RESULTS

75% of the alpha readings on the floors were at or below background (<Lc), as compared to 31% of the beta-gamma readings, indicating that the majority of the alpha radiation was shielded by the material on the surfaces being scanned or measured. Because of this, both alpha and beta gamma results will be reported in the data tables, but only beta-gamma results will be discussed. The alpha results from the overheads correlated slightly better with the beta/gamma results, indicating that the overhead contamination is probably not being shielded by paint. References to all original data can be found in the Work Instruction (BNI WI-95-073).

### Ceiling and Overhead Trusses

The overhead trusses above the Special Finishing Area were scanned to determine if they were above guidelines for beta-gamma contamination (Attachment 3). The survey results are presented in Figure 2 and Table 2.

- At a minimum, 50% of the surfaces of the bottom horizontal chords and the bottom two feet of the vertical members in the trusses were scanned. Twenty-one direct point measurements were recorded. There were no locations above fixed criteria, and only three locations where the direct readings were above transferable criteria (Table 2). Three composite dust samples were also collected and analyzed for radiological parameters: BLS014 from truss 19, BLS015 from truss 20, and BLS016 from truss 18 (Attachment 1). These samples had slightly elevated levels of uranium contamination, with the highest value at 15.6 pCi/g U-238. No samples were above criteria. No chemical characterization samples were collected from the overheads.
- The ceiling and upper sections of the trusses above the Special Finishing Area were surveyed by taking four direct readings on each truss and four readings on the ceiling areas near each truss. Six locations on the upper chords were smeared due to elevated readings. There were

two locations where direct measurements were above fixed criteria, and no locations where transferable measurements were above criteria (Table 2). It was not possible to access the roof vents, or to collect samples from the top portions of the trusses. There were no roof vents directly above the special finishing area.

Accessible areas of the crane were scanned, and showed no elevated readings.

#### Floors

Three different levels of survey were performed on different areas of the floor. Much of the floor throughout the building was obstructed by storage racks filled with steel stock or operations equipment, and was not accessible.

#### Level I Survey

A Level I survey consisting of a 1-meter<sup>2</sup> five-point survey and a floor monitor scan was conducted in the area where contamination was previously identified in the designation report Elevated locations identified as part of the floor monitor scan were then defined and measured using hand-held instruments. The areas of Level I survey are indicated in Figure 3 by the smaller square grid. Complete 5-point survey data for the Level I survey is presented in Attachment 4.

- Figure 3 shows the area encompassed by the Level I survey and the locations identified as not accessible (NA), elevated but below criteria (2,000-5,000 dpm/100cm<sup>2</sup>), above average criteria but below hotspot criteria (5,000 15,000 dpm/100cm<sup>2</sup>), and above hotspot criteria (15,000 dpm/100cm<sup>2</sup>).
- There were a total of ten locations above hotspot criteria. The direct beta/gamma readings for these locations ranged from approximately 17,000 to 280,000 dpm/100cm<sup>2</sup> (Table 3) and are indicated in Figure 3 by boxed X symbols.
- Eight locations fell between the average and hotspot criterias (5,000 15,000 dpm/100cm<sup>2</sup>).
   These locations are indicated in Figure 3 by diamond symbols. The data for these locations is presented in Table 4.
- To aid in remedial design an additional 17 locations were identified as elevated, although none of these locations is above criteria (Table 5). These locations are indicated Figure 3 by open square symbols.

#### Level II Survey

A Level II survey consisting of a 100% scan of accessible areas using a floor monitor and/or hand held instruments was conducted over a six-meter-wide area around the Level I survey areas. The area included is indicated in Figure 3 by the larger square grid.

This survey was used to verify that all elevated areas were bounded within the Level I survey area. No direct readings were taken in this survey. No areas at or above twice background were encountered in this survey.

### Level III Survey

A Level III survey was conducted throughout the remainder of the building. The accessible floors in all areas outside the Level I and Level II areas were scanned using a floor monitor, based on the data quality objectives for this characterization. Large areas which were not accessible are indicated in Figure 1. The remainder of the floors were estimated to be accessible for survey on an average of 40% of the surface. 30 additional point measurements were taken throughout the building based on field observations (Figure 1).

- All 30 point measurements were well below criteria, showing no evidence of contamination. The results from this survey are presented in Table 6.
- Floor monitor surveys did not indicate the presence of any hotspots or elevated areas.

### TCLP Results

One composite sample was collected from the floors in the Special Finishing Area and analyzed for TCLP Total. No RCRA hazardous constituents were identified (Attachment 2).

#### Trenches

Shallow drainage trenches in the vicinity of the special finishing area were surveyed using handheld instruments. No trenches were located in areas of elevated surface activity. The accessible sections of trenches surveyed showed no elevated readings, so no samples were collected. The trenches have been added to the as-built drawing (Figures 1 and 3).

Support columns/Equipment/etc.

- Support columns E18 and E20 were surveyed with hand-held meters to 2 meters high to
- Support containing 110 and 120 mere survey of the survey
- The equipment in the Special Finishing Area did not show evidence of contamination. Floor surfaces underneath equipment were surveyed as part of the Level I survey. One sample of floor material from under a piece of equipment was taken where radiological analysis results above guidelines were present (Attachment 1: BLS018 and Figure 3:E).

### Subsurface Floor Sampling

Six core locations in the Level 1 survey area were selected based on surface features and floor scan results. These locations were in areas where the potential for downward contamination migration was the greatest, either near expansion joints, resurfaced or repaired floor areas, or irregular areas of the floor (Figure 3). Sample results are presented in Attachment 1.

- Core location 1 (Figure 3:H) was partially under one of the pieces of equipment, at an irregular area of the floor. The drilling location was approximately 2.5 ft. E of a location which showed elevated surface readings. The concrete extended deeper than the drill could reach, so no subsurface sample was obtained. The surface of the core showed no elevated readings. A surface sample from the nearby elevated location (Figure 3:E) was collected, and showed U-238 at 1,215 pCi/g (BLS018).
- Core location 2 was taken along the surface of an old equipment stand which had apparently been demolished to the floor surface (Figure 3:I). The first attempt was directly on the broken concrete on an elevated location, but refusal was met at a few inches in depth. A sample of the top of the concrete (BLS007) was below radiological criteria. A second hole approximately 6 inches over reached soil at seven inches deep. A soil sample was collected from the top seven inches of soil (BLS011), that was below radiological criteria.
- Two attempts were made to reach soil at core location 3, which was in a repoured area near the center of the Special Finishing Area (Figure 3:J). A vertical metal bolt was encountered in the first hole, and the second one reached the furthest extent of the drill (approximately 15 inches) without encountering soil. The cores and holes were scanned and showed no elevated direct readings, and no samples were collected.
- Core location 4 was in a repoured area between columns E18 and E20 (Figure 3:K). One core was drilled, and refusal was encountered at approximately 6 inches. The core was removed, revealing gravel and the open end of a section of pipe, indicating that a trench had been filled with debris and then sealed with concrete. The core and hole were scanned and showed no elevated readings, and no samples were collected.
- Core location 5 was adjacent to an expansion joint north of column E20, where elevated readings were measured on the floor (Figure 3:L). A core was removed (approximately 6 inches), and soil samples were collected. The top six inches of soil were sent for analysis (BLS009), and the next six inches were archived. Analysis results showed that the soil was below criteria. A scan of the core and the hole showed no elevated readings.
- Core location 6 was located in the additional level I survey area between columns E16 and E18, in the center of a filled-in trench (Figure 3:M). Approximately four inches of concrete core was removed, revealing old pipe debris, gravel, and black sediment-like material. This material showed elevated readings, and two samples were collected (BLS003 & BLS004). These samples showed 23.5 and 86.7 pCi/g of U-238, respectively. A subsurface soil sample was collected using a hand-auger for analysis (BLS005) which was not above criteria, indicating that the contaminated material is isolated in the debris used to fill in the trench prior to sealing with concrete.

All of the cores which scanned clean were either placed back in the holes or disposed of as clean trash, and all of the boreholes were filled with quick-setting concrete.

)

5 of 7

### Open buried conduit

There is an eight inch deep irregular hole in the floor near Column E-20 in the Special Finishing Area which contains the open end of a buried two inch conduit from which the wires have been cut and removed (Figure 3:C). The hole and the end of the conduit were scanned and a sample of the material around the conduit was collected. The hole and conduit showed no elevated readings, and analysis results of material collected from the hole were below criteria.

### Water Valve Access

There is a three-foot deep water valve access shaft with a 10-inch lid near E18; N4, E11 (Figure 3:D). The interior sides and bottom of the shaft surfaces were not elevated. A sample (Attachment 1: BLS008) was taken from the material in the top of the lid, which showed U-238 at 128 pCi/g.

### SUMMARY

1

)

- Two locations out of 45 surveyed on the overheads above the special finishing area were above 5000 dpm/100 sq cm beta/gamma.
- The surface contamination on the floor in the special finishing area is limited to approximately 19 meters by nine meters of floor, some of it obstructed by machinery.
- No subsurface soil samples showed evidence of contamination. One sample from a core taken through a filled-in trench showed elevated uranium levels. This material contained no long-lived daughters, and appears to be limited to debris deposited in the trench prior to sealing with concrete. The soil collected below this material was not above criteria.
- The remainder of the building was surveyed as extensively as building conditions allowed, and showed no evidence of additional contaminated areas.
- A composite TCLP total sample from the floor in the Special Finishing Area showed no RCRA hazardous constituents.

### WASTE

PPE and equipment was surveyed for release to minimize the volume of radiologically contaminated waste generated. Waste water generated from cooling the core drill was used to mix the concrete used to backfill the boreholes, and the remainder will be evaporated and the residues surveyed for radiological contamination.

### Figures:

Figure 1. Map of building with detail showing survey locations and reference grid.
Figure 2. Overheads above Special Finishing Area with Survey Locations
Figure 3. Detail of Special Finishing Area with Survey Results and Sampling Locations

### Attachments:

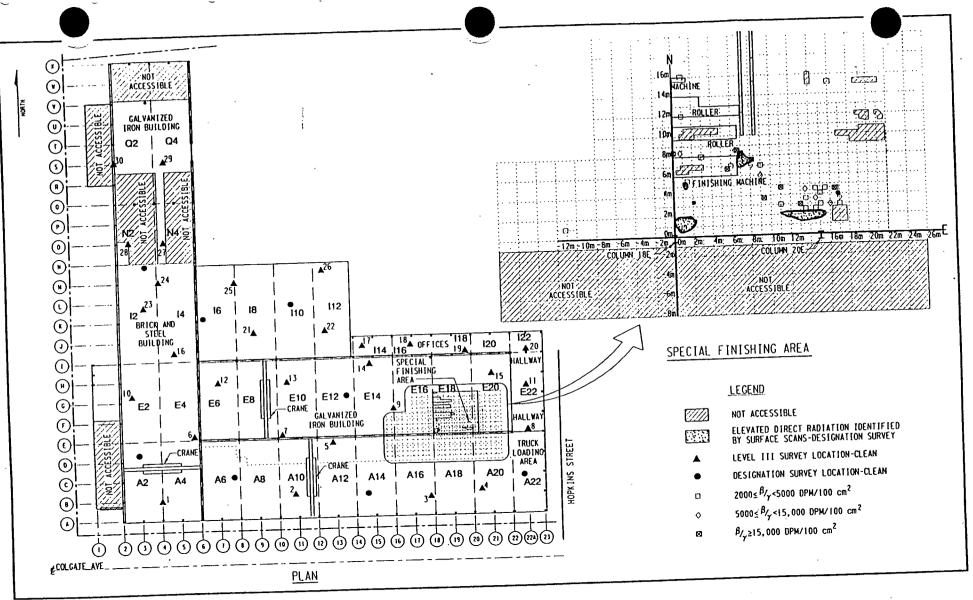
- 1. Bliss and Laughlin Radiological Data
- 2. Bliss and Laughlin Chemical Data
- 3. DOE 5400.5 Figure IV-1, Surface contamination Guidelines
- 4. Bliss and Laughlin Steel 5-point Survey Data

### **References:**

Ŋ

ORISE 1992, <u>Radiological Survey of the Former Bliss and Laughlin Steel Company Facility</u>, Buffalo, New York, ORISE 92/G-6

BNI WI, Bliss and Laughlin Steel Characterization, WI-95-073



128F 002.DGM

Figure 1 Bliss and Laughlin Steel with Reference Grids and Survey Locations

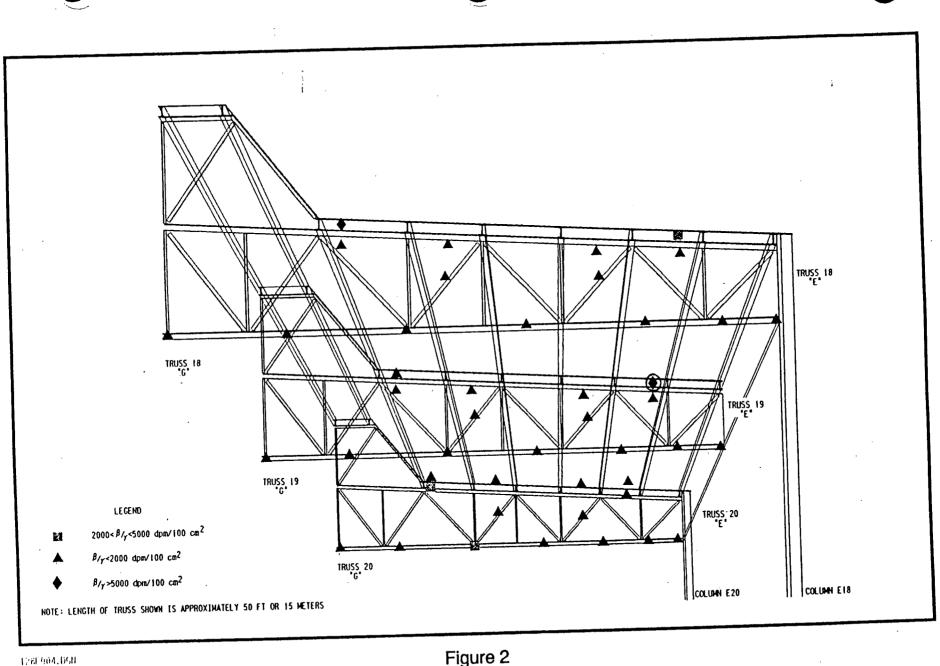
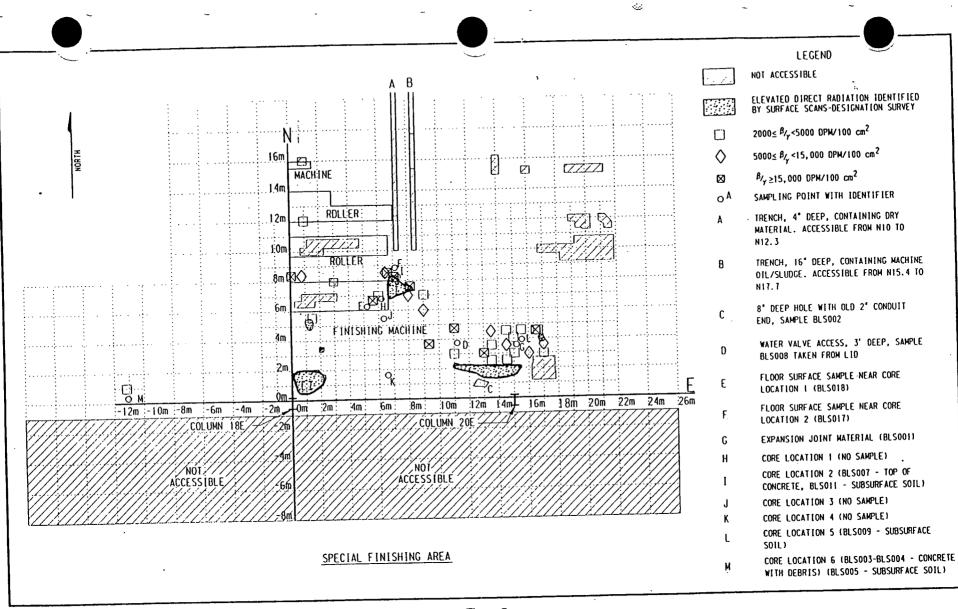


Figure 2 Overheads Above Special Finishing Area with Survey Locations



1281003.DCM

Figure 3 Detail of Special Finishing Area with Survey Results and Sampling Locations

Color. 11×17

#### Table 1: Bliss and Laughlin Steel Characterization Background Values

			DIRECT				TRA	NSFERABLE		
	ALPHA	V100	SQ CM	BETA	A-GAMMA/	100 SQ CM	ALPHA/100	SQ CM	BETA-GAMM	V100 SQ CM
LOCATION/ITEM	SMP	Ľ	STD		SMPL	STD	SMPL	STD	SMPL	STD
COORDINATES	DPM		DEV		DPM	DEV	DPM	DEV	DPM	DEV
GRID E-9		15	26		455	466	NA		NA	
GRID E-9		15	26	<lc< td=""><td>107</td><td>426</td><td>NA</td><td></td><td>NA</td><td></td></lc<>	107	426	NA		NA	
GRID E-9	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>187</td><td>436</td><td>NA</td><td></td><td>NÁ</td><td></td></lc<></td></lc<>	6	19	<lc< td=""><td>187</td><td>436</td><td>NA</td><td></td><td>NÁ</td><td></td></lc<>	187	436	NA		NÁ	
GRID E-9		24	32		375	457	NA		NĂ	
GRID E-9	<lc< td=""><td>6</td><td>-19</td><td></td><td>455</td><td>466</td><td>NA</td><td>1</td><td>NA</td><td>1</td></lc<>	6	-19		455	466	NA	1	NA	1
GRID E-9		19	34		551	565	NA		NA	
GRID E-9		19	34	<lc< td=""><td>32</td><td>504</td><td>NA</td><td></td><td>NA</td><td></td></lc<>	32	504	NA		NA	
GRID E-9	<lc< td=""><td>0</td><td>21</td><td></td><td>421</td><td>550</td><td>NA</td><td></td><td>NA</td><td></td></lc<>	0	21		421	550	NA		NA	
GRID E-9	<lc< td=""><td>10</td><td>28</td><td><lc< td=""><td>357</td><td>543</td><td>NA NA</td><td></td><td>NA</td><td></td></lc<></td></lc<>	10	28	<lc< td=""><td>357</td><td>543</td><td>NA NA</td><td></td><td>NA</td><td></td></lc<>	357	543	NA NA		NA	
GRID E-9	<lc< td=""><td>10</td><td>28</td><td></td><td>616</td><td>572</td><td>NA</td><td></td><td>NA</td><td></td></lc<>	10	28		616	572	NA		NA	

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

#### Table 2: Bliss and Laughlin Steel Characterization Survey of Overheads

			DIRECT				TRAM	SFERABLE			·
	ALPHA			BETA	-GAMMA	100 SQ CM	ALPHAV100		BETA-GA	AMMA	100 SQ CM
LOCATION/ITEM	SMP		STD	the second s	MPL	STD	SMPL	STD	SMP		STD
COORDINATES	DPM		DEV		DPM	DEV	DPM	DEV	DPN	۸ I	DEV
TRUSS 20E-G									†		
CEILING @ 4M	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>54</td><td>420</td><td></td><td></td><td>ŧ</td><td></td><td>·····</td></lc<></td></lc<>	6	19	<lc< td=""><td>54</td><td>420</td><td></td><td></td><td>ŧ</td><td></td><td>·····</td></lc<>	54	420			ŧ		·····
CEILING @ 7M	<lc< td=""><td>-4</td><td>5</td><td><u> </u></td><td>348</td><td>454</td><td></td><td></td><td>∦</td><td></td><td>······································</td></lc<>	-4	5	<u> </u>	348	454			∦		······································
CEILING @ 11M		24	32	<lc< td=""><td>134</td><td>429</td><td></td><td></td><td><u>∦</u></td><td></td><td></td></lc<>	134	429			<u>∦</u>		
CEILING @ 13M	<lc< td=""><td>6</td><td>19</td><td></td><td>482</td><td>469</td><td></td><td><u> </u></td><td><u>∦</u></td><td></td><td></td></lc<>	6	19		482	469		<u> </u>	<u>∦</u>		
TOP OF TRUSS @ 13M	<lc< td=""><td>6</td><td>19</td><td>†</td><td>1874</td><td></td><td><lc 0<="" td=""><td>0</td><td><lc< td=""><td>0</td><td>74</td></lc<></td></lc></td></lc<>	6	19	†	1874		<lc 0<="" td=""><td>0</td><td><lc< td=""><td>0</td><td>74</td></lc<></td></lc>	0	<lc< td=""><td>0</td><td>74</td></lc<>	0	74
TOP OF ANGLE @ 11M	<lc< td=""><td>6</td><td>19</td><td></td><td>509</td><td>472</td><td></td><td><u>                                      </u></td><td>1</td><td><u> </u></td><td></td></lc<>	6	19		509	472		<u>                                      </u>	1	<u> </u>	
TOP OF ANGLE @ 7M		24	32	<lc< td=""><td>-107</td><td>400</td><td></td><td></td><td><u> </u></td><td></td><td></td></lc<>	-107	400			<u> </u>		
TOP OF TRUSS @ 4M	<lc< td=""><td>6</td><td>19</td><td></td><td>2838</td><td>680</td><td>2</td><td>6</td><td><lc< td=""><td>37</td><td>78</td></lc<></td></lc<>	6	19		2838	680	2	6	<lc< td=""><td>37</td><td>78</td></lc<>	37	78
TRUSS 19E-G	1 - 20	24	32		518	454	<u> </u>	<u> </u>		+	
CEILING @ 4M	<lc< td=""><td>-4</td><td>5</td><td>&lt;Ŀc</td><td>294</td><td>448</td><td><u> </u></td><td>+</td><td>⋕</td><td></td><td></td></lc<>	-4	5	<Ŀc	294	448	<u> </u>	+	⋕		
CEILING @ 7M	<lc< td=""><td>-4</td><td>5</td><td><lc< td=""><td>- 204</td><td>413</td><td><u> </u></td><td>┼────</td><td></td><td></td><td>·····</td></lc<></td></lc<>	-4	5	<lc< td=""><td>- 204</td><td>413</td><td><u> </u></td><td>┼────</td><td></td><td></td><td>·····</td></lc<>	- 204	413	<u> </u>	┼────			·····
CEILING @ 11M		24	32	<lc< td=""><td>214</td><td>439</td><td><u> </u></td><td><u> </u></td><td><b></b></td><td></td><td>·</td></lc<>	214	439	<u> </u>	<u> </u>	<b></b>		·
CEILING @ 13M	<lc< td=""><td>6</td><td>19</td><td><u> </u></td><td>. 375</td><td>457</td><td></td><td>┼────</td><td>#</td><td></td><td>-<u></u></td></lc<>	6	19	<u> </u>	. 375	457		┼────	#		- <u></u>
TOP OF TRUSS @ 13M	<u> </u>	24	32		5943	884	2	6	<lc< td=""><td>49</td><td>80</td></lc<>	49	80
TOP OF ANGLE @ 11M		15	26	<u> </u>	562	478	<u>∠</u>	<u> </u>			
TOP OF ANGLE @ 7M	<lc< td=""><td>-4</td><td>20</td><td><u> </u></td><td>455</td><td>478</td><td> </td><td></td><td>#</td><td></td><td></td></lc<>	-4	20	<u> </u>	455	478			#		
TOP OF TRUSS @ 4M		24	32	┞───	1365	558	2	6	╂	86	83
TRUSS 18E-G	∦				1303		<u> </u>		╣────		0
CEILING @ 4M	<lc< td=""><td>-4</td><td>5</td><td><lc< td=""><td>214</td><td>439</td><td><b> </b></td><td><u>↓</u></td><td>╢────</td><td></td><td></td></lc<></td></lc<>	-4	5	<lc< td=""><td>214</td><td>439</td><td><b> </b></td><td><u>↓</u></td><td>╢────</td><td></td><td></td></lc<>	214	439	<b> </b>	<u>↓</u>	╢────		
CEILING @ 7M	<lc< td=""><td>-4</td><td>19</td><td></td><td>214</td><td>448</td><td><b>{{</b></td><td><u> </u></td><td><del>"</del></td><td></td><td></td></lc<>	-4	19		214	448	<b>{{</b>	<u> </u>	<del>"</del>		
CEILING @ 11M		15	26	<lc< td=""><td>-27</td><td>410</td><td><u> </u></td><td><u> </u></td><td>╫</td><td></td><td></td></lc<>	-27	410	<u> </u>	<u> </u>	╫		
		6		<lc< td=""><td>-27</td><td>410</td><td><u> </u></td><td><u> </u></td><td>∦</td><td></td><td>-<u></u></td></lc<>	-27	410	<u> </u>	<u> </u>	∦		- <u></u>
CEILING @ 13M	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>79</td></lc<>										79
TOP OF TRUSS @ 13M		42	41		4149	773	11	11	<pre></pre>	41	79
TOP OF ANGLE @ 11M	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>-80</td><td>403</td><td>¥</td><td><u> </u></td><td></td><td></td><td></td></lc<></td></lc<>	6		<lc< td=""><td>-80</td><td>403</td><td>¥</td><td><u> </u></td><td></td><td></td><td></td></lc<>	-80	403	¥	<u> </u>			
TOP OF ANGLE @ 7M	╟	24	32	╢	616	484	<u> </u>	<u> </u>			
TOP OF TRUSS @ 4M	<b> </b>	52	45	╟	6318	906	5		<lc< td=""><td>0</td><td>74</td></lc<>	0	74
		33	36	╟	5702	870	<lc 0<="" td=""><td>0</td><td><lc< td=""><td>25</td><td>77</td></lc<></td></lc>	0	<lc< td=""><td>25</td><td>77</td></lc<>	25	77
BOTTOM HORIZONTAL TR			<u>_</u> _					ļ	<u>}</u>		
TRUSS #20 Om	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>285</td><td>428</td><td></td><td>ļ</td><td>∦</td><td></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>285</td><td>428</td><td></td><td>ļ</td><td>∦</td><td></td><td></td></lc<>	285	428		ļ	∦		
TRUSS #20 3m	╟	15		<lc< td=""><td>207</td><td>419</td><td></td><td>ļ</td><td><u> </u></td><td></td><td></td></lc<>	207	419		ļ	<u> </u>		
TRUSS #20 6m	╟	15	26	₽	2228	614	NA	<b></b>	<u></u>		
TRUSS #20 9m	<u> </u>	15	26	<lc< td=""><td>259</td><td>425</td><td><b>#</b></td><td>ļ</td><td>⋕</td><td></td><td></td></lc<>	259	425	<b>#</b>	ļ	⋕		
TRUSS #20 12m	<b> </b>	15	26	<b>∦</b>	700	474	·····	ļ	#		
TRUSS #20 15m	<lc< td=""><td>-4</td><td>5</td><td><b>  </b></td><td>544</td><td>457</td><td><b></b></td><td><u> </u></td><td>∦</td><td></td><td>-<u></u></td></lc<>	-4	5	<b>  </b>	544	457	<b></b>	<u> </u>	∦		- <u></u>
TRUSS #20 18m	<b>  </b>	15	26		466	449	I	ļ	<u> </u>		
TRUSS #19 Om	<b> </b>	24	32	<b>  </b>	518	454	l	L	<u> </u>		
TRUSS #19 3m	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>259</td><td>425</td><td><b> </b></td><td>ļ</td><td>ļ</td><td></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>259</td><td>425</td><td><b> </b></td><td>ļ</td><td>ļ</td><td></td><td></td></lc<>	259	425	<b> </b>	ļ	ļ		
TRUSS #19 6m		15	26	<u> </u>	1036	508	NA	[	<u>  </u>		
TRUSS #19 9m		33	36	<b>.</b>	1062	510	NA		<u> </u>		
TRUSS #19 12m		24	. 32		440	446				4	
TRUSS #19 15m		24		<lc< td=""><td>26</td><td>397</td><td></td><td></td><td></td><td></td><td></td></lc<>	26	397					
TRUSS #19 18m	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>285</td><td>428</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6		<lc< td=""><td>285</td><td>428</td><td></td><td></td><td></td><td></td><td></td></lc<>	285	428					
TRUSS #18 0m	<lc< td=""><td>6</td><td>19</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td></td><td></td></lc<>	6	19		518	454					
TRUSS #18 3m.	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>52</td><td>400</td><td></td><td></td><td>1</td><td></td><td></td></lc<></td></lc<>	6	19	<lc< td=""><td>52</td><td>400</td><td></td><td></td><td>1</td><td></td><td></td></lc<>	52	400			1		
TRUSS #18 6m		42	41 -		596	463					
TRUSS #18 9m		24	32	<lc< td=""><td>207</td><td>419</td><td></td><td></td><td></td><td></td><td></td></lc<>	207	419					
TRUSS #18 12m	<lc< td=""><td>6</td><td>19</td><td><lc< td=""><td>285</td><td>428</td><td></td><td>1</td><td></td><td></td><td></td></lc<></td></lc<>	6	19	<lc< td=""><td>285</td><td>428</td><td></td><td>1</td><td></td><td></td><td></td></lc<>	285	428		1			
TRUSS #18 15m	1	24	32	<b>  </b>	363	437		T			······
TRUSS #18 18m	∦-—	24	32	ţ <u></u>	829	487		1			······
	н		·····	њ				<u> </u>	······		······

Comments:

Ima:OVHDSTOT.XLS

0 is the center of the truss ("G"). Measurements are in meters moving south (towards "E").

</p

1

)

)

.

Table 3:Bliss and Laughlin Steel CharacterizationSpecial Finishing Area - Survey locations above 15000 dpm/100 sq cm beta/gamma

I		DIRECT			TR	ANSFER	ABLE		
	ALPHA/100	SQ CM	BETA-GAMMA/10	00 SQ CM	ALPHA/100	SQCM	BET	A-GAMMA	100 SQ CM
LOCATION/ITEM	SMPL	STD	SMPL	STD	SMPL	STD		SMPL	STD
COORDINATES	DPM	DEV	DPM	DEV	DPM	DEV		DPM	DEV
N3.0 E13.0	<lc -4<="" td=""><td>20</td><td>108045</td><td>3303</td><td></td><td></td><td></td><td></td><td></td></lc>	20	108045	3303					
N8.0 E7.0	48	66	58554	2670	11	11	<lc< td=""><td>-21</td><td>73</td></lc<>	-21	73
N3.7 E9.35	15	26	42270	2126	5	8	<lc< td=""><td>. 12</td><td>76</td></lc<>	. 12	76
N7.6 E8.1	3165	335	135430	3755	224	50		1734	181
N8.1 E7.2	181	81	280257	5384	72	28		258	98
N8.5 E6.7	1129	200	29019	1776	17	14		152	89
N6.7 E5.7	42	41	17213	1393	23	16		184	92
N8.2 E0.1	98	60	218953	4763	<lc 0<="" td=""><td>0</td><td><lc< td=""><td>33</td><td>78</td></lc<></td></lc>	0	<lc< td=""><td>33</td><td>78</td></lc<>	33	78
N4.8 E11.0	33	36	55387	2422	<lc 0<="" td=""><td>0</td><td><lc< td=""><td>25</td><td>77</td></lc<></td></lc>	0	<lc< td=""><td>25</td><td>77</td></lc<>	25	77
N4.5 E16.5	88	57	71985	2752	2	6	<lc< td=""><td>20</td><td>77</td></lc<>	20	77

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

2

Page 1 of 1

#### Table 4:

#### Bliss and Laughlin Steel Characterization

Special Finishing Area - Survey locations between 5000 and 15000 dpm/100 sq cm beta/gamma

		DIRECT			TR	ANSFER	ABLE		
	ALPHA/10	SQ CM	BETA-GAMMA/10	0 SQ CM	ALPHA/100	SQ CM	BET	A-GAMMA/1	100 SQ CM
LOCATION/ITEM	SMPL	STD	SMPL	STD	SMPL	STD		SMPL	STD
COORDINATES	DPM	DEV	DPM	DEV	DPM	DEV		DPM	DEV
N3.0 E16.0	2	4 37	6063	871	<lc 2<="" td=""><td>6</td><td><lc< td=""><td>-54</td><td>72</td></lc<></td></lc>	6	<lc< td=""><td>-54</td><td>72</td></lc<>	-54	72
N3.5 E14.5	<lc 2<="" td=""><td>3 50</td><td>7362</td><td>969</td><td><lc -1<="" td=""><td>0</td><td><lc< td=""><td>50</td><td>70</td></lc<></td></lc></td></lc>	3 50	7362	969	<lc -1<="" td=""><td>0</td><td><lc< td=""><td>50</td><td>70</td></lc<></td></lc>	0	<lc< td=""><td>50</td><td>70</td></lc<>	50	70
N4.5 E13.5	<lc< td=""><td>9 43</td><td>5729</td><td>878</td><td><lc -1<="" td=""><td>0</td><td><lc< td=""><td>4</td><td>76</td></lc<></td></lc></td></lc<>	9 43	5729	878	<lc -1<="" td=""><td>0</td><td><lc< td=""><td>4</td><td>76</td></lc<></td></lc>	0	<lc< td=""><td>4</td><td>76</td></lc<>	4	76
N6.0 E9.0	3	3 41	14717	1273	5	8	<lc< td=""><td>-13</td><td>76</td></lc<>	-13	76
N7.0 E8.0	7	7 74	5595	953	5	8	<lc< td=""><td>46</td><td>80</td></lc<>	46	80
N8.5 E6.5	6	62	6130	901	5	8	<lc< td=""><td>59</td><td>81</td></lc<>	59	81
N8.3 E0.9	15	26	14777	1300	<lc 0<="" td=""><td>0</td><td><lc< td=""><td>33</td><td>78</td></lc<></td></lc>	0	<lc< td=""><td>33</td><td>78</td></lc<>	33	78
N3.4 E17.0	<pre>Lc 6</pre>	19	6559	919	2	6	<lc< td=""><td>-12</td><td>73</td></lc<>	-12	73

<Lc indicates less than the critical level of activity which can be said to be above background.</p>

A negative value is the calculated result of a reading which is below the instrument-specific background.

#### Table 5:

#### Bliss and Laughlin Steel Characterization

Special Finishing Area - Survey locations between 2000 and 5000 dpm/100 sq cm beta/gamma

ĺ			DIRECT				TR	ANSFER	ABLE		
[	ALP	HA/100	SQ CM	BETA-GAMMA/10	0 SQ CM	ALPH	HA/100	SQCM	BET	A-GAMMA/	00 SQ CM
LOCATION/ITEM	SI	MPL	STD	SMPL	STD	SN	MPL	STD		SMPL	STD
COORDINATES		PM	DEV	DPM	DEV	D	PM	DEV		DPM	DEV
N1.0 E1.0		24		4949	805						
N12.0 E1.0	<lc< td=""><td>-10</td><td></td><td></td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-33</td><td>71</td></lc<></td></lc<></td></lc<>	-10				<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-33</td><td>71</td></lc<></td></lc<>	2		<lc< td=""><td>-33</td><td>71</td></lc<>	-33	71
N2.5 E13.5	<lc< td=""><td>-9</td><td></td><td></td><td>708</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td><u> </u></td><td>77</td></lc<></td></lc<></td></lc<>	-9			708	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td><u> </u></td><td>77</td></lc<></td></lc<>	-1	0	<lc< td=""><td><u> </u></td><td>77</td></lc<>	<u> </u>	77
N2.5 E14.5	<lc< td=""><td>-9</td><td>35</td><td>2757</td><td>682</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<></td></lc<>	-9	35	2757	682	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>74</td></lc<>	-8	74
N3.0 E11.0		24	37	2176		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td>77</td></lc<></td></lc<>	2	6	<lc< td=""><td>-8</td><td>77</td></lc<>	-8	77
N3.0 E15.0		24	37	4042		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>77</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>77</td></lc<>	-8	77
N3.0 E17.0	<lc< td=""><td>6</td><td></td><td>4405</td><td>770</td><td></td><td>8</td><td>10</td><td><lc< td=""><td>0</td><td>78</td></lc<></td></lc<>	6		4405	770		8	10	<lc< td=""><td>0</td><td>78</td></lc<>	0	78
N3.5 E13.5	<lc< td=""><td>9</td><td></td><td></td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td></td><td>76</td></lc<></td></lc<></td></lc<>	9				<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td></td><td>76</td></lc<></td></lc<>	-1	0	<lc< td=""><td></td><td>76</td></lc<>		76
N4.0 E15.0	<lc< td=""><td>15</td><td>/ 33</td><td></td><td>the second s</td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-33</td><td>74</td></lc<></td></lc<></td></lc<>	15	/ 33		the second s	<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-33</td><td>74</td></lc<></td></lc<>	-1		<lc< td=""><td>-33</td><td>74</td></lc<>	-33	74
N4.5 E14.5		55			670	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>74</td></lc<>	-8	74
N4.5 E15.5	<lc< td=""><td>-9</td><td>35</td><td>3748</td><td>753</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<></td></lc<>	-9	35	3748	753	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-8</td><td></td></lc<>	-8	
N4.5 E16.5	<lc< td=""><td>9</td><td>43</td><td></td><td>636</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-4</td><td>75</td></lc<></td></lc<></td></lc<>	9	43		636	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-4</td><td>75</td></lc<></td></lc<>	2	6	<lc< td=""><td>-4</td><td>75</td></lc<>	-4	75
N5.5 E1.5	<lc< td=""><td>-28</td><td></td><td></td><td>للم ت الم الم الم الم الم الم الم الم الم الم</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-4</td><td>75</td></lc<></td></lc<></td></lc<>	-28			للم ت الم	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-4</td><td>75</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-4</td><td>75</td></lc<>	-4	75
N7.0 E6.0	<lc< td=""><td>10</td><td></td><td></td><td>756</td><td></td><td>5</td><td></td><td><lc< td=""><td>13</td><td>76</td></lc<></td></lc<>	10			756		5		<lc< td=""><td>13</td><td>76</td></lc<>	13	76
N7.0 E9.0	<lc< td=""><td>-29</td><td></td><td></td><td>770</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td>73</td></lc<></td></lc<></td></lc<>	-29			770	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td>73</td></lc<></td></lc<>	2	6	<lc< td=""><td>-21</td><td>73</td></lc<>	-21	73
N7.5 E7.5	<lc< td=""><td>9</td><td>43</td><td>4819</td><td>823</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td>71</td></lc<></td></lc<></td></lc<>	9	43	4819	823	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td>71</td></lc<></td></lc<>	2	6	<lc< td=""><td>-33</td><td>71</td></lc<>	-33	71
N1.0 E-11.1		15	26	3641	738		2	6	<lc< td=""><td>37</td><td>78</td></lc<>	37	78

<Lc indicates less than the critical level of activity which can be said to be above background.

A negative value is the calculated result of a reading which is below the instrument-specific background.

#### Table 6: Bliss and Laughlin Steel Characterization Level III Survey - 30 Points

				DIRECT					TRAN	ISFERABLE			
		ALPH	IA/100 S	SQ CM	BETA	-GAMMA/1	00 SQ CM	ALPHA	V100 S	SQ CM	BETA-	GAMMA/100	SQ CM
	LOCATION/ITEM	SN	1PL	STD		SMPL	STD	SM	PL	STD		SMPL	STD
NO:	COORDINATES	DP	M	DEV		DPM	DEV	DP	M	DEV		DPM	DEV
1	A4; N7.0 E0.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>1101</td><td>617</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td>76</td></lc<></td></lc<></td></lc<>	-10	47		1101	617	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td>76</td></lc<></td></lc<>	2	6	<lc< td=""><td>-21</td><td>76</td></lc<>	-21	76
2	A11; N8.9 W1.4	<lc< td=""><td>0</td><td>51</td><td> </td><td>887</td><td>596</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-84</td><td>69</td></lc<></td></lc<></td></lc<>	0	51		887	596	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-84</td><td>69</td></lc<></td></lc<>	2	6	<lc< td=""><td>-84</td><td>69</td></lc<>	-84	69
3	A18; N6.7 W1.5		NA	NA	<lc< td=""><td>153</td><td>519</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	153	519						
4	A20; N9.2 E3.0	<lc< td=""><td>-29</td><td>39</td><td></td><td>642</td><td>572</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-29	39		642	572						
5	E12; S2.2 E6.2	<lc< td=""><td>-19</td><td>43</td><td></td><td>581</td><td>565</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		581	565						
6	E6; N1.2 W2.0	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39	34	<lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	275	533						
7	E10; N1.0 E1.6	<lc< td=""><td>-19</td><td>43</td><td></td><td>459</td><td>553</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		459	553						
8	120; S29.7 E20.3	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>336</td><td>539</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>336</td><td>539</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	336	539						
9	E16; N10.3 E0.0	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>306</td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>306</td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	306	536						
10	G2; N1.6 E4.3	<l¢< td=""><td>29</td><td>60</td><td><lc< td=""><td>214</td><td>526</td><td>1</td><td>·</td><td></td><td></td><td></td><td></td></lc<></td></l¢<>	29	60	<lc< td=""><td>214</td><td>526</td><td>1</td><td>·</td><td></td><td></td><td></td><td></td></lc<>	214	526	1	·				
11	120; S12.5 E20.3	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>-31</td><td>498</td><td>Í</td><td></td><td></td><td>ſ</td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>-31</td><td>498</td><td>Í</td><td></td><td></td><td>ſ</td><td></td><td></td></lc<>	-31	498	Í			ſ		
12	H2; S1.3 E80.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>367</td><td>543</td><td>1</td><td></td><td></td><td>1</td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>367</td><td>543</td><td>1</td><td></td><td></td><td>1</td><td></td><td></td></lc<>	367	543	1			1		
13	E10; N21.4 E3.9	<lc< td=""><td>-10</td><td>47</td><td>ÍĹ</td><td>734</td><td>581</td><td></td><td></td><td></td><td>}</td><td></td><td></td></lc<>	-10	47	ÍĹ	734	581				}		
14	111; N2.8 W1.5	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>306</td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39	34	<lc< td=""><td>306</td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	306	536						
15	121; S7.5 E0.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>61</td><td>509</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>61</td><td>509</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	61	509						
16	J2; S4.6 E21.1	<lc< td=""><td>-39</td><td>34</td><td></td><td>550</td><td>562</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-39	34		550	562						
17	114; N4.7 E4.0	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	367	543						
18	116; N4.0 E8.4	<lc< td=""><td>-19</td><td>43</td><td></td><td>428</td><td>549</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		428	549						
19	120; N0.7 W0.7	<lc< td=""><td>-48</td><td>28</td><td><lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-48	28	<lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	275	533						
20	120; N0.7 E20.3	<lc< td=""><td>-48</td><td>28</td><td>۱<u>ــــــ</u></td><td>581</td><td>565</td><td></td><td></td><td></td><td>1</td><td></td><td></td></lc<>	-48	28	۱ <u>ــــــ</u>	581	565				1		
_	19; N10.1 W1.0	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>. 275</td><td>533</td><td></td><td></td><td>l</td><td>∦</td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>. 275</td><td>533</td><td></td><td></td><td>l</td><td>∦</td><td></td><td></td></lc<>	. 275	533			l	∦		
22	112; N9.7 E4.3	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>245</td><td>529</td><td><u>  </u></td><td></td><td> </td><td><u> </u></td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>245</td><td>529</td><td><u>  </u></td><td></td><td> </td><td><u> </u></td><td></td><td></td></lc<>	245	529	<u>  </u>			<u> </u>		
23		<lc< td=""><td>-48</td><td>28</td><td><lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td>1</td><td></td><td></td></lc<></td></lc<>	-48	28	<lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td>1</td><td></td><td></td></lc<>	275	533				1		
24	M6; N0.0 W7.5	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>275</td><td>533</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	275	533						
	M8; S0.9 W0.3	<lc< td=""><td>0</td><td>51</td><td><lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0	51	<lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	367	543						
26	M12; N3.1 E3.4		67	71		550	562	1					
27	06; N0.0 W12.4	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39	34	<lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	367	543						
	O2; N0.0 E4.1	<lc< td=""><td>-48</td><td>28</td><td><lc< td=""><td>306</td><td>536</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-48	28	<lc< td=""><td>306</td><td>536</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	306	536	1					
	S6; N0.0 W11.4	<lc< td=""><td>-10</td><td>47</td><td></td><td>1070</td><td>614</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-105</td><td>66</td></lc<></td></lc<></td></lc<>	-10	47		1070	614	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-105</td><td>66</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-105</td><td>66</td></lc<>	-105	66
30	S2; N4.0 E0.2	<lc< td=""><td>-19</td><td>43</td><td></td><td>581</td><td>565</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19	43		581	565						

Comments:

NA= AREA TOO WET TO OBTAIN ALPHA MEASUREMENTS

THE ALPHA NUMERIC CHARACTERS REPRESENT THE REFERENCED COLUMN USED TO OBTAIN THE COORDINATES

THE NUMBER REPRESENTS THE LOCATION AS SHOWN ON THE FIGURE.

<Lc indicates less than the critical level of activity which can be said to be above background. A negative value is the calculated result of a reading which is below the instrument-specific background.

#### Table 7 Bliss and Laughlin Steel Characterization Survey of Columns

	<u>_</u>		DIRECT				TRANSFERABLE					
	ALPH,	AV100 \$	SQ CM	BETA	-GAMMA	100 SQ CM	ALPHA/100	SQ CM	BETA-GAMMA	/100 SQ CM		
LOCATION/ITEM	SMF	PL	STD		SMPL	STD	SMPL	STD	SMPL	STD		
COORDINATES	DPN	л	DEV		DPM	DEV	DPM	DEV	DPM	DEV		
COLUMN E-18A												
FRONT @ 1M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>324</td><td>539</td><td>[</td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<></td></lc<>	0	21	<lc< td=""><td>324</td><td>539</td><td>[</td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<>	324	539	[			· · · · · · · · · · · · · · · · · · ·		
BACK @ 1M		38	43	<lc< td=""><td>-195</td><td>476</td><td></td><td></td><td></td><td></td></lc<>	-195	476						
SIDE @ 1M	<lc< td=""><td>10</td><td>28</td><td><lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td>//////////////////////////////////////</td></lc<></td></lc<>	10	28	<lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td>//////////////////////////////////////</td></lc<>	-130	484				//////////////////////////////////////		
SIDE @ 1M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>-130</td><td>484</td><td></td><td></td><td></td><td></td></lc<>	-130	484						
COLUMN E-18B										·		
FRONT @ 1M		19	34	<lc< td=""><td>97</td><td>512</td><td></td><td></td><td></td><td></td></lc<>	97	512						
BACK @ 1M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-195</td><td>476</td><td></td><td>[</td><td></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>-195</td><td>476</td><td></td><td>[</td><td></td><td></td></lc<>	-195	476		[				
SIDE @ 1M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-389</td><td>449</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>-389</td><td>449</td><td></td><td></td><td></td><td></td></lc<>	-389	449						
SIDE @ 1M		19	34	<lc< td=""><td>-195</td><td>476</td><td>j</td><td>[</td><td></td><td></td></lc<>	-195	476	j	[				
COLUMN E-18A		·						[				
FRONT @ 2M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-227</td><td>471</td><td> </td><td> </td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-227</td><td>471</td><td> </td><td> </td><td></td><td></td></lc<>	-227	471						
BACK @ 2M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>32</td><td>504</td><td></td><td> </td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>32</td><td>504</td><td></td><td> </td><td></td><td></td></lc<>	32	504						
SIDE @ 2M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-389</td><td>449</td><td> </td><td>[</td><td></td><td>······</td></lc<></td></lc<>	-10	8	<lc< td=""><td>-389</td><td>449</td><td> </td><td>[</td><td></td><td>······</td></lc<>	-389	449		[		······		
SIDE @ 2M	<lc< td=""><td>0</td><td>21</td><td></td><td>4085</td><td>871</td><td>8</td><td>10</td><td>111</td><td>85</td></lc<>	0	21		4085	871	8	10	111	85		
QC	<lc< td=""><td>0</td><td>21</td><td> </td><td>3145</td><td>801</td><td>5</td><td>8</td><td>90</td><td>83</td></lc<>	0	21		3145	801	5	8	90	83		
COLUMN E-18B	1						[	f	1			
FRONT @ 2M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>162</td><td>520</td><td></td><td> </td><td></td><td>/**  </td></lc<></td></lc<>	0	21	<lc< td=""><td>162</td><td>520</td><td></td><td> </td><td></td><td>/**  </td></lc<>	162	520				/** 		
BACK @ 2M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>0</td><td>500</td><td></td><td></td><td>¥</td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>0</td><td>500</td><td></td><td></td><td>¥</td><td></td></lc<>	0	500			¥			
SIDE @ 2M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-259</td><td>467</td><td>{</td><td>f</td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-259</td><td>467</td><td>{</td><td>f</td><td></td><td></td></lc<>	-259	467	{	f				
SIDE @ 2M		67	54	<lc< td=""><td>-130</td><td>484</td><td></td><td> </td><td></td><td></td></lc<>	-130	484						
COLUMN E-20A												
FRONT @ 1M		19	34	<lc< td=""><td>-130</td><td>484</td><td></td><td>[</td><td>( <u> </u></td><td></td></lc<>	-130	484		[	( <u> </u>			
BACK @ 1M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>162</td><td>520</td><td></td><td> </td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>162</td><td>520</td><td></td><td> </td><td></td><td></td></lc<>	162	520						
SIDE @ 1M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-97</td><td>488</td><td><u> </u></td><td><u> </u></td><td>li</td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-97</td><td>488</td><td><u> </u></td><td><u> </u></td><td>li</td><td></td></lc<>	-97	488	<u> </u>	<u> </u>	li			
SIDE @ 1M		19	34	<lc< td=""><td>0</td><td>500</td><td></td><td>[</td><td></td><td></td></lc<>	0	500		[				
COLUMN E-20B												
FRONT @ 1M		19	34	<lc< td=""><td>-130</td><td>484</td><td>[</td><td>[</td><td></td><td></td></lc<>	-130	484	[	[				
BACK @ 1M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-162</td><td>480</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-162</td><td>480</td><td></td><td></td><td></td><td></td></lc<>	-162	480						
SIDE @ 1M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-486</td><td>436</td><td><u> </u></td><td>[</td><td><u> </u></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-486</td><td>436</td><td><u> </u></td><td>[</td><td><u> </u></td><td></td></lc<>	-486	436	<u> </u>	[	<u> </u>			
SIDE @ 1M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-162</td><td>480</td><td></td><td><u>├</u>────</td><td></td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>-162</td><td>480</td><td></td><td><u>├</u>────</td><td></td><td></td></lc<>	-162	480		<u>├</u> ────				
COLUMN E-20A	1							<u> </u>	1			
FRONT @ 2M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-32</td><td>496</td><td> </td><td> </td><td></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>-32</td><td>496</td><td> </td><td> </td><td></td><td></td></lc<>	-32	496						
BACK @ 2M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>97</td><td>512</td><td></td><td><u> </u></td><td>1</td><td></td></lc<></td></lc<>	-10	8	<lc< td=""><td>97</td><td>512</td><td></td><td><u> </u></td><td>1</td><td></td></lc<>	97	512		<u> </u>	1			
SIDE @ 2M	<lc< td=""><td>-10</td><td>8</td><td><lc< td=""><td>-227</td><td>471</td><td>8</td><td>10</td><td>111</td><td>85</td></lc<></td></lc<>	-10	8	<lc< td=""><td>-227</td><td>471</td><td>8</td><td>10</td><td>111</td><td>85</td></lc<>	-227	471	8	10	111	85		
SIDE @ 2M	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>-65</td><td>492</td><td> </td><td> <u>`</u></td><td><b>***</b></td><td></td></lc<></td></lc<>	0		<lc< td=""><td>-65</td><td>492</td><td> </td><td> <u>`</u></td><td><b>***</b></td><td></td></lc<>	-65	492		<u>`</u>	<b>***</b>			
COLUMN E-20B	<u> </u>		<u></u>	- <u></u>								
FRONT @ 2M	∦- <u></u> -	19	34	<lc< td=""><td>-130</td><td>484</td><td></td><td> </td><td></td><td></td></lc<>	-130	484						
BACK @ 2M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-454</td><td>440</td><td><u> </u></td><td><u> </u></td><td></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>-454</td><td>440</td><td><u> </u></td><td><u> </u></td><td></td><td></td></lc<>	-454	440	<u> </u>	<u> </u>				
SIDE @ 2M	<lc< td=""><td>-10</td><td>8</td><td><u></u></td><td>-97</td><td>488</td><td> </td><td>}</td><td></td><td></td></lc<>	-10	8	<u></u>	-97	488		}				
SIDE @ 2M	<lc< td=""><td>0</td><td>21</td><td><lc< td=""><td>-227</td><td>471</td><td></td><td> </td><td><b>#</b></td><td></td></lc<></td></lc<>	0	21	<lc< td=""><td>-227</td><td>471</td><td></td><td> </td><td><b>#</b></td><td></td></lc<>	-227	471			<b>#</b>			
	<lc< td=""><td>10</td><td></td><td><lc< td=""><td>0</td><td>500</td><td></td><td><u> </u></td><td></td><td><u> </u></td></lc<></td></lc<>	10		<lc< td=""><td>0</td><td>500</td><td></td><td><u> </u></td><td></td><td><u> </u></td></lc<>	0	500		<u> </u>		<u> </u>		
	<u>n - 20</u>						l	I	11			

Comments: SMEARS COUNTED 3-13-95. FRONT = NORTH SIDE . COLUMN A= SMALLER COLUMN. COLUMN B= LARGER COLUMN.

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

\$

Attachment 1: Bliss & Laughlin Steel Characterization Radiological Data

:

1

## Bliss and Laughlin Radiological Data

Sample Location	Date Collected	Analyte	Result	Error	Units	MDL	BNI Flag
BLS001	3/4/95	AM-241	2	0	PCI/G	2	UJ
BLS001	3/4/95	K-40	0.29	9.9	PCI/G	35.2	UJ
BLS001	3/4/95	RA-226	3.9	0	PCI/G	3.9	UJ
BLS001	3/4/95	RA-228	9.8	0	PCI/G	9.8	UJ
BLS001	3/4/95	TH-228	9.8	0	PCI/G	9.8	UJ
BLS001	3/4/95	TH-232	7.5	0	PCI/G	7.5	UJ
BLS001	3/4/95	U-234	- 71.1	22.5	PCI/G	0.36	J
BLS001	3/4/95	U-235	4.1	1.7	PC1/G	0.34	J
BLS001	3/4/95	U-238	- 73.3	23.2	PCI/G	0.28	t
BLS002	3/5/95	AM-241	0.4	0	PCI/G	0.4	UJ
BLS002	3/5/95	K-40	3.9	1.8	PCI/G	5.7	UJ
BLS002	3/5/95	RA-226	1.1	0.22	PCI/G	0.6	
BLS002	3/5/95	RA-228	1.7	0	PCI/G	1.7	UJ
BLS002	3/5/95	TH-228	1.7	0	PCI/G	1.7	UJ
BLS002	3/5/95	TH-232	0.67	0.44	PCI/G	0.9	UJ
BLS002	3/5/95	U-234	5.1	1.4	PCI/G	0.11	U
BLS002	3/5/95	U-235	0.29	0.18	PCI/G	0.12	J
BLS002	3/5/95	U-238	4.8	1.3	PCI/G	0.05	
BLS003	3/5/95	AM-241	0.3	0	PCI/G	0.3	υJ
BLS003	3/5/95	K-40	8.4	1	PCI/G	1.9	J
BLS003	3/5/95	RA-226	0.53	0.1	PCI/G	0.28	
BLS003	3/5/95	RA-228	0.7	0	PCI/G	- 0.7	ຸບຸ
BLS003	3/5/95	TH-228	0.7	0	PCI/G	0.7	ŪJ
BLS003	3/5/95	TH-232	0.56	0	PCI/G	0.56	UJ
BLS003	3/5/95	U-234	30.8	9.3	PCI/G	0.17	J
BLS003	3/5/95	U-235	1.1	0.5	PCI/G	0.09	J
BLS003	3/5/95	U-238	23.5	6.1	PCI/G	2.6	
BLS004	3/5/95	AM-241	0.76	. 0	PCI/G	0.76	UJ
BLS004	3/5/95	K-40	12.4	2.2	PCI/G	2.2	J
BLS004	3/5/95	RA-226	0.27	0.1	PCI/G	0.35	UJ
BLS004	3/5/95	RA-228	1.1	0	PCI/G	1.1	UJ
BLS004	3/5/95	TH-228	1.1	0	PCI/G	1.1	UJ
BLS004	3/5/95	TH-232	0.92	0	PCI/G	0.92	UJ
BLS004	3/5/95	U-234	- 89.9	35.6	PCI/G	0.24	J
BLS004	3/5/95	U-235	6.2	2.9	PCI/G	0.5	J
BLS004	3/5/95	U-238	- 90.5	35.9	PCI/G	0.47	J
BLS005	3/5/95	AM-241	0.33	0	PCI/G	0.33	UJ
BLS005	3/5/95	K-40	12.1	1.5	PCI/G	2.8	J
BLS005	3/5/95	RA-226	1.3	0.17	PCI/G	0.4	
BLS005	3/5/95	RA-228	1.2	0	PCI/G	1.2	UJ
BLS005	3/5/95	TH-228	1.2	0	PCI/G	1.2	UJ
BLS005	3/5/95	TH-232	0.87	0	PCI/G	0.87	UJ
BLS005	3/5/95	U-234	5	1.5	PCI/G	0.12	U
BLS005	3/5/95	U-235	0.31	0.2	PCI/G	0.12	J
BLS005	3/5/95	U-238	6	1.8	PCI/G	0.13	
BLS007	3/5/95	AM-241	0.49	0	PCI/G	0.49	UJ
BLS007	3/5/95	K-40	18.3	2.8	PCI/G	3.8	J
BLS007	3/5/95	RA-226	0.78	0	PCI/G	0.78	UJ
BLS007	3/5/95	RA-228	1.6	0	PCI/G	1.6	, UJ
BLS007	3/5/95	TH-228	1.6	0	PCI/G	1.6	UJ
BLS007	3/5/95	TH-232	1.3	Ó	PCI/G	1.3	υJ
BLS007	3/5/95	U-234	13.6	3.3	PCI/G	0.07	
BLS007	3/5/95	U-235	0.66	0.25	PCI/G	0.04	J
BLS007	3/5/95	U-238	15.3	3.7	PCI/G	0.03	





: ;)

## Bliss and Laughlin Radiological Data

Sample Location	Date Collected	Analyte	Result	Error	Units	MDL	BNI Flag
BLS008 BLS008 BLS008 BLS008 BLS008 BLS008 BLS008 BLS008 BLS008	3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	1.8 2.6 3.2 8.2 8.2 5.7 96.6 5.4 101.3	0 7.6 0 0 0 32.8 2.3 34.4	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	1.8 26.6 3.2 8.2 8.2 5.7 0.32 0.23 0.18	ר רח רח רח רח רח רח
BLS009 BLS009 BLS009 BLS009 BLS009 BLS009 BLS009 BLS009 BLS009	3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95 3/4/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.48 28 1.3 1.6 1.6 1.2 1.6 0.06 1.4	0 3.1 0.22 0 0 0.22 0.59 0.09 0.53	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.48 2.1 0.58 1.6 1.6 0.79 0.12 0.14 0.07	ח רת רח רח רח רח
BLS011 BLS011 BLS011 BLS011 BLS011 BLS011 BLS011 BLS011	3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95 3/5/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-232 U-234 U-235 U-238	0.56 21.8 1.9 1.9 1.4 1.9 0.07 1.9	0 2.6 0.3 0 0 0.54 0.07 0.55	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.56 2.6 0.68 1.9 1.9 1.4 0.07 0.08 0.04	רח ה רח רח רח רח
BLS014 BLS014 BLS014 BLS014 BLS014 BLS014 BLS014 BLS014 BLS014	2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-232 U-234 U-235 U-238	0.49 21.1 2.3 2.3 1.6 13 1.4 15.6	0 3.4 0 0 0 5.5 0.83 6.5	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.49 4.5 1 2.3 2.3 1.6 0.39 0.3 0.34	ר רח רח רח רח רח רח
BLS015 BLS015 BLS015 BLS015 BLS015 BLS015 BLS015 BLS015 BLS015	2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.64 17.8 1.2 2.7 2.7 2 12.4 0.69 11.8	0 3.7 0 0 0 5.3 0.53 5	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.64 7.2 1.2 2.7 2.7 2.7 0.27 0.39 0.16	ר רח רח רח רח רח רח רח
BLS016 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016 BLS016	2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95 2/25/95	AM-241 K-40 RA-226 RA-228 TH-228 TH-232 U-234 U-235 U-238	0.3 0.85 0.73 1.8 1.8 1.3 10.3 0.47 11.4	0 1.7 0 0 0 0 4.4 0.41 4.9	PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G PCI/G	0.3 5.8 0.73 1.8 1.8 1.3 0.26 0.32 0.26	







Sample Location	Date Collected	Analyte	Result	Error	Units	MDL	BNI Flag
	2/26/05	AM-241	37.2	0	PCI/G	37.2	UJ
BLS017	2/26/95	K-40	21.9	36.1	PCI/G	123	UJ -
BLS017	2/26/95	RA-226	23	0	PCI/G	23	UJ
BLS017	2/26/95	• • • –	39.2	Ō	PCI/G	39.2	UJ
BLS017	2/26/95	RA-228	39.2	ō	PCI/G	39.2	ບງ
BLS017	2/26/95	TH-228	35.1	õ	PCI/G	35.1	UJ
BLS017	2/26/95	TH-232	A	6664	PCI/G	64.7	
BLS017	2/26/95	U-234	24290	443.6	PCI/G	136.3	J
BLS017	2/26/95	U-235	1026	6471	PCI/G	64.4	
BLS017	2/26/95	U-238	1 23570	0471			
	0,005,005	AM-241	2.4	0	PCI/G	2.4	ÛĴ
BLS018	2/26/95	K-40	12.2	2.5	PCI/G	5.8	J
BLS018	2/26/95	• •	3.8	0.39	PCI/G	1.2	
BLS018	2/26/95	RA-226	1.8	0	PCI/G	1.8	UJ
BLS018	2/26/95	RA-228	0.75	1.7	PCI/G	1.8	UJ
BLS018	2/26/95	TH-228	3.8	1.6	PCI/G	1.1	J
BLS018	2/26/95	TH-232		490.8	PCI/G	91.9	
BLS018	2/26/95	U-234		84.2	PCI/G	113.3	UJ
BLS018	2/26/95	U-235	<b>41.8</b>	488.7	PCI/G	91.5	
BLS018	2/26/95	U-238	<b>P</b> 1215	400.1	. 00		

## Bliss and Laughlin Radiological Data

### Data Qualifier Flags

- J Estimate, qualitatively correct but quantitatively suspect
- R Reject, data are not suitable for any purpose.
- UJ Undetected-estimated.
- U Undetected. The blank's result is equal to the detection limit, or above the detection limit and the results of the sample are less than 5 times the blank's result.

Attachment 2: Bliss & Laughlin Steel Characterization Chemical Data

÷.

)

)

۰,

# Bliss and Laughlin Chemical Data

Sample Location	Date Collected	Analyte	Result	Units	BNI Flag	Lab Flag	DL	Matrix
	3/9/95	1,1-Dichloroethene	0.05	mg/l		U	0.05	W
BLS013		Chiorobenzene	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Vinyl Chloride	0.1	mg/l		U	0.1	W
BLS013	3/9/95	Chloroform	0.05	mg/l		U	0.05	W
BLS013	3/9/95	1,2-Dichloroethane	0.05	mg/l		U	0.05	W
BLS013	3/9/95	•	0.1	mg/l		U	0.1	W
BLS013	3/9/95	2-Butanone Carbon Tetrachloride	0.05	mg/l		U	0.05	W
BLS013	3/9/95		0.05	mg/l		U	0.05	W
BLS013	3/9/95	Trichloroethene	0.05	mg/l		U	0.05	W
BLS013	3/9/95	Benzene	0.05	mg/l		U	0.05	w
BLS013	3/9/95	Tetrachloroethene	2.5	ug/i	IJ	U ·	2.5	w
BLS013	3/10/95	Silver, TCLP Leachate	0.1	ug/l		Ū	0.1	w
BLS013	3/10/95	Mercury, TCLP Leachate	0.1	ug/l		U	0.5	w
BLS013	3/10/95	alpha-Chlordane		-		Ŭ	0.5	w
BLS013	3/10/95	Heptachlor	0.5	ug/l		Ŭ	44.4	w
BLS013	3/10/95	Selenium, TCLP Leachate	44.4	ug/l	υJ	U	20.5	w
BLS013	3/10/95	Lead, TCLP Leachate	20.5	ug/l	05	υ	0.5	W
BLS013	3/10/95	gamma-Chlordane	0.5	ug/l		=	2.9	w
BLS013	3/10/95	Chromium, TCLP Leachate	17.7	ug/l			3.5	w
BLS013	3/10/95	Cadmium, TCLP Leachate	3.5	ug/l	•	U	0.5	w
BLS013	3/10/95	gamma-BHC (Lindane)	0.5	ug/l		U	25.5	w
BLS013	3/10/95	Arsenic, TCLP Leachate	25.5	ug/l		U		w
BLS013	3/10/95	1,4-Dichlorobenzene	0.1	mg/l		U	0.1	Ŵ
BLS013	3/10/95	2,4,5-T	5	ug/l		U	5	Ŵ
BLS013	3/10/95	2,4,5-TP (Silvex)	5	ug/l		U	5	
BLS013	3/10/95	Barium, TCLP Leachate	866	ug/l	J	= .	2.8	W
BLS013	3/10/95	Nitrobenzene	0.1	mg/l		U	0.1	W
BLS013	3/10/95	Pentachlorophenol	0.5	mg/l		υ	0.5	W
	3/10/95	Hexachlorobenzene	0.1	mg/l		U	0.1	W
BLS013	3/10/95	2,4-Dinitrotoluene	0.1	mg/l		U	0.1	w
BLS013	3/10/95	2,4,5-Trichlorophenol	0.5	mg/l		U	0.5	w
BLS013	3/10/95	Heptachlor Epoxide	0.5	ug/l		U	0.5	w
BLS013		Hexachlorobutadiene	0.1	mg/l		U	0.1	w
BLS013	3/10/95	Endrin	1	ug/l		U	1	W
BLS013	3/10/95	Hexachloroethane	0.1	mg/l		U	0.1	W
BLS013	3/10/95		0.1	mg/l		U	0.1	w
BLS013	3/10/95	3- and/or 4-Methylphenol	0.1	mg/l		U	0.1	· w
BLS013	3/10/95	2-Methylphenol	0.1	mg/l		U	0.1	w
BLS013	3/10/95	Pyridine	10	ug/l		Ū	10	w
BLS013	3/10/95	2,4-D	10	ug/i ug/i		Ŭ	10	w
BLS013	3/10/95	Toxaphene	5	ug/l		U	5	w
BLS013	3/10/95	Methoxychlor				Ŭ	0.1	w
BLS013	3/10/95	2,4,6-Trichlorophenol	0.1	mg/l				





، ،



Attachment 3: DOE 5400.5, Figure IV-1 <u>Surface Contamination Guidelines</u>

1

;

Contamination	Guidelines	
· · ·	(dpm/100 c	$m^2$ ) <sup>1</sup> /
<u>Average</u> <sup>3/.4/</sup>	Maximum <sup>2</sup> ·2	<u>Removable</u> 4/.6/
RESERVED	RESERVED	RESERVED
1,000	3,000	200
5,000	15,000	1,000
5,000	15,000	1,000
	Contamination Allowable Tot <u>Average</u> 3/.4/ RESERVED 1,000 5,000	Contamination GuidelinesAllowable Total Residual Su (dpm/100 cd (dpm/100 cd Maximum4/.5/Average3/.1/Maximum4/.5/RESERVEDRESERVED1,0003,0005,00015,000

Figure IV-1

- As used in this table, dpm (disintegrations per minute) means the rate of 1/ emission by radioactive material as determined by correcting the counts per minute measured by an appropriate detector for background, efficiency, and geometric factors associated with the instrumentation.
- Where surface contamination by both alpha- and beta-gamma-emitting 2/ radionuclides exists, the limits established for alpha- and beta-gammaemitting radionuclides should apply independently.
- 3/\_\_\_\_ Measurements of average contamination should not be averaged over an area of more than 1  $m^2$ . For objects of less surface area, the average should be derived for each such object.
- The average and maximum dose rates associated with surface contamination 4/ resulting from beta-gamma emitters should not exceed 0.2 mrad/h and 1.0 mrad/h, respectively, at 1 cm.
- The maximum contamination level applies to an area of not more than 100 cm<sup>2</sup>. 5/

IV-6

Attachment 4: Bliss & Laughlin Steel Characterization

5-point Survey Data Special Finishing Area,

Survey of Elevated Locations in the Special finishing Area Identified by Floor Monitor Scans,

)

5-point Survey of Area in Grid E16

[		DIRECT					TR	ANSFER			
	ALPHA/100			GAMMA/1				SQCM			100 SQ CM
LOCATION/ITEM	SMPL	STD		SMPL	STD	SMI		STD		1PL	STD
COORDINATES	DPM	DEV		DPM	DEV	DP	<u>M</u>	DEV	DI	<u>PM</u>	DEV
N-0.5 E-0.5	29		<u> </u>	492	484						<u> </u>
N-0.5 E-1.5	29		<u> </u>	751		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-4</td><td>· · · ·</td></lc<></td></lc<>	-1		<lc< td=""><td>-4</td><td>· · · ·</td></lc<>	-4	· · · ·
N-0.5 E0.5	29			674		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-21</td><td>· ·</td></lc<></td></lc<>	2		<lc< td=""><td>-21</td><td>· ·</td></lc<>	-21	· ·
N-0.5 E1.5	<lc -7<="" td=""><td></td><td></td><td>907</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<></td></lc>			907	· · · · · · · · · · · · · · · · · · ·	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-50</td><td></td></lc<>	-50	
N-0.5 E10.5	39			0		<u> </u>			l		
N-0.5 E11.5	20		<lc< td=""><td>155</td><td>449</td><td></td><td></td><td></td><td>L</td><td></td><td>L</td></lc<>	155	449				L		L
N-0.5 E12.5	<lc 2<="" td=""><td></td><td></td><td>466</td><td>482</td><td></td><td></td><td></td><td></td><td></td><td></td></lc>			466	482						
N-0.5 E13.5	<lc 11<="" td=""><td>A</td><td><lc< td=""><td>233</td><td>457</td><td></td><td></td><td><b> </b></td><td>I</td><td></td><td><u> </u></td></lc<></td></lc>	A	<lc< td=""><td>233</td><td>457</td><td></td><td></td><td><b> </b></td><td>I</td><td></td><td><u> </u></td></lc<>	233	457			<b> </b>	I		<u> </u>
N-0.5 E14.5	20			389	474	11		L	l		<u> </u>
N-0.5 E15.5	48		<lc< td=""><td>285</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	285							
N-0.5 E16.5	20		<u> </u>	777		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>8</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>8</td><td></td></lc<>	8	
N-0.5 E17.5	<lc 11<="" td=""><td></td><td><lc< td=""><td>78</td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>78</td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	78	440						
N-0.5 E18.5	29			674	503	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-59</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-59</td><td></td></lc<>	-59	
N-0.5 E19.5	20	32	<lc< td=""><td>337</td><td>468</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	337	468						
N-0.5 E2.5	39	41		415	476						
N-0.5 E20.5	<lc -7<="" td=""><td>7</td><td><lc< td=""><td>52</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>	7	<lc< td=""><td>52</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	52	437						
N-0.5 E21.5	<lc 11<="" td=""><td></td><td><lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	363	471						
N-0.5 E3.5	29			440	479				l		
N-0.5 E4.5	39		<lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	363	471						
N-0.5 E5.5	<lc 11<="" td=""><td></td><td></td><td>751</td><td>510</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<></td></lc>			751	510	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-50</td><td></td></lc<>	-50	
N-0.5 E6.5	<lc 11<="" td=""><td></td><td><lc< td=""><td>104</td><td>443</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>104</td><td>443</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	104	443						
N-0.5 E7.5	<lc 2<="" td=""><td>2 19</td><td></td><td>959</td><td>530</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-54</td><td>· ·</td></lc<></td></lc<></td></lc>	2 19		959	530	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-54</td><td>· ·</td></lc<></td></lc<>	2	6	<lc< td=""><td>-54</td><td>· ·</td></lc<>	-54	· ·
N-0.5 E8.5	<lc 2<="" td=""><td>. 19</td><td><lc< td=""><td>181</td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>	. 19	<lc< td=""><td>181</td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	181	451						
N-0.5 E9.5	<lc -7<="" td=""><td>7</td><td><lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc>	7	<lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	363	471						
N-1.0 E-1.0	<lc 11<="" td=""><td></td><td></td><td>518</td><td>487</td><td></td><td></td><td></td><td></td><td></td><td></td></lc>			518	487						
N-1.0 E-2.0	<lc 11<="" td=""><td>27</td><td></td><td>700</td><td>505</td><td></td><td>5</td><td>88</td><td>&lt;Ľc</td><td>17</td><td></td></lc>	27		700	505		5	88	<Ľc	17	
N-1.0 E0.0	<lc 2<="" td=""><td></td><td></td><td>415</td><td>476</td><td></td><td></td><td></td><td></td><td></td><td></td></lc>			415	476						
N-1.0 E1.0	20	32	<lc< td=""><td>52</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	52	437						
N-1.0 E10.0	<lc 2<="" td=""><td></td><td></td><td>518</td><td>487</td><td></td><td></td><td></td><td></td><td></td><td></td></lc>			518	487						
N-1.0 E11.0	29	37	<lc< td=""><td>285</td><td>463</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	285	463	1					
N-1.0 E12.0	20	32		700	505	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-25</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-25</td><td></td></lc<>	-25	
N-1.0 E13.0	<pre>Lc 11</pre>	27		415	476						
N-1.0 E14.0	<lc 2<="" td=""><td>19</td><td><lc< td=""><td>207</td><td>454</td><td>1</td><td></td><td>[</td><td></td><td></td><td>1</td></lc<></td></lc>	19	<lc< td=""><td>207</td><td>454</td><td>1</td><td></td><td>[</td><td></td><td></td><td>1</td></lc<>	207	454	1		[			1
N-1.0 E15.0	20	32	<lc< td=""><td>104</td><td>443</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	104	443	1					
N-1.0 E16.0	<lc -7<="" td=""><td>7</td><td><lc< td=""><td>337</td><td>468</td><td></td><td></td><td></td><td></td><td></td><td>Î</td></lc<></td></lc>	7	<lc< td=""><td>337</td><td>468</td><td></td><td></td><td></td><td></td><td></td><td>Î</td></lc<>	337	468						Î
N-1.0 E17.0	<lc 2<="" td=""><td>19</td><td>1</td><td>440</td><td>479</td><td></td><td></td><td></td><td>l</td><td></td><td>1</td></lc>	19	1	440	479				l		1
N-1.0 E18.0	20		<lc< td=""><td>-104</td><td>419</td><td>1</td><td></td><td>[</td><td></td><td></td><td>1</td></lc<>	-104	419	1		[			1
N-1.0 E19.0	<lc 11<="" td=""><td></td><td><lc< td=""><td>363</td><td>471</td><td>1</td><td></td><td></td><td></td><td></td><td>1</td></lc<></td></lc>		<lc< td=""><td>363</td><td>471</td><td>1</td><td></td><td></td><td></td><td></td><td>1</td></lc<>	363	471	1					1
N-1.0 E2.0	<lc -7<="" td=""><td></td><td></td><td>440</td><td>A contract of the second s</td><td>1</td><td></td><td>[</td><td> </td><td></td><td>1</td></lc>			440	A contract of the second s	1		[			1
N-1.0 E20.0	<lc 11<="" td=""><td></td><td></td><td>389</td><td></td><td></td><td></td><td>[</td><td> </td><td></td><td>1 .</td></lc>			389				[			1 .
N-1.0 E21.0	<lc 2<="" td=""><td></td><td></td><td>389</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>1</td></lc>			389				1			1
N-1.0 E22.0	29		<lc< td=""><td>181</td><td></td><td></td><td></td><td> </td><td></td><td></td><td>1</td></lc<>	181							1
N-1.0 E3.0	<lc 11<="" td=""><td></td><td><lc< td=""><td>26</td><td></td><td></td><td></td><td>[</td><td></td><td>······</td><td>T</td></lc<></td></lc>		<lc< td=""><td>26</td><td></td><td></td><td></td><td>[</td><td></td><td>······</td><td>T</td></lc<>	26				[		······	T
N-1.0 E4.0	<lc 2<="" td=""><td></td><td></td><td>466</td><td></td><td></td><td></td><td>[</td><td></td><td></td><td>[</td></lc>			466				[			[
N-1.0 E5.0	<lc 11<="" td=""><td></td><td><lc< td=""><td>52</td><td></td><td></td><td></td><td>[</td><td></td><td></td><td>1</td></lc<></td></lc>		<lc< td=""><td>52</td><td></td><td></td><td></td><td>[</td><td></td><td></td><td>1</td></lc<>	52				[			1
N-1.0 E6.0	<lc 2<="" td=""><td></td><td></td><td>518</td><td></td><td></td><td></td><td></td><td>· · · ·</td><td>•</td><td>1</td></lc>			518					· · · ·	•	1
N-1.0 E7.0	<lc -7<="" td=""><td></td><td></td><td>415</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>1</td></lc>			415				1			1
N-1.0 E8.0	<lc -7<="" td=""><td></td><td></td><td>389</td><td></td><td></td><td></td><td></td><td></td><td></td><td>T</td></lc>			389							T
N-1.0 E9.0	48		<lc< td=""><td>-52</td><td></td><td></td><td></td><td>l</td><td></td><td></td><td>†</td></lc<>	-52				l			†
N-1.5 E-0.5	NA	NA	<u>  </u>	NA	NA	1		1			<u> </u>
N-1.5 E-1.5	NA	NA		NA	INA	1					<u>† .</u>
N-1.5 E0.5	NA	NA		NA	NA	#					t
N-1.5 E1.5	NA	NA		NA	NA NA	<u> </u>		<u>├</u> ────			f
N-1.5 E10.5	NA	NA NA	<b>  </b>	NA	NA	<b>*</b>		┝ <b>─</b> ──	f		

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

.

.,

)

ļ



١

i

1.1

ł

Г		DIRECT		· · · · · · · · · · · · · · · · · · ·	TR	ANSFER	ABLE	
-	ALPHA/100		BETA-GAMMA/10	0 SQ CM	ALPHA/100		BETA-GAMMA	100 SQ CM
LOCATION/ITEM	SMPL	ISTD	SMPL.	STD		STD	SMPL	STD
COORDINATES	DPM	DEV	DPM	DEV	· -	DEV	DPM	DEV
N-1.5 E11.5	NA	NA	NA	NA				1
N-1.5 E12.5	NA	NA	NA	NA				+
N-1.5 E13.5	NA	NA	NA	NA				
N-1.5 E14.5	NA	NA I	NA	NA				<del>-{</del>
N-1.5 E15.5	NA	NA	NA NA	NA				
	NA	NA	NA NA	NA				
N-1.5 E16.5								
N-1.5 E17.5	NA	NA	NA	NA				+
N-1.5 E18.5	<u>NA</u>	NA	NA	NA				<u> </u>
N-1.5 E19.5	NA	NA	NA	NA				
N-1.5 E2.5	<u>NA</u>	NA	NA	NA			·	
N-1.5 E20.5	NA	NA	NA	NA				
N-1.5 E21.5	<u>NA</u>	NA	NA	NA				
N-1.5 E3.5	NA	NA	NA	NA				<u> </u>
N-1.5 E4.5	<u>NA</u>	NA	NA	NA				ļ
N-1.5 E5.5	<u>NA</u>	NA	NA	NA				L
N-1.5 E6.5	NA	NA	NA	NA				
N-1.5 E7.5	NA	NA	NA	NA				
N-1.5 E8.5	NA	NA	NA	NA				
N-1.5 E9.5	NA	NA	NA	NA				
N-2.0 E-1.0	NA	NA	NA	NA				
N-2.0 E-2.0	NA	NA	NA	NA				
N-2.0 E0.0	NA	NA	NA	NA			1	1
N-2.0 E1.0	NA	NA	NĂ	NA				
N-2.0 E10.0	NA	NA	NA	NA				1
N-2.0 E11.0	NA	NA	NA	NA	<u> </u>			
N-2.0 E12.0	NA	NA	NA	NA				1
N-2.0 E13.0	NA	NA	NA	NA				+
N-2.0 E14.0	NA	NA	NA	NA	·			
N-2.0 E15.0	NA	NA	NA	NA				
N-2.0 E16.0	NA	NA	NA NA	NA				
N-2.0 E17.0	NA	NA	NA	NA				
N-2.0 E18.0	NA NA	NA	NA	NA	· · · · · · · · · · · · - ·		l	
N-2.0 E19.0	<u>NA</u>	NA	NA NA	NA				
N-2.0 E 19.0					) 			- <del> </del>
	<u>NA</u>	NA	NA	NA				
N-2.0 E20.0	<u>NA</u>	NA	NA	NA				
N-2.0 E21.0	NA	NA	NA	NA				
N-2.0 E22.0	NA	NA	NA	NA				
N-2.0 E3:0	<u>NA</u>	NA	NA	NA	l		l	
N-2.0 E4.0	NA	NA	NA	NA			L	
N-2.0 E5.0	<u>NA</u>	NA	NA	NA				
N-2.0 E6.0	NA	NA	NA	NA				
N-2.0 E7.0	NA	NA	NA	NA				
N-2.0 E8.0	NA	NA	NA	NA			l	
N-2.0 E9.0	NA	NA	NA	NA				
N0.0 E-1.0	29	37	415	476				
	<lc 11<="" td=""><td>27</td><td>570</td><td>492</td><td></td><td></td><td></td><td></td></lc>	27	570	492				
	<lc -4<="" td=""><td>and the second se</td><td>544</td><td>457</td><td></td><td></td><td></td><td></td></lc>	and the second se	544	457				
N0.0 E1.0	42			484	<lc 2<="" td=""><td>· 6</td><td><lc -13<="" td=""><td>3 7</td></lc></td></lc>	· 6	<lc -13<="" td=""><td>3 7</td></lc>	3 7
	<lc 6<="" td=""><td></td><td><lc 155<="" td=""><td>413</td><td>the second s</td><td></td><td> </td><td>1</td></lc></td></lc>		<lc 155<="" td=""><td>413</td><td>the second s</td><td></td><td> </td><td>1</td></lc>	413	the second s			1
	<lc -4<="" td=""><td></td><td><lc 259<="" td=""><td>425</td><td></td><td></td><td></td><td></td></lc></td></lc>		<lc 259<="" td=""><td>425</td><td></td><td></td><td></td><td></td></lc>	425				
	<lc 6<="" td=""><td>the second se</td><td><lc 259<="" td=""><td>425</td><td></td><td></td><td></td><td>1</td></lc></td></lc>	the second se	<lc 259<="" td=""><td>425</td><td></td><td></td><td></td><td>1</td></lc>	425				1
	<lc 0<br=""><lc 15<="" td=""><td></td><td></td><td>451</td><td></td><td></td><td></td><td>+</td></lc></lc>			451				+
	< <u>LC</u> -3		492 <	413				- <u>+</u>
		i ZUI	i∿LG 100	413			0	1

<Lc indicates less than the critical level of activity which can be said to be above background.</pre>

A negative value is the calculated result of a reading which is below the instrument-specific background.

(		DIRECT				TR	ANSFER	ABLE	
	ALPHA/100		BET	A-GAMMA/1		ALPHA/100		BETA-GAMMA	
LOCATION/ITEM	SMPL	STD		SMPL	STD	SMPL	STD	SMPL	STD
COORDINATES	DPM	DEV		DPM	DEV	DPM	DEV	DPM	DEV
N0.0 E16.0	33	8 41		492	451				
N0.0 E17.0	<lc 15<="" td=""><td>5 33</td><td><lc< td=""><td>285</td><td>428</td><td></td><td></td><td></td><td></td></lc<></td></lc>	5 33	<lc< td=""><td>285</td><td>428</td><td></td><td></td><td></td><td></td></lc<>	285	428				
N0.0 E18.0	24	37	<lc< td=""><td>311</td><td>431</td><td></td><td></td><td></td><td></td></lc<>	311	431				
N0.0 E19.0	<lc 15<="" td=""><td>5 33</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td></td></lc>	5 33		518	454				
N0.0 E2.0	<lc 15<="" td=""><td>5 33</td><td></td><td>337</td><td>434</td><td></td><td></td><td></td><td></td></lc>	5 33		337	434				
N0.0 E20.0	<lc 6<="" td=""><td>6 27</td><td><lc< td=""><td>155</td><td>413</td><td></td><td></td><td></td><td></td></lc<></td></lc>	6 27	<lc< td=""><td>155</td><td>413</td><td></td><td></td><td></td><td></td></lc<>	155	413				
N0.0 E21.0	<lc -4<="" td=""><td>1 20</td><td><lc< td=""><td>259</td><td>425</td><td></td><td>T</td><td></td><td></td></lc<></td></lc>	1 20	<lc< td=""><td>259</td><td>425</td><td></td><td>T</td><td></td><td></td></lc<>	259	425		T		
N0.0 E22.0	<lc 6<="" td=""><td>3 27</td><td><lc< td=""><td>259</td><td>425</td><td></td><td></td><td></td><td></td></lc<></td></lc>	3 27	<lc< td=""><td>259</td><td>425</td><td></td><td></td><td></td><td></td></lc<>	259	425				
N0.0 E3.0	6	52		440	446				
N0.0 E4.0	<lc (<="" td=""><td>3 27</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td></td></lc>	3 27		518	454				
N0.0 E5.0	<lc 15<="" td=""><td>5 33</td><td></td><td>466</td><td>449</td><td></td><td></td><td>1</td><td></td></lc>	5 33		466	449			1	
N0.0 E6.0	24	1 37	1	492	451		1	1	
N0.0 E7.0	33	41		803	484	<lc -1<="" td=""><td>0</td><td><pre></pre><pre>4</pre></td><td>6 8</td></lc>	0	<pre></pre> <pre>4</pre>	6 8
N0.0 E8.0	<lc -13<="" td=""><td>3 10</td><td></td><td>492</td><td></td><td></td><td></td><td>1</td><td></td></lc>	3 10		492				1	
N0.0 E9.0	<lc (<="" td=""><td></td><td></td><td>440</td><td>÷</td><td></td><td>1</td><td></td><td></td></lc>			440	÷		1		
N0.5 E-0.5	29		li	415		1	1	<b> </b>	
N0.5 E-1.5			1	389		l	1	1	
N0.5 E0.5	<lc -4<="" td=""><td></td><td></td><td>440</td><td></td><td></td><td><u>†                                    </u></td><td></td><td></td></lc>			440			<u>†                                    </u>		
N0.5 E1.5	33		<lc< td=""><td>311</td><td>431</td><td></td><td></td><td>1</td><td></td></lc<>	311	431			1	
N0.5 E10.5	<lc 1<="" td=""><td></td><td><lc< td=""><td>207</td><td>419</td><td></td><td>t</td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>207</td><td>419</td><td></td><td>t</td><td></td><td></td></lc<>	207	419		t		
N0.5 E11.5	<lc 1<="" td=""><td></td><td></td><td>389</td><td></td><td></td><td></td><td>1</td><td></td></lc>			389				1	
N0.5 E12.5	42		<lc< td=""><td>181</td><td>416</td><td></td><td></td><td></td><td></td></lc<>	181	416				
N0.5 E13.5	<lc -4<="" td=""><td></td><td><lc< td=""><td>26</td><td></td><td></td><td>†</td><td></td><td></td></lc<></td></lc>		<lc< td=""><td>26</td><td></td><td></td><td>†</td><td></td><td></td></lc<>	26			†		
N0.5 E14.5	24	4 37		596	4		1		
N0.5 E15.5	<lc 1<="" td=""><td></td><td><lc< td=""><td>130</td><td></td><td>1</td><td><u> </u></td><td>1</td><td></td></lc<></td></lc>		<lc< td=""><td>130</td><td></td><td>1</td><td><u> </u></td><td>1</td><td></td></lc<>	130		1	<u> </u>	1	
N0.5 E16.5		5 27		674					
N0.5 E17.5	4:			518			<u> </u>	1	
N0.5 E18.5	3		<lc< td=""><td>104</td><td></td><td></td><td>†</td><td>1</td><td></td></lc<>	104			†	1	
N0.5 E19.5	<lc 1<="" td="" ·=""><td></td><td></td><td>570</td><td></td><td></td><td></td><td>1</td><td></td></lc>			570				1	
N0.5 E2.5	<lc 1<="" td=""><td></td><td><u>  </u></td><td>725</td><td></td><td></td><td></td><td>1</td><td></td></lc>		<u>  </u>	725				1	
N0.5 E20.5	<lc 1<="" td=""><td></td><td><lc< td=""><td>207</td><td>419</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><u> </u></td><td>1</td><td></td></lc<></td></lc>		<lc< td=""><td>207</td><td>419</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><u> </u></td><td>1</td><td></td></lc<>	207	419	· · · · · · · · · · · · · · · · · · ·	<u> </u>	1	
N0.5 E21.5	<lc 1<="" td=""><td></td><td></td><td>389</td><td></td><td></td><td></td><td></td><td></td></lc>			389					
N0.5 E3.5	<lc -4<="" td=""><td></td><td>  </td><td>492</td><td></td><td></td><td><u> </u></td><td>1</td><td></td></lc>			492			<u> </u>	1	
N0.5 E4.5	3			570				1	
N0.5 E5.5		5 27	╫	544			<u> </u>	1	
N0.5 E6.5	3:	_	<lc< td=""><td>259</td><td></td><td></td><td><u> </u></td><td><u>  </u></td><td></td></lc<>	259			<u> </u>	<u>  </u>	
	<lc 1<="" td=""><td></td><td></td><td>1425</td><td></td><td><lc 2<="" td=""><td></td><td><lc -4<="" td=""><td>6</td></lc></td></lc></td></lc>			1425		<lc 2<="" td=""><td></td><td><lc -4<="" td=""><td>6</td></lc></td></lc>		<lc -4<="" td=""><td>6</td></lc>	6
N0.5 E8.5	6			544			<sup>0</sup>	1 ~ L C -4	<u> </u>
N0.5 E9.5	<lc -4<="" td=""><td></td><td></td><td>907</td><td></td><td>0</td><td></td><td><lc< td=""><td>0</td></lc<></td></lc>			907		0		<lc< td=""><td>0</td></lc<>	0
N1.0 E-1.0			<lc< td=""><td>233</td><td></td><td></td><td><u>├</u>°</td><td></td><td></td></lc<>	233			<u>├</u> °		
N1.0 E-2.0	<lc 1<="" td=""><td></td><td></td><td>674</td><td></td><td><lc -1<="" td=""><td>0</td><td>7</td><td>1</td></lc></td></lc>			674		<lc -1<="" td=""><td>0</td><td>7</td><td>1</td></lc>	0	7	1
							ļ	·	-'}
N1.0 E0.0	<lc< td=""><td></td><td><lc< td=""><td>181</td><td></td><td></td><td><del> </del></td><td><b></b></td><td></td></lc<></td></lc<>		<lc< td=""><td>181</td><td></td><td></td><td><del> </del></td><td><b></b></td><td></td></lc<>	181			<del> </del>	<b></b>	
N1.0 E1.0	24			4949			+	<u>H</u>	
N1.0 E10.0	3:		<lc< td=""><td>104</td><td></td><td></td><td><u> </u></td><td><u>8</u> H</td><td></td></lc<>	104			<u> </u>	<u>8</u> H	
N1.0 E11.0	24		<lc< td=""><td>311</td><td></td><td></td><td><b> </b></td><td><u> </u></td><td></td></lc<>	311			<b> </b>	<u> </u>	
N1.0 E12.0	4			518			<u> </u>	<u>H</u>	
N1.0 E13.0	<lc 1<="" td=""><td></td><td><lc< td=""><td>285</td><td></td><td></td><td><del> </del></td><td><u> </u></td><td></td></lc<></td></lc>		<lc< td=""><td>285</td><td></td><td></td><td><del> </del></td><td><u> </u></td><td></td></lc<>	285			<del> </del>	<u> </u>	
N1.0 E14.0		3 27	H	674			<b> </b>	<b></b>	
N1.0 E15.0	3:			492			<u> </u>	<b>#</b>	
N1.0 E16.0	<lc 1<="" td=""><td></td><td><lc< td=""><td>130</td><td></td><td></td><td><u> </u></td><td><u> </u></td><td></td></lc<></td></lc>		<lc< td=""><td>130</td><td></td><td></td><td><u> </u></td><td><u> </u></td><td></td></lc<>	130			<u> </u>	<u> </u>	
N1.0 E17.0	<lc -1<="" td=""><td></td><td><lc< td=""><td>104</td><td></td><td></td><td><u> </u></td><td>ļ</td><td></td></lc<></td></lc>		<lc< td=""><td>104</td><td></td><td></td><td><u> </u></td><td>ļ</td><td></td></lc<>	104			<u> </u>	ļ	
N1.0 E18.0	24			596					
N1.0 E19.0	<lc -4<="" td=""><td>4 20</td><td><lc< td=""><td>155</td><td>413</td><td><lc 2<="" td=""><td></td><td></td><td>1</td></lc></td></lc<></td></lc>	4 20	<lc< td=""><td>155</td><td>413</td><td><lc 2<="" td=""><td></td><td></td><td>1</td></lc></td></lc<>	155	413	<lc 2<="" td=""><td></td><td></td><td>1</td></lc>			1
N1.0 E2.0	<lc -4<="" td=""><td>1 20</td><td>1</td><td>1114</td><td>515</td><td><lc 2<="" td=""><td></td><td><lc -1<="" td=""><td>7</td></lc></td></lc></td></lc>	1 20	1	1114	515	<lc 2<="" td=""><td></td><td><lc -1<="" td=""><td>7</td></lc></td></lc>		<lc -1<="" td=""><td>7</td></lc>	7

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

÷,

			DIRECT							ANSFER	ABLE			
			SQCM	_	-GAMMA/10	_	CM		_	SQCM		SAMMA/		CN
LOCATION/ITEM			STD		SMPL	STD		SMF		STD		IPL	STD	
COORDINATES	D	PM	DEV	L	DPM	DEV		DPI	M	DEV	DF	PM	DEV	
N1.0 E20.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>26</td><td></td><td>397</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>26</td><td></td><td>397</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	26		397							
N1.0 E21.0	<lc< td=""><td>15</td><td>33</td><td></td><td>492</td><td></td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33		492		451							
N1.0 E22		42	45	<lc< td=""><td>181</td><td></td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	181		416							
N1.0 E3.0	<lc< td=""><td>15</td><td>33</td><td></td><td>518</td><td></td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33		518		454							
N1.0 E4.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>233</td><td></td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>233</td><td></td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	233		422							
N1.0 E5.0	<lc< td=""><td>15</td><td>33</td><td></td><td>544</td><td></td><td>457</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	15	33		544		457						1	
N1.0 E6.0	<lc< td=""><td>-4</td><td></td><td></td><td>777</td><td></td><td>482</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-46</td><td></td><td>7</td></lc<></td></lc<></td></lc<>	-4			777		482	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-46</td><td></td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>-46</td><td></td><td>7</td></lc<>	-46		7
N1.0 E7.0		24	37		674		471							
N1.0 E8.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>104</td><td></td><td>406</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6		<lc< td=""><td>104</td><td></td><td>406</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	104		406							
N1.0 E9.0	<lc< td=""><td>15</td><td></td><td><lc< td=""><td>233</td><td></td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	15		<lc< td=""><td>233</td><td></td><td>422</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	233		422							
N1.5 E-0.5	<lc< td=""><td>-7</td><td>7</td><td></td><td>492</td><td></td><td>484</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-7	7		492		484							
N1.5 E-1.5	<lc< td=""><td>2</td><td>19</td><td><lc< td=""><td>78</td><td></td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2	19	<lc< td=""><td>78</td><td></td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	78		440							
N1.5 E0.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>134</td><td></td><td>442</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9	35	<lc< td=""><td>134</td><td></td><td>442</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	134		442							
N1.5 E1.5	<lc< td=""><td>18</td><td></td><td><lc< td=""><td>-134</td><td></td><td>410</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	18		<lc< td=""><td>-134</td><td></td><td>410</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-134		410							
N1.5 E10.5	<lc< td=""><td>28</td><td>50</td><td></td><td>857</td><td></td><td>519</td><td><lc< td=""><td>-1</td><td>· 0</td><td><lc< td=""><td>-59</td><td></td><td>(</td></lc<></td></lc<></td></lc<>	28	50		857		519	<lc< td=""><td>-1</td><td>· 0</td><td><lc< td=""><td>-59</td><td></td><td>(</td></lc<></td></lc<>	-1	· 0	<lc< td=""><td>-59</td><td></td><td>(</td></lc<>	-59		(
N1.5 E11.5	<lc< td=""><td>9</td><td>43</td><td></td><td>482</td><td></td><td>481</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		482		481							
N1.5 E12.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>1017</td><td></td><td>535</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>4</td><td></td><td></td></lc<></td></lc<></td></lc<>	-18	30		1017		535	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>4</td><td></td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>4</td><td></td><td></td></lc<>	4		
N1.5 E13.5	<lc< td=""><td>0</td><td>40</td><td><lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>	0	40	<lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	321		463						1	
N1.5 E14.5	<lc< td=""><td>18</td><td>47</td><td></td><td>857</td><td></td><td>519</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-17</td><td>1</td><td></td></lc<></td></lc<></td></lc<>	18	47		857		519	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-17</td><td>1</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-17</td><td>1</td><td></td></lc<>	-17	1	
N1.5 E15.5	<lc< td=""><td>-18</td><td>30</td><td>11</td><td>883</td><td></td><td>522</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-29</td><td>1</td><td></td></lc<></td></lc<></td></lc<>	-18	30	11	883		522	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-29</td><td>1</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-29</td><td>1</td><td></td></lc<>	-29	1	
N1.5 E16.5		NA	NA		NA	NA							1	
N1.5 E17.5		NA	NA	1	NA	NA								
N1.5 E18.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>696</td><td></td><td>503</td><td></td><td></td><td> </td><td></td><td></td><td>1</td><td></td></lc<>	-18	30		696		503						1	
N1.5 E19.5	<lc< td=""><td>0</td><td>40</td><td>1</td><td>375</td><td></td><td>469</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	0	40	1	375		469						1	
N1.5 E2.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>375</td><td></td><td>469</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	-18	30		375		469						1	
N1.5 E20.5	<lc< td=""><td>0</td><td>40</td><td>1</td><td>1365</td><td>1</td><td>568</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>29</td><td></td><td></td></lc<></td></lc<></td></lc<>	0	40	1	1365	1	568	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>29</td><td></td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>29</td><td></td><td></td></lc<>	29		
N1.5 E21.5	<lc< td=""><td>0</td><td>40</td><td><lc< td=""><td>294</td><td></td><td>460</td><td></td><td></td><td>[</td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>	0	40	<lc< td=""><td>294</td><td></td><td>460</td><td></td><td></td><td>[</td><td></td><td></td><td>1</td><td></td></lc<>	294		460			[			1	
N1.5 E3.5	<lc< td=""><td>9</td><td>43</td><td><lc.< td=""><td>214</td><td>1</td><td>451</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc.<></td></lc<>	9	43	<lc.< td=""><td>214</td><td>1</td><td>451</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc.<>	214	1	451						1	
N1.5 E4.5	<lc< td=""><td>-18</td><td>30</td><td>li</td><td>830</td><td>t</td><td>517</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>8</td><td></td><td></td></lc<></td></lc<></td></lc<>	-18	30	li	830	t	517	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>8</td><td></td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>8</td><td></td><td></td></lc<>	8		
N1.5 E5.5		37	54	1	642		498						1	
N1.5 E6.5	<lc< td=""><td>-18</td><td></td><td></td><td>910</td><td>·</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>38</td><td>1</td><td></td></lc<></td></lc<></td></lc<>	-18			910	·		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>38</td><td>1</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>38</td><td>1</td><td></td></lc<>	38	1	
N1.5 E7.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>294</td><td>t</td><td>460</td><td><u> </u></td><td></td><td><u> </u></td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>	0		<lc< td=""><td>294</td><td>t</td><td>460</td><td><u> </u></td><td></td><td><u> </u></td><td></td><td></td><td>1</td><td></td></lc<>	294	t	460	<u> </u>		<u> </u>			1	
N1.5 E8.5	<lc< td=""><td>9</td><td></td><td></td><td>589</td><td>f</td><td>492</td><td> </td><td></td><td></td><td></td><td></td><td>+</td><td></td></lc<>	9			589	f	492						+	
N1.5 E9.5	<lc< td=""><td>-9</td><td></td><td></td><td>455</td><td> </td><td>478</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	-9			455		478						1	
N10.0 E-1.0	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>337</td><td><u> </u></td><td>468</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>337</td><td><u> </u></td><td>468</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	337	<u> </u>	468						<u> </u>	
N10.0 E-2.0		20		<lc< td=""><td>259</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>+</td><td></td></lc<>	259		460						+	
N10.0 E1.0	1	NA	NA	∦- <u></u> -	<u></u>	NA				<u>+</u>		<u>-</u>		
N10.0 E10.0	<lc< td=""><td>19</td><td></td><td>l </td><td>1040</td><td></td><td>611</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-4</td><td>1</td><td></td></lc<></td></lc<></td></lc<>	19		l	1040		611	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-4</td><td>1</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-4</td><td>1</td><td></td></lc<>	-4	1	
N10.0 E11.0	<lc< td=""><td>10</td><td></td><td><u> </u></td><td>917</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>0</td><td></td><td></td></lc<></td></lc<></td></lc<>	10		<u> </u>	917			<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>0</td><td></td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>0</td><td></td><td></td></lc<>	0		
N10.0 E12.0	<lc< td=""><td>-19</td><td></td><td></td><td>520</td><td></td><td>559</td><td></td><td><u> </u></td><td><u> </u></td><td></td><td></td><td><u>†</u></td><td></td></lc<>	-19			520		559		<u> </u>	<u> </u>			<u>†</u>	
N10.0 E13.0	<lc< td=""><td>-48</td><td></td><td></td><td>734</td><td></td><td>581</td><td></td><td></td><td><u> </u></td><td></td><td></td><td>1</td><td></td></lc<>	-48			734		581			<u> </u>			1	
N10.0 E14.0	<lc< td=""><td>-48</td><td></td><td></td><td>703</td><td></td><td>578</td><td></td><td></td><td><u> </u></td><td></td><td></td><td>1</td><td></td></lc<>	-48			703		578			<u> </u>			1	
N10.0 E15.0	<lc< td=""><td>-39</td><td></td><td><lc< td=""><td>183</td><td></td><td>522</td><td></td><td></td><td><u>├───</u>─</td><td></td><td></td><td>†</td><td></td></lc<></td></lc<>	-39		<lc< td=""><td>183</td><td></td><td>522</td><td></td><td></td><td><u>├───</u>─</td><td></td><td></td><td>†</td><td></td></lc<>	183		522			<u>├───</u> ─			†	
N10.0 E16.0	<lc< td=""><td>29</td><td></td><td></td><td>459</td><td></td><td>553</td><td></td><td></td><td></td><td></td><td><u> </u></td><td><del> </del></td><td></td></lc<>	29			459		553					<u> </u>	<del> </del>	
N10.0 E17.0		NA	NA 00	#	NA 400	NA				· · ·			t	
N10.0 E18.0		NA	NA NA	╫	NA	NA				<u> </u>			+	
N10.0 E19.0		NA	NA	#	NA	NA			· · · · · · · · · · · · · · · · · · ·	<u> </u>			1	
N10.0 E2.0		NA	NA	╫────	NA	NA				<u> </u>			+	
N10.0 E20.0	· · · · · · · · · · · · · · · · · · ·	NA	NA NA	<u> </u>		NA				<u> </u>			<u>+</u>	
N10.0 E21.0		NA	NA	╫	NA NA	NA				<u> </u>			<u> </u>	
N10.0 E22.0	<lc< td=""><td>-10</td><td></td><td><lc< td=""><td>214</td><td>÷</td><td>526</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></lc<></td></lc<>	-10		<lc< td=""><td>214</td><td>÷</td><td>526</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td></lc<>	214	÷	526					<u> </u>		
N10.0 E3.0	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>214</td><td></td><td>526</td><td></td><td></td><td><u>├</u>────</td><td></td><td></td><td>ł</td><td></td></lc<></td></lc<>	0		<lc< td=""><td>214</td><td></td><td>526</td><td></td><td></td><td><u>├</u>────</td><td></td><td></td><td>ł</td><td></td></lc<>	214		526			<u>├</u> ────			ł	
N10.0 E4.0					703		526 578				l		+	
IVIUUE4.U	<lc< td=""><td>-29</td><td>1 38</td><td>11</td><td>103</td><td>1</td><td>210</td><td>1</td><td></td><td>1</td><td>ł</td><td></td><td>1</td><td></td></lc<>	-29	1 38	11	103	1	210	1		1	ł		1	

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

.

,

1

			DIRECT						TR	ANSFER	ABLE		
	ALF	PHA/100	SQCM	BET	A-GAMMA/1	00 SC	2 CM	ALPHA	/100	SQ CM	BET	A-GAMMA/	100 SQ CN
LOCATION/ITEM	S	MPL	STD		SMPL	STD	)	SMP	L	STD		SMPL	STD
COORDINATES		DPM	DEV		DPM	DEV	/	DPN	1	DEV		DPM	DEV
N10.0 E6.0	<lc< td=""><td>0</td><td>51</td><td><lc< td=""><td>-122</td><td></td><td>487</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0	51	<lc< td=""><td>-122</td><td></td><td>487</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-122		487						
N10.0 E7.0	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-39	34	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	397		546						
N10.0 E8.0	<lc< td=""><td>10</td><td>54</td><td><lc< td=""><td>61</td><td></td><td>509</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	10	54	<lc< td=""><td>61</td><td></td><td>509</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	61		509						
N10.0 E9.0	<lc< td=""><td>-48</td><td>28</td><td><lc< td=""><td>306</td><td></td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-48	28	<lc< td=""><td>306</td><td></td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	306		536						
N10.5 E-0.5	<lc< td=""><td>11</td><td>27</td><td></td><td>751</td><td></td><td>510</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-67</td><td></td></lc<></td></lc<></td></lc<>	11	27		751		510	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-67</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-67</td><td></td></lc<>	-67	
N10.5 E-1.5	<lc< td=""><td>11</td><td>27</td><td><lc< td=""><td>259</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td>·<u> </u></td><td>]</td></lc<></td></lc<>	11	27	<lc< td=""><td>259</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td>·<u> </u></td><td>]</td></lc<>	259		460					· <u> </u>	]
N10.5 E0.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>294</td><td>[</td><td>460</td><td>·····</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<></td></lc<>	-9	35	<lc< td=""><td>294</td><td>[</td><td>460</td><td>·····</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	294	[	460	·····					<u> </u>
N10.5 E1.5		NĀ	NA		NA	NA							
N10.5 E10.5	<lc< td=""><td>18</td><td>47</td><td></td><td>776</td><td></td><td>511</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>25</td><td>· · · ·</td></lc<></td></lc<></td></lc<>	18	47		776		511	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>25</td><td>· · · ·</td></lc<></td></lc<>	-1	0	<lc< td=""><td>25</td><td>· · · ·</td></lc<>	25	· · · ·
N10.5 E11.5		46			723		506					·	t
N10.5 E12.5	<lc< td=""><td>0</td><td></td><td></td><td>482</td><td></td><td>481</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	0			482		481						<u> </u>
N10.5 E13.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td><u> </u></td><td><u> </u></td><td></td><td></td></lc<></td></lc<>	9		<lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td><u> </u></td><td><u> </u></td><td></td><td></td></lc<>	321		463			<u> </u>	<u> </u>		
N10.5 E14.5	<lc< td=""><td>-28</td><td></td><td><lc< td=""><td>161</td><td></td><td>445</td><td></td><td></td><td></td><td></td><td>······································</td><td><u> </u></td></lc<></td></lc<>	-28		<lc< td=""><td>161</td><td></td><td>445</td><td></td><td></td><td></td><td></td><td>······································</td><td><u> </u></td></lc<>	161		445					······································	<u> </u>
N10.5 E15.5	<lc< td=""><td>28</td><td></td><td></td><td>375</td><td></td><td>469</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	28			375		469						
N10.5 E16.5	<lc< td=""><td>28</td><td></td><td><u>}</u></td><td>803</td><td></td><td>514</td><td></td><td></td><td>{</td><td></td><td></td><td><u> </u></td></lc<>	28		<u>}</u>	803		514			{			<u> </u>
N10.5 E17.5	<lc< td=""><td>20</td><td></td><td><lc< td=""><td>-80</td><td></td><td>416</td><td></td><td>-1</td><td></td><td><lc< td=""><td>-13</td><td></td></lc<></td></lc<></td></lc<>	20		<lc< td=""><td>-80</td><td></td><td>416</td><td></td><td>-1</td><td></td><td><lc< td=""><td>-13</td><td></td></lc<></td></lc<>	-80		416		-1		<lc< td=""><td>-13</td><td></td></lc<>	-13	
N10.5 E18.5	I-LC	37		-20	616		495				<lc< td=""><td>8</td><td></td></lc<>	8	
N10.5 E19.5	╟───	NA 37	NA 54		010	NA	495		- 1				<u> </u>
	╟───-										<u> </u>		<u> </u>
N10.5 E2.5	i—	NA	NA	<b>[</b>	NA	NA					<b> </b>		Ļ
N10.5 E20.5	∦	NA	NA		<u>NA</u>	NA					<b> </b>		ļ
N10.5 E21.5	<b>  </b>	NA	NA	<b>  </b>	NA	NA		Į			<b> </b>	. <u></u>	ļ
N10.5 E3.5	l	NA	NA	<b> </b>	NA	NA					<u> </u>		ļ
N10.5 E4.5	li	NA	NA	<b> </b>	NA	NA					ľ		ļ
N10.5 E5.5	<lc< td=""><td>9</td><td></td><td></td><td>535</td><td>L</td><td>487</td><td></td><td></td><td></td><td></td><td></td><td>L</td></lc<>	9			535	L	487						L
N10.5 E6.5	<lc< td=""><td>28</td><td></td><td><lc< td=""><td>161</td><td>L</td><td>445</td><td></td><td></td><td></td><td></td><td></td><td>ļ</td></lc<></td></lc<>	28		<lc< td=""><td>161</td><td>L</td><td>445</td><td></td><td></td><td></td><td></td><td></td><td>ļ</td></lc<>	161	L	445						ļ
N10.5 E7.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>348</td><td></td><td>_382</td><td></td><td></td><td></td><td></td><td></td><td><u></u></td></lc<></td></lc<>	0		<lc< td=""><td>348</td><td></td><td>_382</td><td></td><td></td><td></td><td></td><td></td><td><u></u></td></lc<>	348		_382						<u></u>
N10.5 E8.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>80</td><td></td><td>436</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9	35	<lc< td=""><td>80</td><td></td><td>436</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	80		436						
N10.5 E9.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>54</td><td></td><td>433</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0		<lc< td=""><td>54</td><td></td><td>433</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	54		433						
N11.0 E-1.0	<lc< td=""><td>-7</td><td></td><td></td><td>415</td><td></td><td>476</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-7			415		476						
N11.0 E-2.0		20	32	<lc< td=""><td>-104</td><td></td><td>419</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-104		419						
N11.0 E0.0	<lc< td=""><td>6</td><td>27</td><td></td><td>415</td><td></td><td>443</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	6	27		415		443						
N11.0 E1.0		24	37	<lc< td=""><td>52</td><td></td><td>400</td><td></td><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td></lc<>	52		400					· · · · · · · · · · · · · · · · · · ·	
N11.0 E10.0	<lc< td=""><td>-13</td><td>10</td><td><lc< td=""><td>181</td><td></td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-13	10	<lc< td=""><td>181</td><td></td><td>416</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	181		416						
N11.0 E11.0	<lc< td=""><td>15</td><td>33</td><td></td><td>829</td><td><u> </u></td><td>487</td><td></td><td>5</td><td>8</td><td><lc< td=""><td>38</td><td></td></lc<></td></lc<>	15	33		829	<u> </u>	487		5	8	<lc< td=""><td>38</td><td></td></lc<>	38	
N11.0 E12.0		24	37		725	<u> </u>	476						<u> </u>
N11.0 E13.0		24	<u></u>	<lc< td=""><td>285</td><td><u> </u></td><td>428</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	285	<u> </u>	428						<u> </u>
N11.0 E14.0		24		<lc< td=""><td>311</td><td>÷</td><td>431</td><td><u> </u></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	311	÷	431	<u> </u>					<u> </u>
N11.0 E15.0		24			596		463	· · · · · · · · · · · · · · · · · · ·		i		<u></u>	<u> </u>
N11.0 E16.0		33			415	<u> </u>	443				t		1
N11.0 E17.0		42			751	<u></u>	479						<u> </u>
N11.0 E18.0	ļ	52			725		476	<u> </u>				·····	
N11.0 E19.0	<lc< td=""><td></td><td></td><td></td><td>1062</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-25</td><td><u> </u></td></lc<></td></lc<></td></lc<>				1062			<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-25</td><td><u> </u></td></lc<></td></lc<>	-1		<lc< td=""><td>-25</td><td><u> </u></td></lc<>	-25	<u> </u>
N11.0 E19.0	H	-4	1	<lc< td=""><td>-52</td><td></td><td>387</td><td></td><td>- 1</td><td> ' </td><td></td><td>-25</td><td><u> </u></td></lc<>	-52		387		- 1	'		-25	<u> </u>
N11.0 E2.0	<lc< td=""><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td></td><td><u> </u></td><td></td><td> </td><td></td><td></td><td>┝────</td></lc<>				· · · · · · · · · · · · · · · · · · ·			<u> </u>					┝────
	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>130</td><td></td><td>409</td><td><u> </u></td><td></td><td>┠</td><td> </td><td></td><td><b> </b></td></lc<></td></lc<>	-4		<lc< td=""><td>130</td><td></td><td>409</td><td><u> </u></td><td></td><td>┠</td><td> </td><td></td><td><b> </b></td></lc<>	130		409	<u> </u>		┠			<b> </b>
N11.0 E21.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>104</td><td><u> </u></td><td>406</td><td>···</td><td></td><td>┟─────┥</td><td></td><td></td><td><b> </b></td></lc<></td></lc<>	6		<lc< td=""><td>104</td><td><u> </u></td><td>406</td><td>···</td><td></td><td>┟─────┥</td><td></td><td></td><td><b> </b></td></lc<>	104	<u> </u>	406	···		┟─────┥			<b> </b>
N11.0 E22.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>78</td><td><u> </u></td><td>403</td><td></td><td></td><td>┟────┤</td><td></td><td></td><td>ļ</td></lc<></td></lc<>	-4		<lc< td=""><td>78</td><td><u> </u></td><td>403</td><td></td><td></td><td>┟────┤</td><td></td><td></td><td>ļ</td></lc<>	78	<u> </u>	403			┟────┤			ļ
N11.0 E3.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>104</td><td>÷</td><td>406</td><td></td><td></td><td>ļ</td><td>ļ</td><td>·</td><td>ļ</td></lc<></td></lc<>	6		<lc< td=""><td>104</td><td>÷</td><td>406</td><td></td><td></td><td>ļ</td><td>ļ</td><td>·</td><td>ļ</td></lc<>	104	÷	406			ļ	ļ	·	ļ
N11.0 E4.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>104</td><td>_</td><td>406</td><td>ļ</td><td></td><td>·</td><td>ļ</td><td></td><td>ļ</td></lc<></td></lc<>	-4		<lc< td=""><td>104</td><td>_</td><td>406</td><td>ļ</td><td></td><td>·</td><td>ļ</td><td></td><td>ļ</td></lc<>	104	_	406	ļ		·	ļ		ļ
N11.0 E5.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>26</td><td></td><td>397</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td></lc<></td></lc<>	-4		<lc< td=""><td>26</td><td></td><td>397</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td></lc<>	26		397				ļ		
N11.0 E6.0	<lc< td=""><td>-4</td><td></td><td>the second s</td><td>725</td><td>_</td><td>476</td><td></td><td></td><td>ļ</td><td>L</td><td></td><td>L</td></lc<>	-4		the second s	725	_	476			ļ	L		L
N11.0 E7.0	<lc< td=""><td>-13</td><td></td><td></td><td>518</td><td>÷</td><td>454</td><td></td><td></td><td>L</td><td></td><td></td><td>L</td></lc<>	-13			518	÷	454			L			L
N11.0 E8.0	<lc< td=""><td>6</td><td></td><td></td><td>492</td><td></td><td>451</td><td></td><td></td><td></td><td></td><td>·</td><td></td></lc<>	6			492		451					·	
N11.0 E9.0	<lc< td=""><td>6</td><td>27</td><td></td><td>492</td><td></td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	6	27		492		451						
N11.5 E-0.5	<lc< td=""><td>2</td><td>19</td><td><lc< td=""><td>337</td><td>[</td><td>468</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2	19	<lc< td=""><td>337</td><td>[</td><td>468</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	337	[	468						

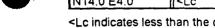
Lc indicates less than the critical level of activity which can be said to be above background.

A negative value is the calculated result of a reading which is below the instrument-specific background.

ſ			DIRECT						TR	ANSFER	ABLE		
	ALF	PHA/100		BETA	A-GAMMA/10	00 SC	CM	ALPH	_	SQ CM		GAMMA/	100 SQ CM
LOCATION/ITEM		MPL	STD		SMPL	STD		SM	PL	STD		MPL	STD
COORDINATES	] [	ОРМ	DEV		DPM	DEV	· [	DP	M	DEV		PM	DEV
N11.5 E-1.5		20	32	<lc< td=""><td>-52</td><td></td><td>425</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-52		425						
N11.5 E0.5	<lc< td=""><td>28</td><td>50</td><td><lc< td=""><td>348</td><td></td><td>466</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	28	50	<lc< td=""><td>348</td><td></td><td>466</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	348		466						
N11.5 E1.5	<lc< td=""><td>-28</td><td>24</td><td>1</td><td>883</td><td></td><td>522</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td></td></lc<></td></lc<></td></lc<>	-28	24	1	883		522	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-38</td><td></td></lc<>	-38	
N11.5 E10.5	<lc< td=""><td>-28</td><td>24</td><td><lc< td=""><td>54</td><td></td><td>433</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-28	24	<lc< td=""><td>54</td><td></td><td>433</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	54		433						
N11.5 E11.5	<lc< td=""><td>18</td><td>47</td><td></td><td>964</td><td></td><td>530</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>21</td><td></td></lc<></td></lc<></td></lc<>	18	47		964		530	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>21</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>21</td><td></td></lc<>	21	
N11.5 E12.5	<lc< td=""><td>9</td><td>43</td><td></td><td>509</td><td></td><td>484</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		509		484						
N11.5 E13.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>27</td><td>1</td><td>429</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<></td></lc<>	-9		<lc< td=""><td>27</td><td>1</td><td>429</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>	27	1	429						
N11.5 E14.5	<lc< td=""><td>-9</td><td>35</td><td><u> </u></td><td>509</td><td>1</td><td>484</td><td></td><td>·</td><td></td><td></td><td></td><td><u> </u></td></lc<>	-9	35	<u> </u>	509	1	484		·				<u> </u>
N11.5 E15.5	<lc< td=""><td>0</td><td>40</td><td><lc< td=""><td>321</td><td><u> </u></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0	40	<lc< td=""><td>321</td><td><u> </u></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	321	<u> </u>	463						
N11.5 E16.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>294</td><td>t</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>h</td></lc<></td></lc<>	-9	35	<lc< td=""><td>294</td><td>t</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>h</td></lc<>	294	t	460						h
N11.5 E17.5	<lc< td=""><td>0</td><td>40</td><td>1</td><td>910</td><td>l</td><td>525</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-29</td><td>·</td></lc<></td></lc<></td></lc<>	0	40	1	910	l	525	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-29</td><td>·</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-29</td><td>·</td></lc<>	-29	·
N11.5 E18.5	<lc< td=""><td>-18</td><td></td><td></td><td>509</td><td><u> </u></td><td>484</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-18			509	<u> </u>	484						
N11.5 E19.5	<u> </u>	NA	NA		NA	NA							
N11.5 E2.5	<lc< td=""><td>9</td><td>43</td><td><lc< td=""><td>241</td><td>†</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td>f</td></lc<></td></lc<>	9	43	<lc< td=""><td>241</td><td>†</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td>f</td></lc<>	241	†	454						f
N11.5 E20.5	, <b> </b>	NA	NA		NA	NA							·
N11.5 E21.5	<u> </u>	NA	NA		NA	NA							t
N11.5 E3.5	<lc< td=""><td>0</td><td>40</td><td><lc< td=""><td>294</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>·</td></lc<></td></lc<>	0	40	<lc< td=""><td>294</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>·</td></lc<>	294		460						·
N11.5 E4.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>375</td><td></td><td>469</td><td></td><td></td><td></td><td></td><td></td><td><u>†                                    </u></td></lc<>	-18	30		375		469						<u>†                                    </u>
N11.5 E5.5	<lc< td=""><td>18</td><td>47</td><td>t</td><td>428</td><td></td><td>475</td><td></td><td></td><td></td><td></td><td></td><td>t</td></lc<>	18	47	t	428		475						t
N11.5 E6.5	<lc< td=""><td>0</td><td></td><td></td><td>402</td><td><u> </u></td><td>472</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	0			402	<u> </u>	472						<u> </u>
N11.5 E7.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>80</td><td></td><td>436</td><td>·</td><td></td><td></td><td>· · · · ·</td><td></td><td>†</td></lc<></td></lc<>	9		<lc< td=""><td>80</td><td></td><td>436</td><td>·</td><td></td><td></td><td>· · · · ·</td><td></td><td>†</td></lc<>	80		436	·			· · · · ·		†
N11.5 E9.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td>†</td></lc<></td></lc<>	0		<lc< td=""><td>321</td><td></td><td>463</td><td></td><td></td><td></td><td></td><td></td><td>†</td></lc<>	321		463						†
N12.0 E-1.0	1-20	29		<lc< td=""><td>285</td><td><u> </u></td><td>463</td><td> </td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	285	<u> </u>	463						<u> </u>
N12.0 E-2.0	<b> </b>	39		<lc< td=""><td>259</td><td></td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>t</td></lc<>	259		460						t
N12.0 E1.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>3639</td><td></td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<></td></lc<>	-10	47		3639			<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-33</td><td></td></lc<>	-33	
N12.0 E10.0	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td>£</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0		<lc< td=""><td>397</td><td></td><td>546</td><td></td><td>£</td><td></td><td></td><td></td><td></td></lc<>	397		546		£				
N12.0 E11.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>1254</td><td><u> </u></td><td>_</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td><u> </u></td></lc<></td></lc<></td></lc<>	-10	47		1254	<u> </u>	_	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td><u> </u></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-38</td><td><u> </u></td></lc<>	-38	<u> </u>
N12.0 E12.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>581</td><td><u> </u></td><td>565</td><td></td><td></td><td></td><td><u> </u></td><td></td><td><u> </u></td></lc<>	-10	47		581	<u> </u>	565				<u> </u>		<u> </u>
N12.0 E13.0	<lc< td=""><td>-19</td><td>43</td><td></td><td>917</td><td><u>+</u></td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td><u> </u></td></lc<></td></lc<></td></lc<>	-19	43		917	<u>+</u>		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td><u> </u></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-38</td><td><u> </u></td></lc<>	-38	<u> </u>
N12.0 E14.0	<lc< td=""><td>-39</td><td>34</td><td></td><td>459</td><td></td><td>553</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-39	34		459		553						<u> </u>
N12.0 E15.0	<lc< td=""><td>-29</td><td>39</td><td></td><td>826</td><td>_</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-25</td><td><u> </u></td></lc<></td></lc<></td></lc<>	-29	39		826	_		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-25</td><td><u> </u></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-25</td><td><u> </u></td></lc<>	-25	<u> </u>
N12.0 E16.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>581</td><td><del> </del></td><td>565</td><td></td><td></td><td>· · · · ·</td><td></td><td></td><td></td></lc<>	-10	47		581	<del> </del>	565			· · · · ·			
N12.0 E17.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>1284</td><td><u> </u></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-50</td><td><u>}</u></td></lc<></td></lc<></td></lc<>	-10	47		1284	<u> </u>		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-50</td><td><u>}</u></td></lc<></td></lc<>	-1		<lc< td=""><td>-50</td><td><u>}</u></td></lc<>	-50	<u>}</u>
N12.0 E18.0	<lc< td=""><td>-39</td><td>34</td><td></td><td>673</td><td><u>}</u></td><td>575</td><td>-20</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-39	34		673	<u>}</u>	575	-20					<u> </u>
N12.0 E19.0		NA	NA 34		NA	NA							<u>↓</u>
N12.0 E2.0	<lc< td=""><td>-10</td><td>·</td><td></td><td>1712</td><td></td><td>673</td><td><lc< td=""><td>-1</td><td>0</td><td><u> </u></td><td>84</td><td></td></lc<></td></lc<>	-10	·		1712		673	<lc< td=""><td>-1</td><td>0</td><td><u> </u></td><td>84</td><td></td></lc<>	-1	0	<u> </u>	84	
		NA	NA 47		NA	INA	075						+
N12.0 E20.0 N12.0 E21.0	H	NA	NA		<u>NA</u>	NA			<u> </u>				<del> </del>
N12.0 E22.0	<lc< td=""><td>-58</td><td></td><td>∦</td><td>459</td><td></td><td>553</td><td></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<>	-58		∦	459		553			<u> </u>			<u> </u>
N12.0 E3.0	<lc< td=""><td>-38</td><td></td><td></td><td>1040</td><td></td><td>611</td><td></td><td>5</td><td>P P</td><td><lc< td=""><td>-21</td><td><u>}</u></td></lc<></td></lc<>	-38			1040		611		5	P P	<lc< td=""><td>-21</td><td><u>}</u></td></lc<>	-21	<u>}</u>
N12.0 E4.0	<lc< td=""><td>-19</td><td></td><td></td><td>703</td><td></td><td></td><td><lc< td=""><td></td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<></td></lc<>	-19			703			<lc< td=""><td></td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>			<lc< td=""><td>-21</td><td></td></lc<>	-21	
	<lc< td=""><td>-19 -29</td><td></td><td></td><td>917</td><td></td><td>599</td><td></td><td>-  </td><td><sup>0</sup></td><td></td><td></td><td>+</td></lc<>	-19 -29			917		599		-	<sup>0</sup>			+
N12.0 E5.0 N12.0 E6.0	<lc< td=""><td>-29 -29</td><td></td><td><u>a</u></td><td>1192</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>33</td><td><u> </u></td></lc<></td></lc<></td></lc<>	-29 -29		<u>a</u>	1192			<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>33</td><td><u> </u></td></lc<></td></lc<>	-1		<lc< td=""><td>33</td><td><u> </u></td></lc<>	33	<u> </u>
N12.0 E7.0	<lc< td=""><td></td><td>the second s</td><td></td><td></td><td>_</td><td>569</td><td></td><td>- 1</td><td><sup>0</sup></td><td></td><td>33</td><td><u>+</u></td></lc<>		the second s			_	569		- 1	<sup>0</sup>		33	<u>+</u>
		<u>-19</u> 19		<lc< td=""><td>612</td><td>A</td><td>_</td><td></td><td></td><td> </td><td></td><td></td><td><del> </del></td></lc<>	612	A	_						<del> </del>
N12.0 E8.0	<lc< td=""><td></td><td></td><td></td><td><u>367</u> 734</td><td></td><td>543 581</td><td></td><td></td><td></td><td><u> </u></td><td></td><td><u> </u></td></lc<>				<u>367</u> 734		543 581				<u> </u>		<u> </u>
N12.0 E9.0	<lc< td=""><td><u> </u></td><td></td><td></td><td>734 535</td><td><u></u></td><td>487</td><td>l</td><td></td><td></td><td></td><td>~<u> </u></td><td><u> </u></td></lc<>	<u> </u>			734 535	<u></u>	487	l				~ <u> </u>	<u> </u>
N12.5 E0.5							_						<u>}</u>
N12.5 E1.5	<lc< td=""><td>-9</td><td></td><td></td><td>776</td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<></td></lc<>	-9			776			<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-50</td><td></td></lc<>	-50	
N12.5 E10.5	∦	39		<lc< td=""><td>78</td><td></td><td>440</td><td></td><td></td><td></td><td><u> </u></td><td></td><td><u> </u></td></lc<>	78		440				<u> </u>		<u> </u>
N12.5 E11.5	₩	48			596		495	<u> </u>				·····	<u> </u>
N12.5 E12.5	<b> </b>	76		<lc< td=""><td>52</td><td>_</td><td>437</td><td><b> </b></td><td></td><td></td><td>ļ</td><td></td><td>}</td></lc<>	52	_	437	<b> </b>			ļ		}
N12.5 E13.5	╟───	29		<lc< td=""><td>181</td><td></td><td>451</td><td></td><td></td><td> </td><td><b> </b></td><td></td><td><u> </u></td></lc<>	181		451				<b> </b>		<u> </u>
	╟───										<u> </u>		·
N12.5 E14.5 N12.5 E15.5		48 20		<lc <lc< td=""><td>0 311</td><td></td><td>431 465</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></lc 	0 311		431 465						

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

ſ			DIRECT		······			TR	ANSFER	ABLE		
1	ALPH	IA/100	SQCM	BET	A-GAMMA/10	0 SQ CM	ALPH/	V100	SQCM	BETA-	GAMMA/	00 SQ CM
LOCATION/ITEM	SM	IPL	STD		SMPL	STD	SMF	2	STD	SI	MPL	STD
COORDINATES	DF	PM	DEV	1	DPM	DEV	DP	м	DEV	D	РМ	DEV
N12.5 E16.5	[	29	37		570	492						
N12.5 E17.5	<lc< td=""><td>2</td><td>19</td><td><u> </u></td><td>725</td><td>508</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-17</td><td>7</td></lc<></td></lc<></td></lc<>	2	19	<u> </u>	725	508	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-17</td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>-17</td><td>7</td></lc<>	-17	7
N12.5 E18.5	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-26</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-26</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-26	428						
N12.5 E19.5	<lc< td=""><td>-7</td><td></td><td><lc< td=""><td>52</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-7		<lc< td=""><td>52</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	52	437						
N12.5 E2.5	<lc< td=""><td>-7</td><td></td><td><lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-7		<lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	363	471						
N12.5 E20.5	<u>                                      </u>	20	the second s	<lc< td=""><td>285</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	285	463						
N12.5 E21.5	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>207</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>207</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	207	454						
N12.5 E3.5	<u> </u>	29	37	<u> </u>	389	474			······			
N12.5 E4.5	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>285</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>285</td><td>463</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	285	463						
N12.5 E5.5	<u> </u>	39	41	<u> </u>	570	492						
N12.5 E6.5		29		<lc< td=""><td>26</td><td>434</td><td></td><td></td><td></td><td></td><td></td><td>[</td></lc<>	26	434						[
N12.5 E7.5	<lc< td=""><td>11</td><td>27</td><td><lc< td=""><td>104</td><td>443</td><td></td><td></td><td></td><td></td><td></td><td>[</td></lc<></td></lc<>	11	27	<lc< td=""><td>104</td><td>443</td><td></td><td></td><td></td><td></td><td></td><td>[</td></lc<>	104	443						[
N12.5 E8.5		20	32	<lc< td=""><td>-52</td><td>425</td><td></td><td></td><td>······································</td><td></td><td></td><td>[</td></lc<>	-52	425			······································			[
N12.5 E9.5	<u> </u>	20	32	<lc< td=""><td>155</td><td>449</td><td></td><td></td><td></td><td></td><td></td><td>[</td></lc<>	155	449						[
N13.0 E1.0	<lc< td=""><td>-39</td><td></td><td><lc< td=""><td>397</td><td>546</td><td></td><td></td><td></td><td></td><td></td><td>(</td></lc<></td></lc<>	-39		<lc< td=""><td>397</td><td>546</td><td></td><td></td><td></td><td></td><td></td><td>(</td></lc<>	397	546						(
N13.0 E10.0	<lc< td=""><td>-19</td><td>43</td><td><u> </u></td><td>1559</td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td>7</td></lc<></td></lc<></td></lc<>	-19	43	<u> </u>	1559		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>-33</td><td>7</td></lc<>	-33	7
N13.0 E11.0	<lc< td=""><td>0</td><td>+</td><td></td><td>1223</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<></td></lc<>	0	+		1223		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>4</td><td></td></lc<>	4	
N13.0 E12.0	<lc< td=""><td>-39</td><td>34</td><td></td><td>459</td><td>553</td><td><u> </u></td><td></td><td> i</td><td><u> </u></td><td></td><td>í</td></lc<>	-39	34		459	553	<u> </u>		i	<u> </u>		í
N13.0 E13.0	<lc< td=""><td>29</td><td>60</td><td></td><td>1009</td><td>608</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-42</td><td>7</td></lc<></td></lc<></td></lc<>	29	60		1009	608	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-42</td><td>7</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-42</td><td>7</td></lc<>	-42	7
N13.0 E14.0	<lc< td=""><td>10</td><td>54</td><td></td><td>826</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-4</td><td></td></lc<></td></lc<></td></lc<>	10	54		826		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-4</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-4</td><td></td></lc<>	-4	
N13.0 E15.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>948</td><td>602</td><td></td><td>2</td><td></td><td><lc< td=""><td>-59</td><td></td></lc<></td></lc<>	-10	47		948	602		2		<lc< td=""><td>-59</td><td></td></lc<>	-59	
N13.0 E16.0	<lc< td=""><td>- 10</td><td>51</td><td></td><td>581</td><td>565</td><td></td><td>2</td><td></td><td></td><td>-00</td><td><u> </u></td></lc<>	- 10	51		581	565		2			-00	<u> </u>
N13.0 E17.0	<lc< td=""><td>-19</td><td></td><td></td><td>581</td><td>565</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-19			581	565						<u> </u>
N13.0 E18.0	<lc< td=""><td>-29</td><td>39</td><td></td><td>673</td><td>575</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-29	39		673	575						<u> </u>
N13.0 E19.0	<lc< td=""><td>-29</td><td><u> </u></td><td><lc< td=""><td>153</td><td>519</td><td>l</td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-29	<u> </u>	<lc< td=""><td>153</td><td>519</td><td>l</td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	153	519	l				<u> </u>	
N13.0 E2.0	<lc< td=""><td>-40</td><td>43</td><td></td><td>642</td><td>572</td><td>ľ</td><td></td><td></td><td></td><td></td><td><u>├</u></td></lc<>	-40	43		642	572	ľ					<u>├</u>
N13.0 E20.0	<lc< td=""><td>-19</td><td>43</td><td></td><td>734</td><td>581</td><td></td><td>· · · · · ·</td><td></td><td></td><td></td><td></td></lc<>	-19	43		734	581		· · · · · ·				
N13.0 E21.0	<lc< td=""><td>-19</td><td></td><td> </td><td></td><td>562</td><td><u> </u></td><td>·</td><td></td><td></td><td></td><td></td></lc<>	-19				562	<u> </u>	·				
N13.0 E22.0	<lc< td=""><td>-19</td><td></td><td></td><td>734</td><td>581</td><td><b> </b></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19			734	581	<b> </b>					
N13.0 E3.0	<lc< td=""><td>-39</td><td></td><td><lc< td=""><td>-428</td><td>448</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<></td></lc<>	-39		<lc< td=""><td>-428</td><td>448</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>	-428	448						
N13.0 E4.0	<lc< td=""><td>-39</td><td><u>+</u></td><td><lc< td=""><td>-420</td><td>509</td><td>l</td><td></td><td></td><td>l</td><td></td><td><u> </u></td></lc<></td></lc<>	-39	<u>+</u>	<lc< td=""><td>-420</td><td>509</td><td>l</td><td></td><td></td><td>l</td><td></td><td><u> </u></td></lc<>	-420	509	l			l		<u> </u>
		10		<lc< td=""><td>336</td><td></td><td></td><td></td><td></td><td> </td><td><u> </u></td><td></td></lc<>	336						<u> </u>	
N13.0 E5.0	<lc< td=""><td></td><td></td><td>·</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>			·								<u> </u>
N13.0 E6.0	<lc< td=""><td>-19</td><td></td><td><lc< td=""><td>336</td><td>•</td><td>l</td><td><u>.                                    </u></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19		<lc< td=""><td>336</td><td>•</td><td>l</td><td><u>.                                    </u></td><td></td><td></td><td></td><td></td></lc<>	336	•	l	<u>.                                    </u>				
N13.0 E7.0	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>397</td><td>546</td><td></td><td></td><td></td><td> </td><td></td><td><u> </u></td></lc<></td></lc<>	0		<lc< td=""><td>397</td><td>546</td><td></td><td></td><td></td><td> </td><td></td><td><u> </u></td></lc<>	397	546						<u> </u>
N13.0 E8.0	<lc< td=""><td>-39</td><td></td><td><u> </u></td><td>459</td><td>553</td><td><u> </u></td><td>·</td><td></td><td></td><td></td><td> </td></lc<>	-39		<u> </u>	459	553	<u> </u>	·				
N13.0 E9.0	<lc< td=""><td>-10</td><td></td><td></td><td>489</td><td></td><td></td><td>·</td><td></td><td></td><td></td><td><u> </u></td></lc<>	-10			489			·				<u> </u>
N14.0 E0.0	∦	24		<lc< td=""><td>233</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	233							<u> </u>
N14.0 E1:0	l	42			363					<b> </b>		ļ
N14.0 E10.0	[	24			700							
N14.0 E11.0	<lc< td=""><td>6</td><td></td><td></td><td>570</td><td></td><td></td><td></td><td></td><td></td><td></td><td>·</td></lc<>	6			570							·
N14.0 E12.0	<lc< td=""><td>15</td><td></td><td></td><td>466</td><td></td><td>·····</td><td>······</td><td></td><td></td><td></td><td>ļ</td></lc<>	15			466		·····	······				ļ
N14.0 E13.0	₩ <u> </u>	24			337	the second s				l		ļ
N14.0 E14.0	<lc< td=""><td>15</td><td></td><td></td><td>959</td><td></td><td></td><td>5</td><td>8</td><td><lc< td=""><td>-13</td><td>7</td></lc<></td></lc<>	15			959			5	8	<lc< td=""><td>-13</td><td>7</td></lc<>	-13	7
N14.0 E15.0	<lc< td=""><td>15</td><td></td><td><lc< td=""><td>259</td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td></lc<></td></lc<>	15		<lc< td=""><td>259</td><td></td><td></td><td></td><td></td><td></td><td></td><td>ļ</td></lc<>	259							ļ
N14.0 E16.0	<lc< td=""><td>-13</td><td></td><td></td><td>466</td><td></td><td><u> </u></td><td></td><td> </td><td><u>`</u></td><td></td><td> </td></lc<>	-13			466		<u> </u>			<u>`</u>		
N14.0 E17.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>285</td><td></td><td>4</td><td></td><td></td><td></td><td></td><td>ļ</td></lc<></td></lc<>	6		<lc< td=""><td>285</td><td></td><td>4</td><td></td><td></td><td></td><td></td><td>ļ</td></lc<>	285		4					ļ
N14.0 E18.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>207</td><td></td><td></td><td></td><td></td><td></td><td></td><td>L</td></lc<></td></lc<>	6		<lc< td=""><td>207</td><td></td><td></td><td></td><td></td><td></td><td></td><td>L</td></lc<>	207							L
N14.0 E19.0	<lc< td=""><td>15</td><td></td><td><lc< td=""><td>0</td><td><u></u></td><td></td><td></td><td>·</td><td></td><td></td><td></td></lc<></td></lc<>	15		<lc< td=""><td>0</td><td><u></u></td><td></td><td></td><td>·</td><td></td><td></td><td></td></lc<>	0	<u></u>			·			
N14.0 E2.0	<lc< td=""><td>6</td><td></td><td></td><td>622</td><td></td><td></td><td></td><td></td><td>·</td><td></td><td></td></lc<>	6			622					·		
N14.0 E20.0	<lc< td=""><td>6</td><td></td><td><lc< td=""><td>259</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6		<lc< td=""><td>259</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	259							
N14.0 E21.0	<lc< td=""><td>-13</td><td></td><td><lc< td=""><td>207</td><td>419</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-13		<lc< td=""><td>207</td><td>419</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	207	419						
N14.0 E22.0		24		<lc< td=""><td>311</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	311							
N14.0 E3.0	<lc< td=""><td>15</td><td>33</td><td><lc< td=""><td>259</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	15	33	<lc< td=""><td>259</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	259							
N14.0 E4.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td>1</td><td></td><td> </td></lc<>	-4	20		518	454				1		



;

ŧ

.)

Ν

ł

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

71

73

70

73

75

71

80

74

76

77

75

73

73

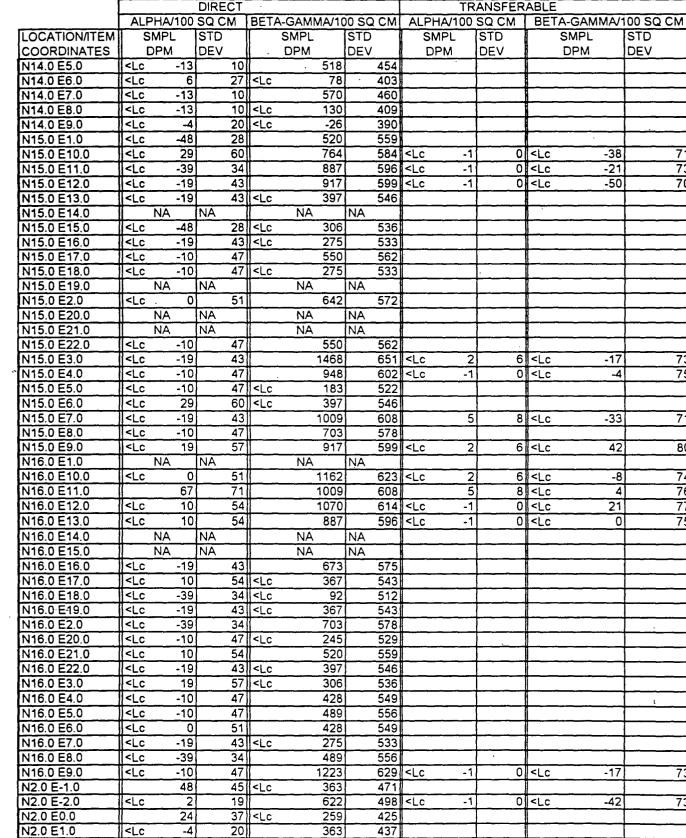


}

j

}

)



<Lc indicates less than the critical level of activity which can be said to be above background.

27

A negative value is the calculated result of a reading which is below the instrument-specific background.

N2.0 E10.0

<Lc

6

389

440

]			DIRECT				TR	ANSFER	ABLE		
	ALF	PHA/100	SQCM	BETA-GAMMA/1	00 SQ CM	ALP	HA/100	SQ CM	BETA	-GAMMA/	100 SQ CM
LOCATION/ITEM	S	MPL	STD	SMPL	STD	S	MPL	STD	s	MPL	STD
COORDINATES	i c	DPM	DEV	DPM	DEV	l C	DPM	DEV	L C	DPM	DEV
N2.0 E11.0		52	49	1218	525	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td>74</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-38</td><td>74</td></lc<>	-38	74
N2.0 E12.0		24	37	622	465	1			,		
N2.0 E13.0	<lc< td=""><td>6</td><td>27</td><td>1347</td><td>537</td><td><lc< td=""><td>-1</td><td>Ō</td><td><lc< td=""><td>-13</td><td>76</td></lc<></td></lc<></td></lc<>	6	27	1347	537	<lc< td=""><td>-1</td><td>Ō</td><td><lc< td=""><td>-13</td><td>76</td></lc<></td></lc<>	-1	Ō	<lc< td=""><td>-13</td><td>76</td></lc<>	-13	76
N2.0 E14.0	<lc< td=""><td>6</td><td>27</td><td>596</td><td>6 463</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	6	27	596	6 463	1					
N2.0 E15.0		61	52	389	440	1					
N2.0 E16.0		NA	NA	NA	NA						· · · · ·
N2.0 E17.0	1	NA	NA	NA	NA	1					1
N2.0 E18.0		24	37	1114	515	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td>74</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-38</td><td>74</td></lc<>	-38	74
N2.0 E19.0	<lc< td=""><td>-4</td><td>20</td><td>725</td><td>5 476</td><td>1</td><td></td><td></td><td></td><td></td><td>1</td></lc<>	-4	20	725	5 476	1					1
N2.0 E2.0		24	37	<lc 18<="" td=""><td>416</td><td>1</td><td></td><td></td><td></td><td>•</td><td>1</td></lc>	416	1				•	1
N2.0 E20.0	<lc< td=""><td>-4</td><td>20</td><td>466</td><td>6 449</td><td>1</td><td></td><td></td><td></td><td></td><td>1</td></lc<>	-4	20	466	6 449	1					1
N2.0 E21.0	<lc< td=""><td>-13</td><td>10</td><td>570</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-13	10	570							
N2.0 E22.0	<lc< td=""><td>-4</td><td>20</td><td><lc 78<="" td=""><td></td><td>1</td><td></td><td> </td><td></td><td></td><td></td></lc></td></lc<>	-4	20	<lc 78<="" td=""><td></td><td>1</td><td></td><td> </td><td></td><td></td><td></td></lc>		1					
N2.0 E3.0	<lc< td=""><td>-4</td><td>20</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td></lc<>	-4	20								1
N2.0 E4.0	<lc< td=""><td>15</td><td>33</td><td>674</td><td></td><td></td><td></td><td>[</td><td></td><td></td><td>1</td></lc<>	15	33	674				[			1
N2.0 E5.0	<lc< td=""><td>-4</td><td>20</td><td>415</td><td></td><td></td><td></td><td>[</td><td></td><td></td><td>1</td></lc<>	-4	20	415				[			1
N2.0 E6.0	- <u></u> -	33	41	389	the second s	14		<u> </u>			1
N2.0 E7.0		24	37	466							
N2.0 E8.0	<lc< td=""><td>-13</td><td>10</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td></lc<>	-13	10								1
N2.0 E9.0	<lc< td=""><td>-13</td><td></td><td><lc 26<="" td=""><td>the second s</td><td>A</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc></td></lc<>	-13		<lc 26<="" td=""><td>the second s</td><td>A</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc>	the second s	A					<u> </u>
N2.5 E-0.5	<lc< td=""><td>-7</td><td>7</td><td>674</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-42</td><td>73</td></lc<></td></lc<></td></lc<>	-7	7	674		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-42</td><td>73</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-42</td><td>73</td></lc<>	-42	73
N2.5 E-1.5	<lc< td=""><td>11</td><td>27</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td></lc<>	11	27								1
N2.5 E0.5	<lc< td=""><td>-18</td><td>30</td><td>750</td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-17</td><td>73</td></lc<></td></lc<></td></lc<>	-18	30	750		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-17</td><td>73</td></lc<></td></lc<>	2	6	<lc< td=""><td>-17</td><td>73</td></lc<>	-17	73
N2.5 E1.5	<lc< td=""><td>9</td><td>43</td><td>482</td><td></td><td>*</td><td></td><td><u> </u></td><td></td><td>····_·</td><td><u> </u></td></lc<>	9	43	482		*		<u> </u>		····_·	<u> </u>
N2.5 E10.5	<lc< td=""><td>-18</td><td>30</td><td>1419</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-63</td><td>68</td></lc<></td></lc<></td></lc<>	-18	30	1419		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-63</td><td>68</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-63</td><td>68</td></lc<>	-63	68
N2.5 E11.5	<lc< td=""><td>-9</td><td></td><td>883</td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<></td></lc<>	-9		883		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<>	2		<lc< td=""><td>4</td><td></td></lc<>	4	
N2.5 E12.5	<lc< td=""><td>-9</td><td></td><td>883</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<></td></lc<>	-9		883		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>4</td><td></td></lc<>	4	
N2.5 E13.5	<lc< td=""><td>-9</td><td></td><td>310</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>17</td><td></td></lc<></td></lc<></td></lc<>	-9		310		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>17</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>17</td><td></td></lc<>	17	
N2.5 E14.5	<lc< td=""><td>-9</td><td></td><td>275</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<></td></lc<>	-9		275		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-8</td><td></td></lc<>	-8	
N2.5 E15.5	<lc< td=""><td>28</td><td></td><td>1419</td><td></td><td><lc< td=""><td>-1</td><td><u></u></td><td><lc< td=""><td>-13</td><td></td></lc<></td></lc<></td></lc<>	28		1419		<lc< td=""><td>-1</td><td><u></u></td><td><lc< td=""><td>-13</td><td></td></lc<></td></lc<>	-1	<u></u>	<lc< td=""><td>-13</td><td></td></lc<>	-13	
N2.5 E16.5	<u> </u>	NA	NA	NA	INA NA						<u> </u>
N2.5 E17.5		NA	NA	NA	NA	<u> </u>		<u> </u>			
N2.5 E18.5	<lc< td=""><td>-9</td><td>35</td><td></td><td></td><td><lc< td=""><td>-1</td><td><u>-</u></td><td><lc< td=""><td>-42</td><td>71</td></lc<></td></lc<></td></lc<>	-9	35			<lc< td=""><td>-1</td><td><u>-</u></td><td><lc< td=""><td>-42</td><td>71</td></lc<></td></lc<>	-1	<u>-</u>	<lc< td=""><td>-42</td><td>71</td></lc<>	-42	71
N2.5 E19.5	<lc< td=""><td>9</td><td>the second s</td><td><lc 32<="" td=""><td></td><td></td><td></td><td><del> </del>-</td><td>-20</td><td></td><td><u> </u></td></lc></td></lc<>	9	the second s	<lc 32<="" td=""><td></td><td></td><td></td><td><del> </del>-</td><td>-20</td><td></td><td><u> </u></td></lc>				<del> </del> -	-20		<u> </u>
N2.5 E2.5	<lc< td=""><td>18</td><td></td><td></td><td>the second s</td><td></td><td></td><td><u> </u></td><td>}</td><td></td><td>+</td></lc<>	18			the second s			<u> </u>	}		+
N2.5 E20.5	<lc< td=""><td>-9</td><td></td><td><lc 32<="" td=""><td></td><td></td><td></td><td><u> </u></td><td>Į</td><td></td><td>+</td></lc></td></lc<>	-9		<lc 32<="" td=""><td></td><td></td><td></td><td><u> </u></td><td>Į</td><td></td><td>+</td></lc>				<u> </u>	Į		+
	<lc< td=""><td>-9</td><td>·</td><td>&lt;<u>Lc 32</u></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<>	-9	·	< <u>Lc 32</u>				<u> </u>			<u> </u>
N2.5 E3.5	<lc< td=""><td>0</td><td></td><td></td><td></td><td><lc< td=""><td>2</td><td>- F</td><td><lc< td=""><td>-33</td><td>71</td></lc<></td></lc<></td></lc<>	0				<lc< td=""><td>2</td><td>- F</td><td><lc< td=""><td>-33</td><td>71</td></lc<></td></lc<>	2	- F	<lc< td=""><td>-33</td><td>71</td></lc<>	-33	71
N2.5 E4.5	<lc< td=""><td>-18</td><td></td><td></td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<></td></lc<>	-18				<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-33</td><td></td></lc<>	-33	
N2.5 E5.5	<lc< td=""><td>-18</td><td></td><td></td><td></td><td></td><td>2</td><td><u>├</u>°</td><td></td><td>-55</td><td>·/-</td></lc<>	-18					2	<u>├</u> °		-55	·/-
N2.5 E6.5	<lc< td=""><td>-9</td><td></td><td></td><td></td><td><u> </u></td><td></td><td><u> </u></td><td></td><td></td><td>+</td></lc<>	-9				<u> </u>		<u> </u>			+
N2.5 E7.5	<lc< td=""><td>-18</td><td></td><td></td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-29</td><td>72</td></lc<></td></lc<></td></lc<>	-18				<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-29</td><td>72</td></lc<></td></lc<>	-1		<lc< td=""><td>-29</td><td>72</td></lc<>	-29	72
N2.5 E8.5	<lc< td=""><td>-18</td><td></td><td></td><td></td><td></td><td>- 1</td><td></td><td></td><td>-29</td><td>1</td></lc<>	-18					- 1			-29	1
	<lc< td=""><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<>					<u> </u>		<u> </u>			<u> </u>
N2.5 E9.5	_	-28						<b> </b>			<u> </u>
N3.0 E-1.0	<lc< td=""><td>11</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><del> </del></td></lc<>	11									<del> </del>
N3.0 E-2.0		20 6						<u> </u>	<u> </u>		<del> </del>
N3.0 E0.0	<lc< td=""><td></td><td></td><td><lc 104<="" td=""><td></td><td></td><td></td><td><u> </u></td><td></td><td><u></u></td><td><u>+</u>_</td></lc></td></lc<>			<lc 104<="" td=""><td></td><td></td><td></td><td><u> </u></td><td></td><td><u></u></td><td><u>+</u>_</td></lc>				<u> </u>		<u></u>	<u>+</u> _
N3.0 E1.0		24		44(				<u> </u>			<u> </u>
N3.0 E10.0	<lc< td=""><td>-4</td><td></td><td></td><td></td><td><lc< td=""><td><u></u></td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<></td></lc<>	-4				<lc< td=""><td><u></u></td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	<u></u>		<lc< td=""><td>-21</td><td></td></lc<>	-21	
N3.0 E11.0	. 	24				<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-8</td><td></td></lc<>	-8	
N3.0 E12.0	<lc< td=""><td>15</td><td></td><td></td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-13</td><td>76</td></lc<></td></lc<></td></lc<>	15				<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-13</td><td>76</td></lc<></td></lc<>	2	6	<lc< td=""><td>-13</td><td>76</td></lc<>	-13	76
N3.0 E13.0	<lc< td=""><td>-4</td><td></td><td>10804</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<>	-4		10804				<u> </u>			<u> </u>
N3.0 E14.0		33		1399		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-25</td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-25</td><td></td></lc<>	-25	
N3.0 E15.0	1	24	37	4042	2 746	<lc< td=""><td>-1</td><td>10</td><td><lc< td=""><td>-8</td><td>77</td></lc<></td></lc<>	-1	10	<lc< td=""><td>-8</td><td>77</td></lc<>	-8	77

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

-1

ļ		A /1 0 0	DIRECT		20.50 CM			ANSFER		CANANAA	
OO TIONITE !!				BETA-GAMMA/1				SQ CM		the second se	100 SQ CI
	SMF		STD DEV	SMPL DPM	STD DEV	SMF DPI	-	STD		MPL PM	STD DEV
OORDINATES	DP							DEV			
13.0 E16.0	L	24	37	6063	871	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-54</td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-54</td><td></td></lc<>	-54	
13.0 E17.0	<lc< td=""><td>6</td><td>27</td><td>4405</td><td></td><td></td><td>88</td><td>10</td><td><lc< td=""><td>0</td><td></td></lc<></td></lc<>	6	27	4405			88	10	<lc< td=""><td>0</td><td></td></lc<>	0	
13.0 E18.0	<lc< td=""><td>15</td><td>33</td><td>648</td><td></td><td></td><td></td><td></td><td></td><td></td><td>Ļ</td></lc<>	15	33	648							Ļ
13.0 E19.0	<lc< td=""><td>-4</td><td>20</td><td>725</td><td>476</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	20	725	476						
13.0 E2.0	<lc< td=""><td>15</td><td>33</td><td>622</td><td>465</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33	622	465						
13.0 E20.0	<lc< td=""><td>6</td><td>27</td><td><lc 155<="" td=""><td>413</td><td></td><td></td><td></td><td></td><td></td><td>· .</td></lc></td></lc<>	6	27	<lc 155<="" td=""><td>413</td><td></td><td></td><td></td><td></td><td></td><td>· .</td></lc>	413						· .
13.0 E21.0	<lc< td=""><td>6</td><td>27</td><td><lc 207<="" td=""><td>419</td><td></td><td></td><td></td><td></td><td></td><td></td></lc></td></lc<>	6	27	<lc 207<="" td=""><td>419</td><td></td><td></td><td></td><td></td><td></td><td></td></lc>	419						
3.0 E22.0		125	71	337	434	1					1
13.0 E3.0		70	55	803							t
3.0 E4.0	<lc< td=""><td>15</td><td>33</td><td>622</td><td>465</td><td></td><td>5</td><td>8</td><td><lc< td=""><td>-4</td><td>1</td></lc<></td></lc<>	15	33	622	465		5	8	<lc< td=""><td>-4</td><td>1</td></lc<>	-4	1
13.0 E5.0	<lc< td=""><td>-4</td><td>20</td><td>674</td><td>471</td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	20	674	471	<u> </u>					
			33	725		¥					┼────
13.0 E6.0	<lc< td=""><td>15</td><td></td><td></td><td></td><td><b></b></td><td></td><td></td><td><b> </b></td><td></td><td></td></lc<>	15				<b></b>			<b> </b>		
13.0 E7.0		33	41	751	479						<u> </u>
13.0 E8.0	<lc< td=""><td>6</td><td>27</td><td>466</td><td></td><td></td><td></td><td></td><td> </td><td></td><td>┨─────</td></lc<>	6	27	466							┨─────
13.0 E9.0	<lc< td=""><td>15</td><td>33</td><td>518</td><td></td><td>N</td><td></td><td> </td><td><b> </b></td><td></td><td><u> </u></td></lc<>	15	33	518		N			<b> </b>		<u> </u>
13.5 E-0.5	<lc< td=""><td>11</td><td>27</td><td></td><td>406</td><td></td><td></td><td></td><td>l</td><td>+</td><td>↓</td></lc<>	11	27		406				l	+	↓
13.5 E-1.5		20	32					[	I	· ··=	L
13.5 E0.5	<lc< td=""><td>-9</td><td>35</td><td>375</td><td></td><td></td><td></td><td></td><td> </td><td></td><td></td></lc<>	-9	35	375							
13.5 E1.5	<lc< td=""><td>-9</td><td>35</td><td>375</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9	35	375							
13.5 E10.5	<lc< td=""><td>0</td><td>40</td><td>1526</td><td>582</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-25</td><td></td></lc<></td></lc<></td></lc<>	0	40	1526	582	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-25</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-25</td><td></td></lc<>	-25	
13.5 E11.5	<lc< td=""><td>-9</td><td>35</td><td><lc 348<="" td=""><td>466</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc></td></lc<>	-9	35	<lc 348<="" td=""><td>466</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc>	466	1					
13.5 E12.5	<lc< td=""><td>9</td><td>43</td><td>375</td><td>469</td><td>l</td><td></td><td></td><td></td><td></td><td>1</td></lc<>	9	43	375	469	l					1
13.5 E13.5	<lc< td=""><td>9</td><td>43</td><td>2329</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>8</td><td><u> </u></td></lc<></td></lc<></td></lc<>	9	43	2329		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>8</td><td><u> </u></td></lc<></td></lc<>	-1	0	<lc< td=""><td>8</td><td><u> </u></td></lc<>	8	<u> </u>
13.5 E14.5	<lc< td=""><td>28</td><td>50</td><td>7362</td><td></td><td><lc< td=""><td></td><td></td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<></td></lc<>	28	50	7362		<lc< td=""><td></td><td></td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<>			<lc< td=""><td>-50</td><td></td></lc<>	-50	
13.5 E15.5	<lc< td=""><td>-28</td><td>24</td><td>535</td><td></td><td></td><td></td><td><del>[</del></td><td></td><td></td><td></td></lc<>	-28	24	535				<del>[</del>			
13.5 E17.5	<lc< td=""><td>18</td><td>47</td><td>1258</td><td></td><td>1</td><td></td><td></td><td>H</td><td></td><td>┼────</td></lc<>	18	47	1258		1			H		┼────
the second s								<u> </u>			·}
13.5 E18.5	<lc< td=""><td>-28</td><td></td><td><pre><lc 268<="" pre=""></lc></pre></td><td></td><td></td><td></td><td></td><td>·</td><td></td><td></td></lc<>	-28		<pre><lc 268<="" pre=""></lc></pre>					·		
13.5 E19.5	<lc< td=""><td>-9</td><td></td><td><lc 294<="" td=""><td></td><td>*</td><td></td><td></td><td> </td><td></td><td>·  </td></lc></td></lc<>	-9		<lc 294<="" td=""><td></td><td>*</td><td></td><td></td><td> </td><td></td><td>·  </td></lc>		*					·
13.5 E2.5		64	62	696					l		
13.5 E20.5	<lc< td=""><td>-28</td><td>24</td><td>509</td><td></td><td>#</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-28	24	509		#					<u> </u>
3.5 E21.5	<lc< td=""><td>00</td><td></td><td>482</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td><td></td></lc<>	00		482				ļ			
13.5 E3.5	<lc< td=""><td>9</td><td>43</td><td>1071</td><td>540</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<></td></lc<>	9	43	1071	540	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-21</td><td></td></lc<>	-21	
13.5 E4.5	<lc< td=""><td>0</td><td>40</td><td>1660</td><td>594</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	0	40	1660	594						
13.5 E5.5	<lc< td=""><td>18</td><td>47</td><td>375</td><td>469</td><td></td><td>8</td><td>10</td><td><lc< td=""><td>-42</td><td></td></lc<></td></lc<>	18	47	375	469		8	10	<lc< td=""><td>-42</td><td></td></lc<>	-42	
13.5 E6.5	<lc< td=""><td>-18</td><td></td><td>616</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>1</td></lc<>	-18		616				1			1
13.5 E7.5	<lc< td=""><td>-9</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td>í</td><td></td><td>1</td></lc<>	-9						<u> </u>	í		1
13.5 E8.5	<u> </u>	74									+
13.5 E9.5	<del> </del>	74				<lc< td=""><td>2</td><td> F</td><td><lc< td=""><td>46</td><td>+</td></lc<></td></lc<>	2	F	<lc< td=""><td>46</td><td>+</td></lc<>	46	+
the second s	<lc< td=""><td></td><td></td><td><pre>937 <lc 207<="" pre=""></lc></pre></td><td></td><td><b>n</b></td><td>2</td><td>+°</td><td></td><td>40</td><td>+</td></lc<>			<pre>937 <lc 207<="" pre=""></lc></pre>		<b>n</b>	2	+°		40	+
4.0 E-1.0		-7			the second s			{	<u> </u>		
14.0 E-2.0	<lc< td=""><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td>l</td><td></td><td></td></lc<>				<u> </u>				l		
14.0 E0.0	<lc< td=""><td>-4</td><td></td><td></td><td></td><td></td><td></td><td>ļ</td><td><b> </b></td><td></td><td>·</td></lc<>	-4						ļ	<b> </b>		·
4.0 E1.0		42						<b> </b>	ļ		ļ
14.0 E10.0		24				<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-21</td><td></td></lc<>	-21	
4.0 E11.0	<lc< td=""><td>15</td><td></td><td></td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<></td></lc<>	15				<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-33</td><td></td></lc<>	-33	
4.0 E12.0	<lc< td=""><td>15</td><td></td><td></td><td>468</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15			468						
4.0 E13.0		24	37	. 959	500	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>33</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>33</td><td></td></lc<>	33	
4.0 E14.0	<lc< td=""><td>6</td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td></td><td></td><td>T</td></lc<>	6				<u> </u>					T
4.0 E15.0	<lc< td=""><td>15</td><td></td><td></td><td>and the second se</td><td><lc< td=""><td>1</td><td>0</td><td><lc< td=""><td>-33</td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<></td></lc<></td></lc<>	15			and the second se	<lc< td=""><td>1</td><td>0</td><td><lc< td=""><td>-33</td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<></td></lc<>	1	0	<lc< td=""><td>-33</td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<>	-33	· · · · · · · · · · · · · · · · · · ·
4.0 E16.0	<lc< td=""><td></td><td></td><td>777</td><td></td><td><lc< td=""><td>-1</td><td>the second s</td><td><lc< td=""><td>-38</td><td></td></lc<></td></lc<></td></lc<>			777		<lc< td=""><td>-1</td><td>the second s</td><td><lc< td=""><td>-38</td><td></td></lc<></td></lc<>	-1	the second s	<lc< td=""><td>-38</td><td></td></lc<>	-38	
4.0 E17.0	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td><td></td><td>+</td></lc<>							<u> </u>			+
the second se		-			the second s	· · · · · · · · · · · · · · · · · · ·		<u> </u>	f		<del> </del>
14.0 E18.0	<lc< td=""><td>6</td><td></td><td></td><td></td><td>*</td><td></td><td></td><td></td><td></td><td>·</td></lc<>	6				*					·
4.0 E19.0	<lc< td=""><td>-4</td><td></td><td></td><td>the second s</td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-67</td><td></td></lc<></td></lc<></td></lc<>	-4			the second s	<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-67</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-67</td><td></td></lc<>	-67	
14.0 E2.0	<lc< td=""><td>6</td><td>27</td><td>933</td><td>I 498</td><td><lc< td=""><td>-1</td><td>I 0</td><td><lc< td=""><td>-17</td><td></td></lc<></td></lc<></td></lc<>	6	27	933	I 498	<lc< td=""><td>-1</td><td>I 0</td><td><lc< td=""><td>-17</td><td></td></lc<></td></lc<>	-1	I 0	<lc< td=""><td>-17</td><td></td></lc<>	-17	

<Lc indicates less than the critical level of activity which can be said to be above background.

A negative value is the calculated result of a reading which is below the instrument-specific background.

2

ŧ

)

3

۱

1			DIRECT					TR	ANSFER	ABLE		
	ALPHA			BETA-	GAMMA/10	DO SQ CM	ALPHA	_	SQCM		-GAMMA/	100 SQ CM
LOCATION/ITEM	SMF	2	STD .		SMPL	STD	SMF	۲	STD	S	SMPL	STD
COORDINATES	DPI	N	DEV _		DPM	DEV	DPN	N	DEV	1	DPM	DEV
N4.0 E21.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>570</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-4	20		570	460						
N4.0 E22.0	<lc< td=""><td>15</td><td>33</td><td></td><td>440</td><td>446</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33		440	446						
N4.0 E3.0		24	37		415	443						
N4.0 E4.0	<lc< td=""><td>4</td><td>20</td><td></td><td>337</td><td>434</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td>78</td></lc<></td></lc<></td></lc<>	4	20		337	434	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td>78</td></lc<></td></lc<>	-1	0	<lc< td=""><td>4</td><td>78</td></lc<>	4	78
N4.0 E5.0		42	45	<lc< td=""><td>311</td><td>431</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	311	431						
N4.0 E6.0		52	49		751	479					•	
N4.0 E7.0		24	37	<lc< td=""><td>285</td><td>428</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	285	428						
N4.0 E8.0	<lc< td=""><td>6</td><td>27</td><td></td><td>492</td><td>451</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	6	27		492	451						
N4.0 E9.0	<lc< td=""><td>15</td><td>33</td><td></td><td>363</td><td>437</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	15	33		363	437						
N4.5 E-0.5	<lc< td=""><td>-7</td><td>7</td><td>1</td><td>959</td><td>530</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-42</td><td>73</td></lc<></td></lc<></td></lc<>	-7	7	1	959	530	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-42</td><td>73</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-42</td><td>73</td></lc<>	-42	73
N4.5 E-1.5	<u> </u>	20	32		466	482						
N4.5 E0.5	<lc< td=""><td>0</td><td>40</td><td>[</td><td>535</td><td>487</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	0	40	[	535	487						
N4.5 E1.5	<lc< td=""><td>-28</td><td>24</td><td>1</td><td>402</td><td>472</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-28	24	1	402	472						
N4.5 E10.5	1	46	57		883		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>21</td><td>77</td></lc<></td></lc<>	2	6	<lc< td=""><td>21</td><td>77</td></lc<>	21	77
N4.5 E11.5	1	55	59	·	/ 1365	568	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>74</td></lc<>	-8	74
N4.5 E12.5	<b></b>	46	57	<lc< td=""><td>0</td><td>426</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	0	426						
N4.5 E13.5	<lc< td=""><td>9</td><td>43</td><td></td><td>5729</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td>76</td></lc<></td></lc<></td></lc<>	9	43		5729		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td>76</td></lc<></td></lc<>	-1	0	<lc< td=""><td>4</td><td>76</td></lc<>	4	76
N4.5 E14.5	1	55	59	1	2597	670	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>74</td></lc<>	-8	74
N4.5 E15.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>3748</td><td>753</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<></td></lc<>	-9	35		3748	753	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td>74</td></lc<></td></lc<>	2	6	<lc< td=""><td>-8</td><td>74</td></lc<>	-8	74
N4.5 E16.5	<lc< td=""><td>9</td><td>43</td><td>1</td><td>2168</td><td>636</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-4</td><td>75</td></lc<></td></lc<></td></lc<>	9	43	1	2168	636	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-4</td><td>75</td></lc<></td></lc<>	2	6	<lc< td=""><td>-4</td><td>75</td></lc<>	-4	75
N4.5 E17.5	<lc< td=""><td>28</td><td>50</td><td></td><td>1044</td><td>538</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-46</td><td>70</td></lc<></td></lc<></td></lc<>	28	50		1044	538	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-46</td><td>70</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-46</td><td>70</td></lc<>	-46	70
N4.5 E18.5	<lc< td=""><td>28</td><td>50</td><td>1</td><td>455</td><td>478</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	28	50	1	455	478	1					
N4.5 E19.5	<lc< td=""><td>9</td><td>43</td><td><lc< td=""><td>348</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9	43	<lc< td=""><td>348</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	348							
N4.5 E2.5	<lc< td=""><td>28</td><td></td><td><lc< td=""><td>214</td><td></td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	28		<lc< td=""><td>214</td><td></td><td><u> </u></td><td></td><td></td><td></td><td></td><td></td></lc<>	214		<u> </u>					
N4.5 E20.5	<lc< td=""><td>9</td><td>43</td><td><u> </u></td><td>402</td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td></td><td></td><td>[</td><td></td><td>1</td></lc<>	9	43	<u> </u>	402	· · · · · · · · · · · · · · · · · · ·				[		1
N4.5 E21.5	<lc< td=""><td>-18</td><td></td><td><lc< td=""><td>187</td><td>448</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-18		<lc< td=""><td>187</td><td>448</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	187	448						
N4.5 E3.5	<u> </u>	37	54	<u> </u>	669		1					<u> </u>
N4.5 E4.5	<lc< td=""><td>28</td><td>50</td><td>1</td><td>589</td><td>492</td><td>l</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	28	50	1	589	492	l					<u> </u>
N4.5 E5.5	<lc< td=""><td>9</td><td>43</td><td></td><td>776</td><td></td><td> </td><td>8</td><td>10</td><td><lc< td=""><td>-38</td><td>71</td></lc<></td></lc<>	9	43		776			8	10	<lc< td=""><td>-38</td><td>71</td></lc<>	-38	71
N4.5 E6.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>348</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9		<lc< td=""><td>348</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	348							
N4.5 E7.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>214</td><td>451</td><td>(i</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<></td></lc<>	-9		<lc< td=""><td>214</td><td>451</td><td>(i</td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	214	451	(i					<u> </u>
N4.5 E8.5		46	57		1151		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td>73</td></lc<></td></lc<>	2	6	<lc< td=""><td>-21</td><td>73</td></lc<>	-21	73
N4.5 E9.5	+	48	57		1231	555		8		<lc< td=""><td>46</td><td>80</td></lc<>	46	80
N5.0 E-1.0	┠────	20		<lc< td=""><td>155</td><td></td><td><u> </u></td><td>.<u> </u></td><td></td><td></td><td></td><td> </td></lc<>	155		<u> </u>	. <u> </u>				
N5.0 E-2.0	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>285</td><td></td><td>0</td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	11		<lc< td=""><td>285</td><td></td><td>0</td><td></td><td></td><td></td><td></td><td></td></lc<>	285		0					
N5.0 E0.0	<lc< td=""><td>15</td><td></td><td></td><td>544</td><td></td><td></td><td></td><td></td><td> </td><td></td><td><u>├</u></td></lc<>	15			544							<u>├</u>
N5.0 E1.0		33		<lc< td=""><td>285</td><td></td><td>¥</td><td></td><td></td><td></td><td></td><td><u>├</u></td></lc<>	285		¥					<u>├</u>
N5.0 E10.0	<lc< td=""><td><u> </u></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td><td>363</td><td></td><td>∦</td><td>······</td><td></td><td></td><td></td><td><u> </u></td></lc<>	<u> </u>	· · · · · · · · · · · · · · · · · · ·		363		∦	······				<u> </u>
N5.0 E11.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>648</td><td>·</td><td>╫────</td><td></td><td><u> i</u></td><td> </td><td></td><td></td></lc<>	-4	20		648	·	╫────		<u> i</u>			
N5.0 E12.0		61	52		674							
N5.0 E12.0	<lc< td=""><td>15</td><td>33</td><td></td><td>1658</td><td>·····</td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-63</td><td>71</td></lc<></td></lc<></td></lc<>	15	33		1658	·····	<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-63</td><td>71</td></lc<></td></lc<>	-1		<lc< td=""><td>-63</td><td>71</td></lc<>	-63	71
		61	52		725		<u></u>			~	-03	<u> /</u>
N5.0 E14.0		-4	20		725		<u> </u>			<u> </u>		<u> </u>
N5.0 E15.0	<lc< td=""><td></td><td></td><td></td><td>700 751</td><td></td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>				700 751							
N5.0 E16.0	<lc< td=""><td>-13</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-13										<u> </u>
N5.0 E17.0	<lc< td=""><td>-13</td><td></td><td>+</td><td>544</td><td></td><td></td><td></td><td></td><td></td><td>·</td><td><u> </u></td></lc<>	-13		+	544						·	<u> </u>
N5.0 E18.0		33		<lc< td=""><td>285</td><td>And the second se</td><td><lc< td=""><td><u>1</u></td><td></td><td><lc< td=""><td>-67</td><td>7'</td></lc<></td></lc<></td></lc<>	285	And the second se	<lc< td=""><td><u>1</u></td><td></td><td><lc< td=""><td>-67</td><td>7'</td></lc<></td></lc<>	<u>1</u>		<lc< td=""><td>-67</td><td>7'</td></lc<>	-67	7'
N5.0 E19.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>1114</td><td></td><td><u> </u></td><td>5</td><td>8</td><td><lc< td=""><td>50</td><td>83</td></lc<></td></lc<>	-4	20		1114		<u> </u>	5	8	<lc< td=""><td>50</td><td>83</td></lc<>	50	83
N5.0 E2.0	ļ	33		<lc< td=""><td>233</td><td><u> </u></td><td><b>.</b></td><td></td><td></td><td>ļ</td><td></td><td><u> </u></td></lc<>	233	<u> </u>	<b>.</b>			ļ		<u> </u>
N5.0 E20.0	I <lc< td=""><td>-4</td><td></td><td><lc< td=""><td>104</td><td></td><td></td><td></td><td>  </td><td>ļ</td><td></td><td>ļ</td></lc<></td></lc<>	-4		<lc< td=""><td>104</td><td></td><td></td><td></td><td>  </td><td>ļ</td><td></td><td>ļ</td></lc<>	104					ļ		ļ
N5.0 E21.0	<	-13			337			<u> </u>				
N5.0 E22.0	<b> </b>	24	37		363							- <u></u>
N5.0 E3.0	<lc< td=""><td>15</td><td></td><td></td><td>415</td><td></td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	15			415							<u> </u>
N5.0 E4.0		24	37	·	622							
N5.0 E5.0		33	41		596	463						•

Lc indicates less than the critical level of activity which can be said to be above background.

A negative value is the calculated result of a reading which is below the instrument-specific background.



1

)

1

ì.

,

I

1



	ALPH	AV100	DIRECT	BETA	-GAMMA/10	DO SQ CM	ALPH		ANSFER		GAMMA/	100 SQ C
LOCATION/ITEM	SMF		STD		SMPL	ISTD	SM		STD		MPL	ISTD
COORDINATES	DPI		DEV	[	DPM	DEV	DF		DEV		PM	DEV
N5.0 E6.0		33	41		725	476						
N5.0 E7.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>1866</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>0</td><td></td></lc<></td></lc<></td></lc<>	-4	20		1866	· · · · · · · · · · · · · · · · · · ·	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>0</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>0</td><td></td></lc<>	0	
N5.0 E8.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>518</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	-4	20		518	454						<u> </u>
N5.0 E9.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>207</td><td>419</td><td></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<></td></lc<>	-4		<lc< td=""><td>207</td><td>419</td><td></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<>	207	419			<u> </u>			<u> </u>
N5.5 E-0.5	< <u>L</u> c	11	27	- 20	1036		<lc< td=""><td></td><td></td><td><lc< td=""><td>-88</td><td></td></lc<></td></lc<>			<lc< td=""><td>-88</td><td></td></lc<>	-88	
N5.5 E-1.5	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>155</td><td>449</td><td></td><td></td><td></td><td></td><td>-00</td><td><u> </u></td></lc<></td></lc<>	11		<lc< td=""><td>155</td><td>449</td><td></td><td></td><td></td><td></td><td>-00</td><td><u> </u></td></lc<>	155	449					-00	<u> </u>
N5.5 E0.5	<lc< td=""><td>-18</td><td>30</td><td></td><td>883</td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-59</td><td><u> </u></td></lc<></td></lc<></td></lc<>	-18	30		883		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-59</td><td><u> </u></td></lc<></td></lc<>	2		<lc< td=""><td>-59</td><td><u> </u></td></lc<>	-59	<u> </u>
N5.5 E1.5	<lc< td=""><td>-28</td><td>24</td><td>┣</td><td>2088</td><td></td><td><lc< td=""><td>-1</td><td>······</td><td><lc< td=""><td></td><td><u> </u></td></lc<></td></lc<></td></lc<>	-28	24	┣	2088		<lc< td=""><td>-1</td><td>······</td><td><lc< td=""><td></td><td><u> </u></td></lc<></td></lc<>	-1	······	<lc< td=""><td></td><td><u> </u></td></lc<>		<u> </u>
N5.5 E10.5	<lc< td=""><td>-20</td><td></td><td><lc< td=""><td>2000</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>}·</td></lc<></td></lc<>	-20		<lc< td=""><td>2000</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td>}·</td></lc<>	2000	460						}·
N5.5 E11.5	<lc< td=""><td>28</td><td>50</td><td></td><td>937</td><td></td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-13</td><td><u> </u></td></lc<></td></lc<></td></lc<>	28	50		937		<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-13</td><td><u> </u></td></lc<></td></lc<>	-1		<lc< td=""><td>-13</td><td><u> </u></td></lc<>	-13	<u> </u>
		28		<u> </u>			····					÷
N5.5 Ê12.5	<lc< td=""><td></td><td>50</td><td></td><td>1151</td><td>548</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<></td></lc<>		50		1151	548	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>4</td><td></td></lc<>	4	
N5.5 E13.5	<lc< td=""><td>28</td><td></td><td><lc< td=""><td>-27</td><td>423</td><td></td><td></td><td></td><td><b></b></td><td></td><td>ļ</td></lc<></td></lc<>	28		<lc< td=""><td>-27</td><td>423</td><td></td><td></td><td></td><td><b></b></td><td></td><td>ļ</td></lc<>	-27	423				<b></b>		ļ
N5.5 E14.5	<lc< td=""><td></td><td></td><td><lc< td=""><td>-80</td><td>416</td><td></td><td><u> </u></td><td><b></b></td><td><b> </b></td><td></td><td><b> </b></td></lc<></td></lc<>			<lc< td=""><td>-80</td><td>416</td><td></td><td><u> </u></td><td><b></b></td><td><b> </b></td><td></td><td><b> </b></td></lc<>	-80	416		<u> </u>	<b></b>	<b> </b>		<b> </b>
N5.5 E15.5	<lc< td=""><td>9</td><td>43</td><td><u> </u></td><td>455</td><td>478</td><td></td><td></td><td>·</td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td><u> </u></td></lc<>	9	43	<u> </u>	455	478			·		· · · · · · · · · · · · · · · · · · ·	<u> </u>
N5.5 E16.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>27</td><td>429</td><td>·</td><td></td><td> </td><td></td><td></td><td><u> </u></td></lc<></td></lc<>	0		<lc< td=""><td>27</td><td>429</td><td>·</td><td></td><td> </td><td></td><td></td><td><u> </u></td></lc<>	27	429	·					<u> </u>
N5.5 E17.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>241</td><td>454</td><td></td><td></td><td>ļ</td><td></td><td></td><td>ļ</td></lc<></td></lc<>	-9		<lc< td=""><td>241</td><td>454</td><td></td><td></td><td>ļ</td><td></td><td></td><td>ļ</td></lc<>	241	454			ļ			ļ
N5.5 E18.5	<lc< td=""><td>-9</td><td>35</td><td> </td><td>723</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>21</td><td>ļ</td></lc<></td></lc<></td></lc<>	-9	35		723		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>21</td><td>ļ</td></lc<></td></lc<>	-1	0	<lc< td=""><td>21</td><td>ļ</td></lc<>	21	ļ
N5.5 E19.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>268</td><td>457</td><td>1</td><td></td><td>L</td><td></td><td></td><td></td></lc<></td></lc<>	0		<lc< td=""><td>268</td><td>457</td><td>1</td><td></td><td>L</td><td></td><td></td><td></td></lc<>	268	457	1		L			
N5.5 E2.5	<lc_< td=""><td>18</td><td>47</td><td><lc< td=""><td>268</td><td>457</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc_<>	18	47	<lc< td=""><td>268</td><td>457</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	268	457						
N5.5 E20.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>375</td><td>469</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9	35		375	469						
N5.5 E21.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>642</td><td>498</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9	35		642	498						
N5.5 E3.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>455</td><td>478</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9	35		455	478						
N5.5 E4.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>642</td><td>498</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9	35		642	498						
N5.5 E5.5	1	37	54		1606	589	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>4</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>4</td><td></td></lc<>	4	
N5.5 E6.5		37	54		1231	555		5	8	<lc< td=""><td>-13</td><td><u> </u></td></lc<>	-13	<u> </u>
N5.5 E7.5		37	54	<u> </u>	562	489						
N5.5 E8.5	<lc< td=""><td>18</td><td>47</td><td>ļ — —</td><td>402</td><td>472</td><td></td><td></td><td></td><td></td><td></td><td><u>†</u></td></lc<>	18	47	ļ — —	402	472						<u>†</u>
N5.5 E9.5	<lc< td=""><td>28</td><td>50</td><td><u> </u></td><td>803</td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-46</td><td>· · · · · ·</td></lc<></td></lc<></td></lc<>	28	50	<u> </u>	803		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-46</td><td>· · · · · ·</td></lc<></td></lc<>	2	6	<lc< td=""><td>-46</td><td>· · · · · ·</td></lc<>	-46	· · · · · ·
N6.0 E-1.0	<lc< td=""><td>2</td><td>19</td><td><u>                                      </u></td><td>674</td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>†</td></lc<></td></lc<></td></lc<>	2	19	<u>                                      </u>	674		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>†</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>†</td></lc<>	-8	†
N6.0 E-2.0	1	57	48	<lc< td=""><td>363</td><td>471</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td></lc<>	363	471						<u> </u>
N6.0 E0.0	<lc< td=""><td>6</td><td>27</td><td></td><td>570</td><td>460</td><td></td><td></td><td> </td><td></td><td></td><td><u> </u></td></lc<>	6	27		570	460						<u> </u>
N6.0 E1.0	<lc< td=""><td>6</td><td>27</td><td></td><td>907</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-59</td><td><u> </u></td></lc<></td></lc<></td></lc<>	6	27		907	· · · · · · · · · · · · · · · · · · ·	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-59</td><td><u> </u></td></lc<></td></lc<>	2	6	<lc< td=""><td>-59</td><td><u> </u></td></lc<>	-59	<u> </u>
N6.0 E10.0		33	41	<lc< td=""><td>0</td><td>393</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	0	393						
N6.0 E11.0	<lc< td=""><td>-4</td><td>20</td><td>1900</td><td>389</td><td>440</td><td> </td><td></td><td></td><td></td><td></td><td>f</td></lc<>	-4	20	1900	389	440						f
N6.0 E12.0	<lc< td=""><td>-4</td><td>20</td><td><b> </b></td><td>725</td><td>440</td><td></td><td></td><td></td><td><b>{</b></td><td></td><td><u> </u></td></lc<>	-4	20	<b> </b>	725	440				<b>{</b>		<u> </u>
N6.0 E12.0	<lc< td=""><td>-4</td><td>20</td><td><u> </u></td><td>492</td><td></td><td><b> </b></td><td></td><td> </td><td><u> </u></td><td></td><td><u> </u></td></lc<>	-4	20	<u> </u>	492		<b> </b>			<u> </u>		<u> </u>
									<u> </u>			<u> </u>
N6.0 E14.0	<lc< td=""><td>4</td><td>20</td><td></td><td>855</td><td></td><td><lc< td=""><td>2</td><td>0</td><td><lc< td=""><td>-13</td><td>ł</td></lc<></td></lc<></td></lc<>	4	20		855		<lc< td=""><td>2</td><td>0</td><td><lc< td=""><td>-13</td><td>ł</td></lc<></td></lc<>	2	0	<lc< td=""><td>-13</td><td>ł</td></lc<>	-13	ł
N6.0 E15.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>622</td><td>÷</td><td></td><td></td><td><u> </u></td><td></td><td></td><td><u> </u></td></lc<>	-4	20		622	÷			<u> </u>			<u> </u>
N6.0 E16.0	<lc< td=""><td>-13</td><td></td><td>┨────</td><td>622</td><td></td><td></td><td></td><td><u> </u></td><td><u></u></td><td></td><td><u> </u></td></lc<>	-13		┨────	622				<u> </u>	<u></u>		<u> </u>
N6.0 E17.0	<lc< td=""><td>6</td><td></td><td><u> </u></td><td>985</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><lc< td=""><td>-1</td><td>0</td><td>&lt;<u>L</u>c</td><td>-63</td><td> </td></lc<></td></lc<>	6		<u> </u>	985	· · · · · · · · · · · · · · · · · · ·	<lc< td=""><td>-1</td><td>0</td><td>&lt;<u>L</u>c</td><td>-63</td><td> </td></lc<>	-1	0	< <u>L</u> c	-63	
N6.0 E18.0	<lc< td=""><td>4</td><td>20</td><td></td><td>544</td><td></td><td></td><td></td><td> </td><td></td><td></td><td>{</td></lc<>	4	20		544							{
N6.0 E19.0	<lc< td=""><td>6</td><td>27</td><td></td><td>518</td><td>A</td><td></td><td></td><td><b> </b></td><td></td><td><u> </u></td><td> </td></lc<>	6	27		518	A			<b> </b>		<u> </u>	
N6.0 E2.0	<lc< td=""><td>-4</td><td></td><td><lc< td=""><td>285</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td><td><u> </u></td></lc<></td></lc<>	-4		<lc< td=""><td>285</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td><td><u> </u></td></lc<>	285				ļ			<u> </u>
N6.0 E20.0	<lc< td=""><td>15</td><td>33</td><td><b> </b></td><td>570</td><td></td><td></td><td></td><td>ļ</td><td></td><td></td><td>ļ</td></lc<>	15	33	<b> </b>	570				ļ			ļ
N6.0 E21.0	<lc< td=""><td>6</td><td>27</td><td></td><td>570</td><td></td><td></td><td></td><td></td><td>· · · ·</td><td></td><td></td></lc<>	6	27		570					· · · ·		
N6.0 E22.0	L	33			777		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-25</td><td>L</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-25</td><td>L</td></lc<>	-25	L
N6.0 E3.0	<lc< td=""><td>-13</td><td></td><td><lc< td=""><td>104</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-13		<lc< td=""><td>104</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	104							
N6.0 E4.0		24	37		596	463						
N6.0 E5.0	<lc< td=""><td>6</td><td>27</td><td></td><td>570</td><td>460</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	6	27		570	460						
N6,0 E6.0		33	41		829	487	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-84</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-84</td><td></td></lc<>	-84	
N6.0 E7.0	<lc< td=""><td>15</td><td>33</td><td></td><td>725</td><td>476</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>	15	33		725	476						
N6.0 E8.0		24			751							
V6.0 E9.0	<u> </u>	33				+		5	8	<lc< td=""><td>-13</td><td></td></lc<>	-13	
N6.5 E-0.5	<del>!</del>	20	32		622	•	<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	-1		<lc< td=""><td>-21</td><td></td></lc<>	-21	

<Lc indicates less than the critical level of activity which can be said to be above background.</p>

A negative value is the calculated result of a reading which is below the instrument-specific background.

,

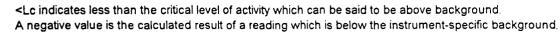
1

1

)

)

			DIRECT							ANSFER			
			SQCM	BETA	-GAMMA/1		CM			SQ.CM	BET	A-GAMMA/	
LOCATION/ITEM		/IPL	STD		SMPL	STD		, i i i i i i i i i i i i i i i i i i i	1PL	STD		SMPL	STD
COORDINATES	D	PM	DEV	Ŀ	DPM	DEV			PM	DEV		DPM	DEV
N6.5 E-1.5	<lc< td=""><td>2</td><td>19</td><td></td><td>751</td><td></td><td>510</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>7</td></lc<></td></lc<></td></lc<>	2	19		751		510	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-8</td><td>7</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-8</td><td>7</td></lc<>	-8	7
N6.5 E0.5	1	Ā	NĂ		NA	NA							
N6.5 E1.5	1	NA A	NA		NA	NA			_				
N6.5 E10.5	<lc< td=""><td>0</td><td>51</td><td></td><td>1040</td><td></td><td>611</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td>7</td></lc<></td></lc<></td></lc<>	0	51		1040		611	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-38</td><td>7</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-38</td><td>7</td></lc<>	-38	7
N6.5 E11.5	<lc< td=""><td>19</td><td>57</td><td>1</td><td>887</td><td></td><td>596</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-17</td><td>7</td></lc<></td></lc<></td></lc<>	19	57	1	887		596	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-17</td><td>7</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-17</td><td>7</td></lc<>	-17	7
N6.5 E12.5	<lc< td=""><td>-39</td><td>34</td><td></td><td>978</td><td></td><td>605</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>17</td><td>7</td></lc<></td></lc<></td></lc<>	-39	34		978		605	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>17</td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>17</td><td>7</td></lc<>	17	7
N6.5 E13.5	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td>· · · · · · · · · · · · · · · · · · ·</td><td></td></lc<>	397		546					· · · · · · · · · · · · · · · · · · ·	
N6.5 E14.5	<lc< td=""><td>-58</td><td>21</td><td></td><td>612</td><td></td><td>569</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-58	21		612		569						
N6.5 E15.5	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>336</td><td></td><td>539</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>336</td><td></td><td>539</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	336		539					<u> </u>	
N6.5 E16.5	<lc< td=""><td>-29</td><td>39</td><td><lc< td=""><td>92</td><td></td><td>512</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-29	39	<lc< td=""><td>92</td><td></td><td>512</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	92		512						
N6.5 E17.5	<lc< td=""><td>19</td><td>57</td><td><u> </u></td><td>826</td><td></td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<></td></lc<>	19	57	<u> </u>	826			<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-33</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-33</td><td></td></lc<>	-33	
N6.5 E18.5	<lc< td=""><td>-29</td><td>39</td><td></td><td>581</td><td></td><td>565</td><td>-20</td><td></td><td></td><td>-20</td><td></td><td><u> </u></td></lc<>	-29	39		581		565	-20			-20		<u> </u>
N6.5 E19.5	<lc< td=""><td>-10</td><td>47</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10	47	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	397		546						
N6.5 E2.5	<lc< td=""><td>10</td><td>54</td><td></td><td>734</td><td></td><td>546 581</td><td><b> </b></td><td></td><td>  </td><td></td><td>·····</td><td> </td></lc<>	10	54		734		546 581	<b> </b>				·····	
					المسجدي الشمعيد النكنديين ومعد						<b> </b>		
N6.5 E20.5	<lc< td=""><td>-19</td><td>43</td><td></td><td>336</td><td></td><td>539</td><td>┞</td><td></td><td></td><td></td><td></td><td><b>↓</b></td></lc<>	-19	43		336		539	┞					<b>↓</b>
N6.5 E21.5	<lc< td=""><td>-39</td><td></td><td><lc< td=""><td>275</td><td></td><td>533</td><td>}</td><td></td><td></td><td></td><td></td><td> </td></lc<></td></lc<>	-39		<lc< td=""><td>275</td><td></td><td>533</td><td>}</td><td></td><td></td><td></td><td></td><td> </td></lc<>	275		533	}					
N6.5 E3.5	<lc< td=""><td>-48</td><td>28</td><td><b></b></td><td>612</td><td></td><td>569</td><td>L</td><td></td><td></td><td>ļ</td><td></td><td>l</td></lc<>	-48	28	<b></b>	612		569	L			ļ		l
N6.5 E4.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>306</td><td></td><td>536</td><td>L</td><td></td><td></td><td></td><td></td><td>L</td></lc<></td></lc<>	0		<lc< td=""><td>306</td><td></td><td>536</td><td>L</td><td></td><td></td><td></td><td></td><td>L</td></lc<>	306		536	L					L
N6.5 E5.5	<lc< td=""><td>29</td><td>60</td><td>L</td><td>703</td><td></td><td>578</td><td></td><td></td><td></td><td></td><td></td><td>ļ</td></lc<>	29	60	L	703		578						ļ
N6.5 E6.5	<lc< td=""><td>19</td><td>43</td><td>L</td><td>1987</td><td></td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>25</td><td></td></lc<></td></lc<></td></lc<>	19	43	L	1987			<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>25</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>25</td><td></td></lc<>	25	
N6.5 E7.5	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>245</td><td></td><td>529</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>245</td><td></td><td>529</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	245		529						
N6.5 E8.5	<lc< td=""><td>10</td><td>54</td><td></td><td>612</td><td></td><td>569</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	10	54		612		569						
N6.5 E9.5	<lc< td=""><td>19</td><td>57</td><td></td><td>1254</td><td></td><td>631</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<></td></lc<>	19	57		1254		631	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-21</td><td></td></lc<>	-21	
N7.0 E-1.0	<lc< td=""><td>2</td><td>19</td><td><lc< td=""><td>78</td><td></td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	2	19	<lc< td=""><td>78</td><td></td><td>440</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	78		440						
N7.0 E-2.0		76	55	<lc< td=""><td>78</td><td></td><td>440</td><td>ļ</td><td>-<u>-</u></td><td></td><td></td><td></td><td></td></lc<>	78		440	ļ	- <u>-</u>				
N7.0 E1.0		NA	NA		NA	NĂ							
N7.0 E10.0	<lc< td=""><td>-19</td><td></td><td><lc< td=""><td>306</td><td></td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19		<lc< td=""><td>306</td><td></td><td>536</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	306		536						
N7.0 E11.0	<lc< td=""><td>-10</td><td></td><td><lc< td=""><td>214</td><td></td><td>526</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-10		<lc< td=""><td>214</td><td></td><td>526</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	214		526						
N7.0 E12.0	<lc< td=""><td>-19</td><td>43</td><td></td><td>520</td><td></td><td>559</td><td></td><td>·</td><td></td><td></td><td></td><td> </td></lc<>	-19	43		520		559		·				
N7.0 E13.0	<lc< td=""><td>-48</td><td>28</td><td><u> </u></td><td>489</td><td></td><td>556</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-48	28	<u> </u>	489		556						
N7.0 E14.0	<lc< td=""><td>-40</td><td></td><td>╂</td><td>795</td><td></td><td>_</td><td><lc< td=""><td></td><td></td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<></td></lc<>	-40		╂	795		_	<lc< td=""><td></td><td></td><td><lc< td=""><td>-8</td><td></td></lc<></td></lc<>			<lc< td=""><td>-8</td><td></td></lc<>	-8	
N7.0 E15.0	<lc< td=""><td>10</td><td>54</td><td>┣━━━</td><td>550</td><td></td><td>-</td><td></td><td>-  </td><td></td><td><lc< td=""><td>-0</td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<></td></lc<>	10	54	┣━━━	550		-		-		<lc< td=""><td>-0</td><td>· · · · · · · · · · · · · · · · · · ·</td></lc<>	-0	· · · · · · · · · · · · · · · · · · ·
						_	562				[		
N7.0 E16.0	<lc< td=""><td>-48</td><td></td><td><lc< td=""><td>122</td><td></td><td>516</td><td><b>[</b></td><td></td><td></td><td> </td><td></td><td></td></lc<></td></lc<>	-48		<lc< td=""><td>122</td><td></td><td>516</td><td><b>[</b></td><td></td><td></td><td> </td><td></td><td></td></lc<>	122		516	<b>[</b>					
N7.0 E17.0	<lc_< td=""><td>-10</td><td>47</td><td><b> </b></td><td>703</td><td><u> </u></td><td>578</td><td>1</td><td></td><td>  </td><td> </td><td></td><td>ļ</td></lc_<>	-10	47	<b> </b>	703	<u> </u>	578	1					ļ
N7.0 E18.0	<lc< td=""><td>-10</td><td>47</td><td><b> </b></td><td>550</td><td></td><td>562</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-10	47	<b> </b>	550		562						
N7.0 E19.0	<lc< td=""><td>-29</td><td>39</td><td>I</td><td>459</td><td></td><td>553</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	-29	39	I	459		553	1					
N7.0 E2.0		NA	NA		NA	NA .							
N7.0 E20.0	<lc< td=""><td>-19</td><td>43</td><td><lc< td=""><td>367</td><td></td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-19	43	<lc< td=""><td>367</td><td></td><td>543</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	367		543						
N7.0 E21.0	<lc< td=""><td>10</td><td>54</td><td><lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td>[</td><td></td><td></td></lc<></td></lc<>	10	54	<lc< td=""><td>397</td><td></td><td>546</td><td></td><td></td><td></td><td>[</td><td></td><td></td></lc<>	397		546				[		
N7.0 E22.0	<lc< td=""><td>-48</td><td>28</td><td></td><td>1009</td><td></td><td>608</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<></td></lc<>	-48	28		1009		608	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-21</td><td></td></lc<>	-21	
N7.0 E3.0		NĀ	NA		NA	NA							
N7.0 E4.0	<lc< td=""><td>-39</td><td></td><td></td><td>428</td><td></td><td>549</td><td></td><td></td><td></td><td> </td><td>······</td><td></td></lc<>	-39			428		549					······	
N7.0 E5.0	<u> </u>	48		_	612		569						
N7.0 E6.0	<lc< td=""><td>10</td><td></td><td></td><td>2721</td><td></td><td>756</td><td></td><td>5</td><td>8</td><td><lc< td=""><td>13</td><td></td></lc<></td></lc<>	10			2721		756		5	8	<lc< td=""><td>13</td><td></td></lc<>	13	
N7.0 E7.0	<lc< td=""><td></td><td></td><td></td><td>948</td><td></td><td>602</td><td></td><td></td><td></td><td><lc< td=""><td></td><td></td></lc<></td></lc<>				948		602				<lc< td=""><td></td><td></td></lc<>		
N7.0 E8.0		77	74	_	5595		953		5		<lc< td=""><td>46</td><td></td></lc<>	46	
N7.0 E9.0	<lc< td=""><td>-29</td><td></td><td></td><td>2905</td><td></td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<></td></lc<>	-29			2905			<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-21</td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-21</td><td></td></lc<>	-21	
N7.5 E-0.5	<b> </b>	57	48		751			<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-50</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-50</td><td></td></lc<>	-50	
N7.5 E-1.5	l	48		<lc< td=""><td>285</td><td></td><td>463</td><td></td><td></td><td> </td><td>ļ</td><td></td><td> </td></lc<>	285		463				ļ		
N7.5 E0.5	<lc< td=""><td>28</td><td></td><td><lc< td=""><td>241</td><td></td><td>454</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<></td></lc<>	28		<lc< td=""><td>241</td><td></td><td>454</td><td></td><td></td><td></td><td></td><td></td><td> </td></lc<>	241		454						
N7.5 E1.5	<lc< td=""><td>-9</td><td></td><td></td><td>723</td><td></td><td>506</td><td></td><td>8</td><td>10</td><td><lc< td=""><td>-88</td><td></td></lc<></td></lc<>	-9			723		506		8	10	<lc< td=""><td>-88</td><td></td></lc<>	-88	
N7.5 E10.5	<lc< td=""><td>-28</td><td></td><td><lc< td=""><td>0</td><td></td><td>426</td><td></td><td></td><td></td><td>1</td><td></td><td></td></lc<></td></lc<>	-28		<lc< td=""><td>0</td><td></td><td>426</td><td></td><td></td><td></td><td>1</td><td></td><td></td></lc<>	0		426				1		
N7.5 E11.5	<lc< td=""><td>9</td><td>43</td><td></td><td>642</td><td></td><td>498</td><td>3</td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		642		498	3					
N7.5 E12.5	<lc< td=""><td>9</td><td>43</td><td></td><td>455</td><td></td><td>478</td><td>1</td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		455		478	1					



;

	A1 51		DIRECT	0574					ANSFER		<u></u>		
	ALPHA/100 SQ CM BETA-GAMMA/100 SQ CM							_	SQCM		GAMMA/		<u>.</u> M
LOCATION/ITEM			STD	ł	SMPL	STD	SM	-	STD		MPL	STD	
COORDINATES			DEV	ļ	DPM	DEV	DP	<u>'M</u>	DEV		PM	DEV	_
N7.5 E13.5	<lc< td=""><td>-18</td><td>30</td><td><lc< td=""><td>187</td><td>448</td><td><b></b></td><td></td><td></td><td></td><td></td><td>ļ</td><td>_</td></lc<></td></lc<>	-18	30	<lc< td=""><td>187</td><td>448</td><td><b></b></td><td></td><td></td><td></td><td></td><td>ļ</td><td>_</td></lc<>	187	448	<b></b>					ļ	_
N7.5 E14.5	<lc< td=""><td>-9</td><td>A</td><td><b> </b></td><td>1017</td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>0</td><td><u> </u></td><td>7</td></lc<></td></lc<></td></lc<>	-9	A	<b> </b>	1017		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>0</td><td><u> </u></td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>0</td><td><u> </u></td><td>7</td></lc<>	0	<u> </u>	7
N7.5 E15.5	<lc< td=""><td>-18</td><td>30</td><td>L</td><td>696</td><td>503</td><td></td><td></td><td></td><td>·</td><td></td><td>1</td><td></td></lc<>	-18	30	L	696	503				·		1	
N7.5 E16.5	<lc< td=""><td>00</td><td>40</td><td></td><td>509</td><td>484</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	00	40		509	484							
N7.5 E17.5	<lc< td=""><td>9</td><td></td><td></td><td>616</td><td>495</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	9			616	495							
N7.5 E18.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>161</td><td>445</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9	35	<lc< td=""><td>161</td><td>445</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	161	445							
N7.5 E19.5	<lc< td=""><td>-28</td><td>24</td><td></td><td>455</td><td>478</td><td></td><td></td><td></td><td>•</td><td></td><td></td><td></td></lc<>	-28	24		455	478				•			
N7.5 E2.5	<lc< td=""><td>-18</td><td>30</td><td>ļ</td><td>616</td><td>495</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	-18	30	ļ	616	495						1	
N7.5 E20.5	<lc< td=""><td>9</td><td>43</td><td><lc< td=""><td>241</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>	9	43	<lc< td=""><td>241</td><td>454</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	241	454						1	
N7.5 E21.5	<lc< td=""><td>0</td><td>40</td><td>1</td><td>482</td><td>481</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	0	40	1	482	481						1	
N7.5 E3.5	<lc< td=""><td>-9</td><td>35</td><td>1</td><td>803</td><td>514</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>0</td><td>1</td><td>-</td></lc<></td></lc<></td></lc<>	-9	35	1	803	514	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>0</td><td>1</td><td>-</td></lc<></td></lc<>	2	6	<lc< td=""><td>0</td><td>1</td><td>-</td></lc<>	0	1	-
N7.5 E4.5	<u> </u>	55		1	1419	572						1	
N7.5 E5.5	1	55	59	1	669	501			†			t	_
N7.5 E6.5		258	103		857		<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-4</td><td>1</td><td>7</td></lc<></td></lc<>	-1	0	<lc< td=""><td>-4</td><td>1</td><td>7</td></lc<>	-4	1	7
N7.5 E7.5	<lc< td=""><td>9</td><td></td><td>1</td><td>4819</td><td></td><td>&lt;</td><td>2</td><td></td><td><lc< td=""><td>-33</td><td>·</td><td></td></lc<></td></lc<>	9		1	4819		<	2		<lc< td=""><td>-33</td><td>·</td><td></td></lc<>	-33	·	
N7.5 E8.5	<lc< td=""><td>-18</td><td>30</td><td><u> </u></td><td>1767</td><td>603</td><td><u> </u></td><td></td><td>†</td><td><u>                                      </u></td><td></td><td><u>†                                    </u></td><td>-</td></lc<>	-18	30	<u> </u>	1767	603	<u> </u>		†	<u>                                      </u>		<u>†                                    </u>	-
N7.5 E9.5	<lc< td=""><td>0</td><td>40</td><td>1</td><td>1365</td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-71</td><td><u> </u></td><td>e</td></lc<></td></lc<></td></lc<>	0	40	1	1365		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-71</td><td><u> </u></td><td>e</td></lc<></td></lc<>	2		<lc< td=""><td>-71</td><td><u> </u></td><td>e</td></lc<>	-71	<u> </u>	e
N8.0 E-1.0	<lc< td=""><td>11</td><td>27</td><td>1</td><td>1088</td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-33</td><td></td><td></td></lc<></td></lc<></td></lc<>	11	27	1	1088		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-33</td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-33</td><td></td><td></td></lc<>	-33		
N8.0 E-2.0		39	<u> </u>	<lc< td=""><td>000</td><td></td><td></td><td>2</td><td><sup>0</sup></td><td></td><td></td><td><u>├</u>────</td><td></td></lc<>	000			2	<sup>0</sup>			<u>├</u> ────	
N8.0 E1.0	<lc< td=""><td>-39</td><td>34</td><td><lc< td=""><td>153</td><td></td><td>l</td><td></td><td></td><td></td><td>×</td><td>╂</td><td>-</td></lc<></td></lc<>	-39	34	<lc< td=""><td>153</td><td></td><td>l</td><td></td><td></td><td></td><td>×</td><td>╂</td><td>-</td></lc<>	153		l				×	╂	-
N8.0 E10.0	<lc< td=""><td>-48</td><td></td><td></td><td>642</td><td>572</td><td></td><td></td><td>}</td><td></td><td></td><td>┨─────</td><td>-</td></lc<>	-48			642	572			}			┨─────	-
N8.0 E11.0	<lc< td=""><td>-40</td><td></td><td>╡───</td><td>948</td><td></td><td><lc< td=""><td></td><td><u> </u></td><td><lc< td=""><td>25</td><td><del> </del></td><td>-</td></lc<></td></lc<></td></lc<>	-40		╡───	948		<lc< td=""><td></td><td><u> </u></td><td><lc< td=""><td>25</td><td><del> </del></td><td>-</td></lc<></td></lc<>		<u> </u>	<lc< td=""><td>25</td><td><del> </del></td><td>-</td></lc<>	25	<del> </del>	-
N8.0 E12.0		19		<u> </u>	1376	+	·····	<u></u> -1		<lc< td=""><td>-38</td><td></td><td>-</td></lc<>	-38		-
	<lc< td=""><td></td><td></td><td></td><td></td><td></td><td><lc< td=""><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>						<lc< td=""><td></td><td></td><td></td><td></td><td></td><td></td></lc<>						
N8.0 E13.0	<lc< td=""><td>10</td><td>÷</td><td>ļ</td><td>917</td><td>· · · · · · · · · · · · · · · · · · ·</td><td><lc< td=""><td>-1</td><td>ļ0</td><td><lc< td=""><td>-4</td><td></td><td>_</td></lc<></td></lc<></td></lc<>	10	÷	ļ	917	· · · · · · · · · · · · · · · · · · ·	<lc< td=""><td>-1</td><td>ļ0</td><td><lc< td=""><td>-4</td><td></td><td>_</td></lc<></td></lc<>	-1	ļ0	<lc< td=""><td>-4</td><td></td><td>_</td></lc<>	-4		_
N8.0 E14.0	<lc< td=""><td>-48</td><td>28</td><td></td><td>581</td><td>565</td><td>ļ</td><td></td><td><b></b></td><td><u> </u></td><td></td><td><b> </b></td><td>_</td></lc<>	-48	28		581	565	ļ		<b></b>	<u> </u>		<b> </b>	_
N8.0 E15.0	<lc< td=""><td>-19</td><td></td><td><lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td>·</td><td></td><td><u> </u></td><td>_</td></lc<></td></lc<>	-19		<lc< td=""><td>367</td><td>543</td><td></td><td></td><td></td><td>·</td><td></td><td><u> </u></td><td>_</td></lc<>	367	543				·		<u> </u>	_
N8.0 E16.0	<lc< td=""><td>-10</td><td></td><td></td><td>459</td><td>553</td><td></td><td></td><td>ļ</td><td></td><td></td><td><b> </b></td><td></td></lc<>	-10			459	553			ļ			<b> </b>	
N8.0 E17.0	<lc< td=""><td>29</td><td>+</td><td><b> </b></td><td>642</td><td>572</td><td>∦</td><td></td><td>ļ</td><td></td><td></td><td><u> </u></td><td>_</td></lc<>	29	+	<b> </b>	642	572	∦		ļ			<u> </u>	_
N8.0 E18.0	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>275</td><td>533</td><td>l</td><td></td><td>Ì</td><td></td><td></td><td>ļ</td><td>_</td></lc<></td></lc<>	0		<lc< td=""><td>275</td><td>533</td><td>l</td><td></td><td>Ì</td><td></td><td></td><td>ļ</td><td>_</td></lc<>	275	533	l		Ì			ļ	_
N8.0 E19.0	<lc< td=""><td>-39</td><td></td><td></td><td>734</td><td>581</td><td><b>f</b></td><td></td><td>ļ</td><td></td><td></td><td>ļ</td><td>_</td></lc<>	-39			734	581	<b>f</b>		ļ			ļ	_
N8.0 E2.0	<lc< td=""><td>-29</td><td></td><td><lc< td=""><td>122</td><td>516</td><td>I</td><td></td><td>ļ</td><td></td><td></td><td><b></b></td><td></td></lc<></td></lc<>	-29		<lc< td=""><td>122</td><td>516</td><td>I</td><td></td><td>ļ</td><td></td><td></td><td><b></b></td><td></td></lc<>	122	516	I		ļ			<b></b>	
N8.0 E20.0	<lc< td=""><td>-39</td><td></td><td></td><td>550</td><td></td><td>l</td><td></td><td></td><td>   </td><td></td><td><u></u></td><td>_</td></lc<>	-39			550		l			 		<u></u>	_
N8.0 E21.0	<lc< td=""><td>0</td><td></td><td>l</td><td>550</td><td></td><td></td><td></td><td></td><td>ļ</td><td></td><td><u> </u></td><td></td></lc<>	0		l	550					ļ		<u> </u>	
N8.0 E22.0	<lc< td=""><td>-58</td><td>21</td><td><lc< td=""><td>397</td><td>546</td><td>li</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-58	21	<lc< td=""><td>397</td><td>546</td><td>li</td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	397	546	li						
N8.0 E3.0	۱ ۱	<u> </u>	NA		NA	NA							
N8.0 E4.0	<lc< td=""><td>19</td><td>57</td><td><lc< td=""><td>336</td><td>539</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	19	57	<lc< td=""><td>336</td><td>539</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	336	539							
N8.0 E5.0	<lc< td=""><td>-19</td><td></td><td></td><td>734</td><td>581</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-19			734	581							
N8.0 E6.0	<lc< td=""><td>-10</td><td>47</td><td></td><td>1590</td><td>662</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>17</td><td></td><td></td></lc<></td></lc<></td></lc<>	-10	47		1590	662	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>17</td><td></td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>17</td><td></td><td></td></lc<>	17		
N8.0 E7.0		48			<b>*</b> 58554	2670		11		<lc< td=""><td>-21</td><td></td><td></td></lc<>	-21		
N8.0 E8.0	<lc< td=""><td>19</td><td></td><td></td><td>1101</td><td>·····</td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>·0</td><td></td><td></td></lc<></td></lc<></td></lc<>	19			1101	·····	<lc< td=""><td>2</td><td></td><td><lc< td=""><td>·0</td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>·0</td><td></td><td></td></lc<>	·0		
N8.0 E9.0	<lc< td=""><td>-10</td><td></td><td></td><td>489</td><td></td><td></td><td></td><td>1</td><td></td><td></td><td>1</td><td>_</td></lc<>	-10			489				1			1	_
N8.5 E-0.5	<lc< td=""><td>2</td><td></td><td></td><td>674</td><td></td><td></td><td>5</td><td>8</td><td><lc< td=""><td>-63</td><td>1</td><td></td></lc<></td></lc<>	2			674			5	8	<lc< td=""><td>-63</td><td>1</td><td></td></lc<>	-63	1	
N8.5 E-1.5	<u> </u>	39			466		<u></u>		†	<u> </u>		1	-
N8.5 E0.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>294</td><td></td><td><u>u</u></td><td></td><td><u> </u></td><td><b> </b></td><td></td><td>1</td><td></td></lc<></td></lc<>	9		<lc< td=""><td>294</td><td></td><td><u>u</u></td><td></td><td><u> </u></td><td><b> </b></td><td></td><td>1</td><td></td></lc<>	294		<u>u</u>		<u> </u>	<b> </b>		1	
N8.5 E1.5	<lc< td=""><td>-18</td><td></td><td>_</td><td>642</td><td></td><td></td><td>····_</td><td>ţ</td><td>·</td><td></td><td>t</td><td></td></lc<>	-18		_	642			····_	ţ	·		t	
N8.5 E10.5	<lc< td=""><td>9</td><td></td><td></td><td>402</td><td></td><td></td><td>-<u>-</u></td><td>t</td><td></td><td></td><td>1</td><td>-</td></lc<>	9			402			- <u>-</u>	t			1	-
N8.5 E11.5	<lc< td=""><td>9</td><td></td><td></td><td>857</td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td><u>†</u></td><td></td></lc<></td></lc<></td></lc<>	9			857		<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-8</td><td><u>†</u></td><td></td></lc<></td></lc<>	2	6	<lc< td=""><td>-8</td><td><u>†</u></td><td></td></lc<>	-8	<u>†</u>	
N8.5 E12.5	<lc< td=""><td></td><td></td><td></td><td>803</td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-13</td><td></td><td></td></lc<></td></lc<></td></lc<>				803		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-13</td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-13</td><td></td><td></td></lc<>	-13		
N8.5 E13.5	<lc< td=""><td>-18</td><td></td><td></td><td>723</td><td></td><td>A</td><td>2</td><td></td><td><lc< td=""><td>4</td><td></td><td>-</td></lc<></td></lc<>	-18			723		A	2		<lc< td=""><td>4</td><td></td><td>-</td></lc<>	4		-
N8.5 E14.5	<lc< td=""><td>-18</td><td></td><td></td><td>455</td><td></td><td></td><td></td><td>°</td><td></td><td></td><td>╂────</td><td>-</td></lc<>	-18			455				°			╂────	-
									<u>├</u>	<b> </b>		┼────	-
N8.5 E15.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>214</td><td></td><td></td><td></td><td><u> </u></td><td>[<u> </u></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	0		<lc< td=""><td>214</td><td></td><td></td><td></td><td><u> </u></td><td>[<u> </u></td><td></td><td><u> </u></td><td></td></lc<>	214				<u> </u>	[ <u> </u>		<u> </u>	
N8.5 E16.5	<lc< td=""><td>0</td><td></td><td></td><td>402</td><td></td><td><u></u></td><td></td><td>t</td><td></td><td></td><td><del> </del></td><td></td></lc<>	0			402		<u></u>		t			<del> </del>	
N8.5 E17.5	<lc< td=""><td>9</td><td></td><td></td><td>750</td><td></td><td><lc< td=""><td>2</td><td></td><td><lc< td=""><td>-17</td><td></td><td></td></lc<></td></lc<></td></lc<>	9			750		<lc< td=""><td>2</td><td></td><td><lc< td=""><td>-17</td><td></td><td></td></lc<></td></lc<>	2		<lc< td=""><td>-17</td><td></td><td></td></lc<>	-17		
N8.5 E18.5	<lc< td=""><td>0</td><td>40</td><td>1</td><td>883</td><td>522</td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>17</td><td>1</td><td></td></lc<></td></lc<></td></lc<>	0	40	1	883	522	<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>17</td><td>1</td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>17</td><td>1</td><td></td></lc<>	17	1	

Lc indicates less than the critical level of activity which can be said to be above background.

A negative value is the calculated result of a reading which is below the instrument-specific background.

ì

)

1

)

			DIRECT				·		_	NSFER				_
								ALPHA/10	_			<b>JAMMA</b> /		CM
LOCATION/ITEM			STD		SMPL	STD		SMPL	S	STD	SN	1PL	STD	
COORDINATES	D	PM	DEV	· .	DPM	DEV		DPM_		DEV	DI	<u>PM</u>	DEV	
N8.5 E19.5	<lc< td=""><td>-18</td><td>30</td><td><lc< td=""><td>-294</td><td>31</td><td>89</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-18	30	<lc< td=""><td>-294</td><td>31</td><td>89</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-294	31	89							
N8.5 E2.5	<lc< td=""><td>18</td><td></td><td><lc< td=""><td>294</td><td>4</td><td>60</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	18		<lc< td=""><td>294</td><td>4</td><td>60</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	294	4	60							
N8.5 E20.5	<lc< td=""><td>-28</td><td>24</td><td><lc< td=""><td>161</td><td>4</td><td>45</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-28	24	<lc< td=""><td>161</td><td>4</td><td>45</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	161	4	45							
N8.5 E21.5	<lc< td=""><td>9</td><td>43</td><td><lc< td=""><td>214</td><td>4</td><td>51</td><td></td><td></td><td></td><td></td><td>······</td><td>1</td><td></td></lc<></td></lc<>	9	43	<lc< td=""><td>214</td><td>4</td><td>51</td><td></td><td></td><td></td><td></td><td>······</td><td>1</td><td></td></lc<>	214	4	51					······	1	
N8.5 E3.5	<lc< td=""><td>9</td><td>43</td><td></td><td>375</td><td>4</td><td>69</td><td></td><td>-1-</td><td></td><td></td><td></td><td></td><td></td></lc<>	9	43		375	4	69		-1-					
N8.5 E4.5	<lc< td=""><td>18</td><td>47</td><td><lc< td=""><td>134</td><td>4</td><td>42</td><td>······································</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	18	47	<lc< td=""><td>134</td><td>4</td><td>42</td><td>······································</td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	134	4	42	······································					<u> </u>	
N8.5 E5.5	<lc< td=""><td>-18</td><td></td><td><lc< td=""><td>187</td><td></td><td>48</td><td>· · · · · · · · · · · · · · · · · · ·</td><td>-+-</td><td></td><td></td><td>······</td><td>t</td><td></td></lc<></td></lc<>	-18		<lc< td=""><td>187</td><td></td><td>48</td><td>· · · · · · · · · · · · · · · · · · ·</td><td>-+-</td><td></td><td></td><td>······</td><td>t</td><td></td></lc<>	187		48	· · · · · · · · · · · · · · · · · · ·	-+-			······	t	
N8.5 E6.5	<u> </u>	64	62		6130		01		5	8	<lc< td=""><td>59</td><td><u> </u></td><td>8</td></lc<>	59	<u> </u>	8
N8.5 E7.5	<lc< td=""><td>9</td><td>43</td><td><u> </u></td><td>509</td><td></td><td>84</td><td></td><td>-+-</td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	9	43	<u> </u>	509		84		-+-				<u> </u>	
N8.5 E8.5	<lc< td=""><td>18</td><td></td><td><lc< td=""><td>294</td><td></td><td>60</td><td></td><td>-+-</td><td></td><td></td><td>-<u></u></td><td>+</td><td></td></lc<></td></lc<>	18		<lc< td=""><td>294</td><td></td><td>60</td><td></td><td>-+-</td><td></td><td></td><td>-<u></u></td><td>+</td><td></td></lc<>	294		60		-+-			- <u></u>	+	
N8.5 E9.5	<lc< td=""><td>18</td><td>47</td><td>1-20</td><td>616</td><td></td><td>95</td><td></td><td>-+-</td><td></td><td></td><td></td><td><del> </del></td><td></td></lc<>	18	47	1-20	616		95		-+-				<del> </del>	
N9.0 E-1.0	<lc< td=""><td>11</td><td></td><td><lc< td=""><td>259</td><td></td><td>60</td><td></td><td>-+-</td><td></td><td></td><td></td><td>+</td><td></td></lc<></td></lc<>	11		<lc< td=""><td>259</td><td></td><td>60</td><td></td><td>-+-</td><td></td><td></td><td></td><td>+</td><td></td></lc<>	259		60		-+-				+	
N9.0 E-2.0		20		<lc< td=""><td>130</td><td></td><td>46</td><td></td><td>-+-</td><td></td><td></td><td></td><td>+</td><td></td></lc<>	130		46		-+-				+	
				·	725		76		-+-			·	+	
N9.0 E0.0	<lc< td=""><td><u>-13</u> 15</td><td>10</td><td></td><td>and the second secon</td><td></td><td></td><td></td><td>╶┼╴</td><td></td><td></td><td>47</td><td><u>.</u></td><td>-7</td></lc<>	<u>-13</u> 15	10		and the second secon				╶┼╴			47	<u>.</u>	-7
N9.0 E1.0	<lc< td=""><td></td><td></td><td></td><td>829</td><td></td><td></td><td><lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-17</td><td></td><td></td></lc<></td></lc<></td></lc<>				829			<lc< td=""><td>-1</td><td>0</td><td><lc< td=""><td>-17</td><td></td><td></td></lc<></td></lc<>	-1	0	<lc< td=""><td>-17</td><td></td><td></td></lc<>	-17		
N9.0 E10.0		24		<lc< td=""><td>181</td><td></td><td>16</td><td></td><td>_</td><td></td><td></td><td></td><td><b></b></td><td></td></lc<>	181		16		_				<b></b>	
N9.0 E11.0	<lc< td=""><td>6</td><td>27</td><td></td><td>751</td><td></td><td>79</td><td></td><td>_</td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	6	27		751		79		_				<u> </u>	
N9.0 E12.0	<lc< td=""><td>15</td><td>33</td><td>¥</td><td>855</td><td></td><td></td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-67</td><td><b></b></td><td>7</td></lc<></td></lc<></td></lc<>	15	33	¥	855			<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-67</td><td><b></b></td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>-67</td><td><b></b></td><td>7</td></lc<>	-67	<b></b>	7
N9.0 E13.0	<u> </u>	42	45.	<b> </b>	337		34		-+		ļ		<u> </u>	·
N9.0 E14.0	<lc< td=""><td>-4</td><td>20</td><td></td><td>648</td><td></td><td>68</td><td>Ļ</td><td></td><td></td><td> </td><td></td><td><u> </u></td><td></td></lc<>	-4	20		648		68	Ļ					<u> </u>	
N9.0 E15.0	<u> </u>	24			363		37							
N9.0 E16.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>52</td><td></td><td>87</td><td>L</td><td></td><td></td><td>[</td><td></td><td></td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>52</td><td></td><td>87</td><td>L</td><td></td><td></td><td>[</td><td></td><td></td><td></td></lc<>	52		87	L			[			
N9.0 E17.0	<lc< td=""><td>-13</td><td>10</td><td> </td><td>518</td><td>4</td><td>54</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-13	10		518	4	54							
N9.0 E18.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>311</td><td>4</td><td>31</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>311</td><td>4</td><td>31</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	311	4	31							
N9.0 E19.0	<lc< td=""><td>6</td><td>27</td><td><lc< td=""><td>285</td><td>4</td><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6	27	<lc< td=""><td>285</td><td>4</td><td>28</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	285	4	28							
N9.0 E2.0	<lc< td=""><td>6</td><td>27</td><td></td><td>985</td><td>5</td><td>03</td><td><lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-59</td><td></td><td>7</td></lc<></td></lc<></td></lc<>	6	27		985	5	03	<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>-59</td><td></td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>-59</td><td></td><td>7</td></lc<>	-59		7
N9.0 E20.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>78</td><td>4</td><td>03</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>78</td><td>4</td><td>03</td><td></td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	78	4	03						1	
N9.0 E21.0	<lc< td=""><td>6</td><td>27</td><td><lc< td=""><td>104</td><td>4</td><td>06</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	6	27	<lc< td=""><td>104</td><td>4</td><td>06</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	104	4	06							
N9.0 E22.0	<lc< td=""><td>-4</td><td>20</td><td><lc< td=""><td>311</td><td>4</td><td>31</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-4	20	<lc< td=""><td>311</td><td>4</td><td>31</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	311	4	31							
N9.0 E3.0		33	41	<lc< td=""><td>155</td><td></td><td>13</td><td>· · ·</td><td></td><td></td><td></td><td></td><td>1</td><td></td></lc<>	155		13	· · ·					1	
N9.0 E4.0	<lc< td=""><td>6</td><td></td><td></td><td>415</td><td></td><td>43</td><td></td><td>-+-</td><td></td><td></td><td>·</td><td>1</td><td></td></lc<>	6			415		43		-+-			·	1	
N9.0 E5.0	<u> </u>	24	37	<u> </u>	570		60							
N9.0 E6.0	<u> </u>	33		<lc< td=""><td>207</td><td></td><td>19</td><td></td><td></td><td></td><td></td><td></td><td><u> </u></td><td></td></lc<>	207		19						<u> </u>	
N9.0 E7.0	<lc< td=""><td>-4</td><td>+</td><td><lc< td=""><td>181</td><td></td><td>16</td><td></td><td>-+-</td><td></td><td> </td><td></td><td><u> </u></td><td></td></lc<></td></lc<>	-4	+	<lc< td=""><td>181</td><td></td><td>16</td><td></td><td>-+-</td><td></td><td> </td><td></td><td><u> </u></td><td></td></lc<>	181		16		-+-				<u> </u>	
N9.0 E8.0	<lc< td=""><td>-4</td><td>20</td><td>H</td><td>440</td><td>·</td><td>46</td><td></td><td>-+-</td><td></td><td></td><td></td><td>+</td><td></td></lc<>	-4	20	H	440	·	46		-+-				+	
N9.0 E9.0		33			518		54	<u> </u>	-+-		<u> </u>		<u>├</u> ───	
	10						_		-+-				+	
	<lc< td=""><td>20</td><td></td><td><lc< td=""><td>78</td><td></td><td>40</td><td><u> </u></td><td>-+-</td><td></td><td> </td><td></td><td>╂</td><td></td></lc<></td></lc<>	20		<lc< td=""><td>78</td><td></td><td>40</td><td><u> </u></td><td>-+-</td><td></td><td> </td><td></td><td>╂</td><td></td></lc<>	78		40	<u> </u>	-+-				╂	
N9.5 E-1.5				<lc< td=""><td>233</td><td></td><td>57</td><td></td><td>-+-</td><td></td><td><u> </u></td><td></td><td>·</td><td></td></lc<>	233		57		-+-		<u> </u>		·	
N9.5 E0.5	<lc< td=""><td>28</td><td></td><td><lc< td=""><td>107</td><td></td><td>39</td><td></td><td></td><td></td><td><b>├</b>────</td><td></td><td><u>↓</u></td><td></td></lc<></td></lc<>	28		<lc< td=""><td>107</td><td></td><td>39</td><td></td><td></td><td></td><td><b>├</b>────</td><td></td><td><u>↓</u></td><td></td></lc<>	107		39				<b>├</b> ────		<u>↓</u>	
N9.5 E1.5	<lc< td=""><td>-18</td><td></td><td><lc< td=""><td>27</td><td></td><td>29</td><td></td><td><u>_</u> -</td><td></td><td> </td><td></td><td></td><td></td></lc<></td></lc<>	-18		<lc< td=""><td>27</td><td></td><td>29</td><td></td><td><u>_</u> -</td><td></td><td> </td><td></td><td></td><td></td></lc<>	27		29		<u>_</u>  -					
N9.5 E10.5		37	54		1419			<lc< td=""><td>2</td><td>6</td><td><lc< td=""><td>4</td><td></td><td>7</td></lc<></td></lc<>	2	6	<lc< td=""><td>4</td><td></td><td>7</td></lc<>	4		7
N9.5 E11.5	<lc< td=""><td>9</td><td></td><td></td><td>428</td><td></td><td>75</td><td></td><td></td><td></td><td>L</td><td></td><td><b></b></td><td></td></lc<>	9			428		75				L		<b></b>	
N9.5 E12.5	<lc< td=""><td>0</td><td></td><td><lc< td=""><td>241</td><td></td><td>54</td><td></td><td><math>\perp</math></td><td></td><td></td><td>~</td><td>ļ</td><td></td></lc<></td></lc<>	0		<lc< td=""><td>241</td><td></td><td>54</td><td></td><td><math>\perp</math></td><td></td><td></td><td>~</td><td>ļ</td><td></td></lc<>	241		54		$\perp$			~	ļ	
N9.5 E13.5	L	46	•·····		562		89				Ļ		I	
N9.5 E14.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>294</td><td></td><td>60</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	9		<lc< td=""><td>294</td><td></td><td>60</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	294		60							
N9.5 E15.5	<lc< td=""><td>-18</td><td></td><td><lc< td=""><td>54</td><td></td><td>33</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-18		<lc< td=""><td>54</td><td></td><td>33</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	54		33							
N9.5 E16.5	<lc< td=""><td>0</td><td></td><td></td><td>402</td><td></td><td>72</td><td></td><td>5</td><td>8</td><td><lc< td=""><td>-25</td><td></td><td>7</td></lc<></td></lc<>	0			402		72		5	8	<lc< td=""><td>-25</td><td></td><td>7</td></lc<>	-25		7
N9.5 E17.5	<lc< td=""><td>-9</td><td>35</td><td></td><td>1151</td><td>5</td><td>48</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></lc<>	-9	35		1151	5	48							
N9.5 E18.5	] 1	NA	NA		NA	NA							1	
N9.5 E19.5	<u> </u>	NA	NA	1	NA	NA	-1		1				1	
N9.5 E2.5	<lc< td=""><td>9</td><td></td><td><lc< td=""><td>107</td><td></td><td>39</td><td></td><td>-</td><td></td><td></td><td><del></del></td><td>1</td><td></td></lc<></td></lc<>	9		<lc< td=""><td>107</td><td></td><td>39</td><td></td><td>-</td><td></td><td></td><td><del></del></td><td>1</td><td></td></lc<>	107		39		-			<del></del>	1	
N9.5 E20.5		NA	NA		NA	NA			-+-				1	
N9.5 E21.5		NA	NA		NA	NA			-+-				<u>†</u>	·
N9.5 E3.5	<lc< td=""><td>9</td><td></td><td></td><td>1098</td><td></td><td>12#</td><td><lc< td=""><td>-1</td><td></td><td><lc< td=""><td>38</td><td>+</td><td>7</td></lc<></td></lc<></td></lc<>	9			1098		12#	<lc< td=""><td>-1</td><td></td><td><lc< td=""><td>38</td><td>+</td><td>7</td></lc<></td></lc<>	-1		<lc< td=""><td>38</td><td>+</td><td>7</td></lc<>	38	+	7

Lc indicates less than the critical level of activity which can be said to be above background.
A negative value is the calculated result of a reading which is below the instrument-specific background.

i

;

÷)

١

[			DIRECT				TRANSFERABLE					
	ALPHA/100 SQ CM			BETA-GAMMA/100 SQ CM			ALPHA/10	SQ CM	BETA-GAMMA/100 SQ C			
LOCATION/ITEM	SMP	L	STD		SMPL	STD	SMPL	STD	SMPL	STD		
COORDINATES	DPN	<u>1</u> .	DEV		DPM	DEV	DPM	DEV	DPM	DEV		
N9.5 E4.5	<lc< td=""><td>-9</td><td>35</td><td><lc< td=""><td>187</td><td>448</td><td></td><td>T</td><td></td><td></td></lc<></td></lc<>	-9	35	<lc< td=""><td>187</td><td>448</td><td></td><td>T</td><td></td><td></td></lc<>	187	448		T				
N9.5 E5.5	<lc< td=""><td>0</td><td>40</td><td><lc< td=""><td>161</td><td>445</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	0	40	<lc< td=""><td>161</td><td>445</td><td></td><td></td><td></td><td></td></lc<>	161	445						
N9.5 E6.5	<lc< td=""><td>-9</td><td></td><td><lc< td=""><td>241</td><td>454</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-9		<lc< td=""><td>241</td><td>454</td><td></td><td></td><td></td><td></td></lc<>	241	454						
N9.5 E7.5	<lc< td=""><td>18</td><td>47</td><td><lc< td=""><td>187</td><td>448</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	18	47	<lc< td=""><td>187</td><td>448</td><td></td><td></td><td></td><td></td></lc<>	187	448						
N9.5 E8.5	<lc< td=""><td>-28</td><td>24</td><td><lc< td=""><td>214</td><td>451</td><td></td><td></td><td></td><td></td></lc<></td></lc<>	-28	24	<lc< td=""><td>214</td><td>451</td><td></td><td></td><td></td><td></td></lc<>	214	451						
N9.5 E9.5	<lc< td=""><td>0</td><td>-40</td><td><lc< td=""><td>54</td><td>433</td><td></td><td>T</td><td></td><td></td></lc<></td></lc<>	0	-40	<lc< td=""><td>54</td><td>433</td><td></td><td>T</td><td></td><td></td></lc<>	54	433		T				

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

J

#### Bliss and Laughlin Steel Characterization Survey of Elevated Locations in the Special Finishing Area Identified by Floor Monitor Scans

		DIRECT									
	ALPHA/100	BETA-GAMMA/100 SQ CM			ALPHA/100 SQ CM			BETA-GAMMA/100 SQ CM			
LOCATION/ITEM	SMPL	STD		SMPL	STD	SN	/IPL	STD		SMPL	STD
COORDINATES	DPM	DEV		DPM	DEV	D	РМ	DEV		DPM	DEV
N 3.7 E 9.35	15	26		42270	2126		5	8	<lc< td=""><td>12</td><td>76</td></lc<>	12	76
N 7.6 E 8.1	3165	335		135430	3755		224	50		1734	181
N 8.1 E 7.2	181	81		280257	5384		72	28		258	98
N 8.5 E 6.7	1129	200		29019	1776	1	17	14		152	89
N 6.7 E 5.7	42	41		17213	1393	1	23	16		184	92
N 8.2 E 0.1	98	60		218953	4763	<lc< td=""><td>0</td><td>0</td><td><lc< td=""><td>33</td><td>78</td></lc<></td></lc<>	0	0	<lc< td=""><td>33</td><td>78</td></lc<>	33	78
N 8.3 E 0.9	15	26		14777	1300	<lc< td=""><td>0</td><td>· 0</td><td><lc< td=""><td>33</td><td>78</td></lc<></td></lc<>	0	· 0	<lc< td=""><td>33</td><td>78</td></lc<>	33	78
N 4.8 E 11	33	36		55387	2422	<lc< td=""><td>0</td><td>0</td><td><lc< td=""><td>25</td><td>77</td></lc<></td></lc<>	0	0	<lc< td=""><td>25</td><td>77</td></lc<>	25	77
N 4.5 E 16.5	88	57		71985	2752		2	6	<lc< td=""><td>20</td><td>77</td></lc<>	20	77
N 3.4 E 17	<pre>Lc 6</pre>	19		6559	919		2	6	<lc< td=""><td>-12</td><td>73</td></lc<>	-12	73

<Lc indicates less than the critical level of activity which can be said to be above background.

A negative value is the calculated result of a reading which is below the instrument-specific background.

.....

.)

)

#### Bliss Laughlin Steel Characterization Area in Grid E16, 5-point Survey

(	
	<u> </u>

1

)

		DIRECT			TRANSFERABLE							
	ALPHA/100 SQ CM		BETA-GAMMA/1	00 SQ CM	ALPHA/100 S	Q CM	BETA-GAMMA/100 SQ CM					
LOCATION/ITEM	SMPL	STD	SMPL	STD	SMPL	STD	SMPL	STD				
COORDINATES	DPM	DEV	DPM	DEV	DPM	DEV	DPM	DEV				
N0 E3	15	26	562	478								
N1 E3	24	32	589	481								
N2 E3	42	41	562	478								
N 0.5 E 3.5	24	32	669	489			1					
N 1.5 E 3.5	42	41	<lc 187<="" th=""><th>436</th><th></th><th></th><th></th><th></th></lc>	436								
N0 E4	24	32	1526	572	5	8	<lc 25<="" th=""><th>77</th></lc>	77				
N1 E4	15	26	3641	738	2	6	<lc 37<="" th=""><th>78</th></lc>	78				
N2 E4	<lc 6<="" th=""><th>19</th><th>402</th><th>460</th><th></th><th></th><th></th><th></th></lc>	19	402	460								
N 0.5 E 4.5	<lc 6<="" th=""><th>19</th><th>642</th><th>487</th><th></th><th></th><th></th><th></th></lc>	19	642	487								
N 1.5 E 4.5	15	26	<lc 321<="" th=""><th>451</th><th></th><th></th><th></th><th></th></lc>	451								
N0 E5	52	45	990	522	<lc 0<="" th=""><th>0</th><th><lc 33<="" th=""><th>78</th></lc></th></lc>	0	<lc 33<="" th=""><th>78</th></lc>	78				
N1 E5	42	41	589	481								
N2 E5	24	32	1205	543	<lc 0<="" th=""><th>0</th><th><lc 12<="" th=""><th>76</th></lc></th></lc>	0	<lc 12<="" th=""><th>76</th></lc>	76				
QC	33	36	937	517	<lc 0<="" th=""><th>0</th><th><lc 0<="" th=""><th>74</th></lc></th></lc>	0	<lc 0<="" th=""><th>74</th></lc>	74				

<Lc indicates less than the critical level of activity which can be said to be above background.</p>
A negative value is the calculated result of a reading which is below the instrument-specific background.

## Appendix B COST ESTIMATE

ì

)

,

)

#### Bliss & Laughlin Cost Estimate Alternative 2 Institutional Controls Cost in FY1998\$

	az nome		FulsI Cost		Lotal Last
	N. NO		(78 198)		
					"Contogracy)
3XXX	Bliss & Laughlin Project	5	302,537	S	347,917
32XX	Studies and Design	1 s			
33XXX	Htrw Construction Activities	Ś		Ś	
331XX	Htrw Remedial Action (Construction)	S	•	5	
331XX01	Mobilization And Preparatory Work	5		Ś	
331XX02	Monitoring, Sampling, Testing, And Analysis	5		\$	•
331XX0201	IRA	\$		\$	<u> </u>
331XX0202	Exc/Transp	\$	-	\$	 •
331XX03	Site Work	S	•	5	
331XX0301	Site Work - Preliminary	\$	-	\$	•
331XX0302	Site Work - Sustaining	\$	•	\$	······································
331XX04	Oe-Cwm Removal And Destruction	\$	-	\$	
331XX05	Surface Water Collection And Control	\$		\$	•
331XX06	Groundwater Collection And Control	\$		\$	
331XX07	Air Pollution/Gas Collection And Control	\$	•	\$	•
331XX08	Solids Collection And Containment	\$	-	\$	•
331XX0801	Excavation	\$	-	\$	
331XX0802	Backfill	\$	•	\$	-
331XX09	Liquids/Sediments/Sludges Collection And Containment	\$	-	\$	•
331XX10	Drums/Tanks/Structures/Misc Demolition And Removal	\$	-	\$	
331XX11	Biological Treatment	\$	-	\$	•
331XX12	Chemical Treatment	\$	•	\$	•
331XX13	Physical Treatment	\$	-	\$	•
331XX14	Thermal Treatment	\$	•	\$	•
331XX15	Stabilization/Fixation/Encapsulation	\$	-	\$	-
331XX16	(Reserved For Future Use)	\$	-	\$	
331XX17	Decontamination And Decommissioning (D&D)	\$		\$	•
331XX18	Disposal (Other Than Commercial)	\$	-	\$	-
331XX1801	Transportation to Storage/Disposal Facility	\$	+	\$	-
331XX1802	Disposal Fees and Taxes	\$	-	\$	•
331XX19	Disposal (Commercial)	\$		\$	•
331XX1901	Transportation to Storage/Disposal Facility	\$	-	\$	-
331XX1902	Disposal Fees and Taxes	\$	-	\$	-
331XX20	Site Restoration	\$	•	\$	•
331XX21	Demobilization	\$		\$	· ·
331XX22	General Requirements (Optional Breakout)	\$		\$	•
331XX2201	Supervision, Management & Administration	\$		\$	· · ·
331XX2202	ICSM RA	\$	<u> </u>	\$	•
331XX9X	Other (Use Numbers 90-99)	5		\$	•
332XX	Engineering During Construction (Edc)	\$		\$	
333XX	Supervision & Admin (S&A) (Construction Management)	\$		\$	
34XXX	HTRW (POST CONSTRUCTION)	5	302,537	\$	347,917
342XX	HTRW OPERATION AND MAINTENANCE (POST CONSTRUCTION)	\$	302,537	\$	347,917
342XX01	MONITORING, SAMPLING, TESTING, AND ANALYSIS	\$	88,599	\$	101,889
342XX02	ICSM O&M	\$	191,520	\$	220,248
342XX03	Project Management	\$	22,418	\$	25,780
343XX	Supervision & Admin (S&A) (Construction Management)	\$	-	\$	· · · ·

1

Contingency is a standard 15% unless otherwise noted.

BlissInstCon.xls

)

)

2

į.

)

#### Bliss & Laughlin Cost Estimate Alternative 3 Building Decontamination Cost in FY1998\$

		-		F	
					Lotal Cost
WIIS Elemen	r Schwity		- Indal Cost		(50-1993)
			(\$ <b>F</b> ¥99)		TWI Commence
3XXX	Bliss and Laughlin Project	5	305,664	\$	351,514
32XX	Studies and Design	\$	•	\$	
33XXX	Htrw Construction Activities	\$	290,437	\$	334,003
331XX	Htrw Remedial Action (Construction)	\$	264,034	\$	303,639
331XX01	Mobilization And Preparatory Work	\$	4,729	\$	5,439
331XX02	Monitoring, Sampling, Testing, And Analysis	\$	15,049	\$	17,307
331XX0201	RA	\$	14,780	\$	16,997
331XX0202	Exc/Transp	\$	269	\$	309
331XX03	Site Work	\$	59,265	\$	68,143
331XX0301	Site Work - Preliminary	\$	50,000	\$	57,500
331XX0302	Site Work - Sustaining	\$	9,255	\$	10,643
331XX04	Oe-Cwm Removal And Destruction	\$	•	\$	
331XX05	Surface Water Collection And Control	\$	-	\$	
331XX06	Groundwater Collection And Control	\$	•	\$	
331XX07	Air Pollution/Gas_Collection And Control	\$	•	\$	-
331XX08	Solids Collection And Containment	\$	-	\$	•
331XX0801	Excavation	\$	-	\$	•
331XX0802	Backfill	\$	•	\$	
331XX09	Liquids/Sediments/Sludges Collection And Containment	\$	-	\$	-
331XX10	Drums/Tanks/Structures/Misc Demolition And Removal	\$		\$	
331XX11	Biological Treatment	\$	-	\$	
331XX12	Chemical Treatment	\$	-	\$	-
331XX13	Physical Treatment	\$	•	\$	•
331XX14	Thermal Treatment	\$	•	\$	
331XX15	Stabilization/Fixation/Encapsulation	\$		\$	
331XX16	(Reserved For Future Use)	\$	-	\$	
331XX17	Decontamination And Decommissioning (D&D)	\$	3,736	\$	4,296
331XX18	Disposal (Other Than Commercial)	\$	-	\$	
331XX1801	Transportation to Storage/Disposal Facility	\$	•	\$	-
331XX1802	Disposal Fees and Taxes	\$	-	\$	
331XX19	Disposal (Commercial)	\$	5,379	\$	6,186
331XX1901	Transportation to Storage/Disposal Facility	\$	1,959	\$	2,253
331XX1902	Disposal Fees and Taxes	\$	3,420	\$	3,933
331XX20	Site Restoration	\$		\$	-
331XX21	Demobilization	\$	4,504	\$	5,180
331XX22	General Requirements (Optional Breakout)	\$	58,917	\$	67,754
331XX2201	Supervision, Management & Administration	\$	57,853	\$	66,531
331XX2202	ICSM RA	\$	1,064	\$	1,224
331XX9X	Other (Use Numbers 90-99)	\$	112,464	\$	129,334
332XX	Engineering During Construction (Edc)	\$	-	\$	
333XX	Supervision & Admin (S&A) (Construction Management)	\$	26,403	\$	30,364
34XXX	HTRW (POST CONSTRUCTION)	\$	15,227	\$	17,511
342XX	HTRW OPERATION AND MAINTENANCE (POST CONSTRU	\$	13,843	\$	15,919
342XX01	MONITORING, SAMPLING, TESTING, AND ANALYSIS	\$	3,695	\$	4,249
342XX02	ICSM O&M	\$	532	\$	612
342XX03	Project Management	\$	9,615	\$	11,058
343XX	Supervision & Admin (S&A) (Construction Management)	\$	1,384	\$	1,592

1

Contingency is a standard 15% unless otherwise noted.

Blisslaf.xls

}

)

.)

)

ł